Filtration process in earth fill dam body and its chemical effect on piezometers

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Abstract. Estimation of aggressiveness of filtration flow in the dam body is gaining importance in providing the stability of reservoir dam and its parts. In order to estimate the aggressiveness of filtration flow in the dam body it is necessary to know the movement pattern of filtration water in reservoir dam and its effect on dam elements. The article brings up the definition of gradients of filtration flow in the dam body, analysis of the reasons of their change by cross section at the example of Tashkent reservoir dam. Besides, chemical composition of water in piezometers has been analyzed, aggressive effect of sulfate salts on piezometers, and their corrosion have been determined. Measures on systematic piezometer observations are mentioned.

1 Introduction

The goal of the research is to determine filtration flow gradients in the dam body, analyze the reasons of their change by cross section, estimate water filtration effect on structure elements at the example of Tashkent reservoir dam. In order to estimate the aggressiveness of filtration flow in the dam body it is necessary to know the movement pattern of filtration water in reservoir dam and its effect on the dam elements. The results of the analysis gain importance in providing the stability of reservoir dam and its parts [1, 2, 3, 4, 5, 6].

Filtration water in the reservoir dam body usually move in chaotic flow, in particular, filtration flow is nonpressure flow. It is known, that in nonpressure flow filtration flow has an open surface, moves towards the side from the upper part of the dam to its lower part. The head difference is

$$\Delta \mathbf{H} = \mathbf{H}_1 - \mathbf{H}_2 \,.$$

Filtration flow gradient (J) is the ratio of the head difference of filtration flow in the dam body ($\Delta H = H_1$ - H_2) to the length of filtration path:

$$J = \frac{\Delta H}{l} \tag{1}$$

Filtration flow in the dam body follow the Darcy's law. Such movement can be thoroughly observed in the base soils and in the dam body, including sands, loams and sandy loams [7, 8].

Filtration flow discharge in the dam body can by determined by the following equation according to the law of the French scientist Darcy:

$$Q = K_{\phi} F \frac{\Delta H}{l} = K_{\phi} F J \tag{2}$$

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where: Q – filtration flow discharge, i.e. amount of filtrated water through soil in a unit of time, m^3/day ;

 K_{φ} - filtration coefficient, i.e. the amount, expressing the ability of the dam soil pass water through itself, m/day;

F – filtration flow zone cross section area, m^2 ;

l- filtration flow path length, m;

 Δ H- head difference of the head race and the tail race, m;

By dividing the both sides of the equation by (F), we can determine filtration velocity $v=K_{\phi} J$.

Thus, by Darcy's law, it is considered that the velocity (v) of filtration or water movement in soil, composing the dam body is proportionate to filtration head gradient (J) and filtration coefficient.

In cases, when head gradient $J = \frac{\Delta H}{l} = 1$, the equation $v = K_{\phi} J$ becomes $v = K_{\phi}$, i.e. filtration coefficient will be equal to filtration velocity in relation with numerical value [9].

While estimating the filtration stability of the earth fill dam and its antifiltration elements the following conditions must be met:

$$J_{est,m} = \frac{\Delta H}{t_2} \le J_{cr,m} = J_{\text{AOI}} \qquad J_{est,m} \le \frac{1}{y_n} J_{cr}$$
(3)

where: $J_{est,m}$ - mean gradient of the dam design element.

 γ_n – dam reliability coefficient (I-class-1,25; II-class-1,2; III-class-1,15; IV-class-1,1);

 J_{cr} - mean filtration gradient allowable for earth fill dams.

2 Method

Collection of data from hydrometheorological stations and reservoir operation. Mathematical processing of statistical data and comparison of the obtained data with field observations [10,11,12].

3 Results

Tashkent reservoir dam is made of local soil and has a core. Design amount of the mean filtration head gradient for the core and prism is determined by the following equation for such dams:

For the core
$$J_{\text{доп}} = \frac{1}{\chi_n} J_{cr}$$
 (4)

For the prism
$$J_{\text{доп}} = \frac{1}{\gamma_n} J_{cr}$$
 (5)

On the basis of field research gradients have been calculated between piezometers 1, 2, 3, 4 and 5, located at section N_{99} (IIK 22+00) of Tashkent reservoir dam and the results are shown in Table 1 and Picture 2 [13,14]. Tashkent reservoir dam cross section is shown in Picture 1.



Fig. 1. Tashkent reservoir dam cross section.

Table 1. Design gradients between the piezometers in the Tashkent reservoir dam.

Piezometers	Design	Years					
	gradients	2012	2013	2014	2015	2016	2017
П1-П2	0.75	1,33	0,92	1,17	1,42	1,16	1,08
П2-П3	0.55	0,42	0,42	0,42	0,42	0,39	0,39
П3-П4	0.024	0,017	0,024	0,018	0,019	0,024	0,024
П4-П5	0.031	0,031	0,031	0,029	0,028	0,031	0,031

The analysis show, that according to the design results, filtration water movement velocity and head differences are large and filtration path is short in the section between piezometers 1,2 and 3, but in section between piezometers 3,4 and 5 filtration water movement velocity and head differences are low and filtration path is long. As a result, in section between piezometers 3,4 and 5 head gradient sharply decreases. Water stability is observed in the piezometers, if the amount of gradient is very low [15,16,17].

On the results of the research it is considered, that the movement of soil filtration is unsteady. The unsteadiness depends on the amount of gradient between piezometers, located in the dam, i.e. if the gradient is at normal level, then the change of filtration movement will comply with the pattern, and if the amount of gradient is too low, then water level stability is observed in piezometers.

Quality change analysis was conducted for the water samples, taken from Tashkent water reservoir basin and tail race drainage with the purpose of determining the state of changes mentioned above within the research and estimation of water filtration effect on the structure elements (Table 2 and pictures 3,4).



Fig. 2. Gradient change between piezometers in section 9 (IIK 22+00) of the dam.

Water	рН	Hard residual, mg/l	Amount of the basic ions, dissolved in water, mg/l					
sample point			<i>HCO</i> ' ₃	Cľ	SO"4	Ca	Mg	Na'+ K
Water reservoir basin	7,4	265,7	134,4	15,3	74,6	48,8	11,2	20,5
Drainage water	7,59	842,8	242,8	28,7	351,3	148	26	59

Table 2. Chemical analysis of the quality of water, taken from Tashkent water reservoir basin.



Fig. 3. Diagram of the chemical analysis of the quality of water, taken from Tashkent water reservoir basin.



Fig. 4. The staff of the Research Institute of Irrigation and water problems are doing research in the laboratory.

In estimating the filtration water aggressiveness stability of the dam elements in the reservoir, it is necessary to consider the soil filtration coefficient. The aggressive effect of water on the elements, located in soils, where the filtration coefficient is large, can also be high. On the basis of this, water aggressiveness has also been estimated for concrete structures in the head race of Tashkent water reservoir basin (Table 3). Also the aggressiveness of water has been specified for concrete structures and piezometers, located in the body of the dam (Table 4) [18,19,20].

		Results of laboratory analysis	Nonpres	sure structure	
Nº	Data description		Portland cement original and sulfate resistant	Pupallan and Portland cement with slag original and sulfate resistant	Results of determining aggressiveness regarding concrete structures
1	2	3	4	5	6
1	Type of structure	Nonpressure			
2	Size of structure, m	Abobe 2,5			
3	K_{ϕ} , m/day	0,1<Кф<10			
4	Ca ²⁺ , mg/l	48,8			
5	рН	7,76	5,2	5,5	No aggressiveness of general water acidity
6	HCO_3^{-} , mg eq /l	0,7872	0,4	Not standardized	No lye aggressiveness of water
7	Carbxylic acid CO ₂ , mg/l	Not determined			No carboxylic acid aggressiveness of water

 Table 3. Water aggressiveness for concreter structures in the head race of Tashkent water reservoir basin.

8	Chloride, Cl⁻, mg	32,9			
9	Sulfate SO ₄ ²⁻ , mg/l	74,6	74,6<350	74,6<350	No sulfate aggressiveness for usual cement structures
10	Mg ²⁺ , mg/l	11,2	11,2<1000	11,2<1000	No magnesia aggressiveness of water

 Table 4. Aggressive effect on concrete structures and piezometers of filtration water, located in the body of Tashkent water reservoir dam.

	Data	Results of	Nonpres	sure structure	Results of determining
N⁰	description laboratory analysis		Portland cement original and sulfate resistant	Pupallan and Portland cement with slag original and sulfate resistant	aggressiveness regarding concrete structures
1	2	3	4	5	6
1	Type of structure	Nonpressure			
2	Size of structure, m	Above 2,5			
3	Кф, m/day	0,1<Кф<10			
4	Ca2+, mg/l	148			
5	pН	7,59	5,2	5,5	No aggressiveness of general acidity of water
6	НСОЗ-,	3.98	0,4	Not standardized	No lye aggressiveness of water, filtrating through the water reservoir dam
7	mg eq /l	Not determined			No carboxylic acid aggressiveness of water
8	Carbxylic acid CO2, mg/l	28,7	28,7<1000	28,7<1000	Accelerates corrosion o f metal structures
9	Chloride, Cl-, mg	351,3	351,3>350	351,3>350	Has sulfate aggressiveness for usual cement and metal structures
10	Sulfate	26	26<1000	26<1000	No magnesia aggressiveness of water

4 Conclusions

Filtration flow in the body of Tashkent water reservoir dam is sulfate aggressive with regard to concrete and metal structures, it accelerates the corrosion of piezometers in the dam. It requires taking measures on processing the concrete surfaces and joints on the head race of Tashkent water reservoir dam with hydroisolation materials and providing good operation of drainage in the tail race of the dam. Sensitivity of piezometers in the water reservoir dam must be checked, during the process of checking the sensitibility piezometers must be filled with water and then emptied, thus providing the process of water replacement in them. As a result, filtration flow water aggressiveness will decrease with regard to piezometers.

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