## Exercise 2

# Conception of a Landfill



Exercise "Landfill" Solid Waste Management 102

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#### Task 1: Basic Data

Basic Data				
Inhabitants	600,000			
		waste requiring treatmen	nt	waste not requiring
	domestic and bulky waste	domestic waste-like commercial waste	production specific waste	treatment
specific waste potential [kg/(lnh*a)]	300	125	150	20 % of waste requiring treatment
waste amount [Mg/a]				
material utilization [%]	50	40	50	50
waste amount material utilization [Mg/a]				
residual waste = MBT input [Mg/a]				
MBT output to landfill [%]	30	30	30	0
landfill input [Mg/a]				
landfill input [kg/(lnh*a)]				
annual increase [%]	0.5	0.5	-1.0	-1.0



### Task 1: Basic Data

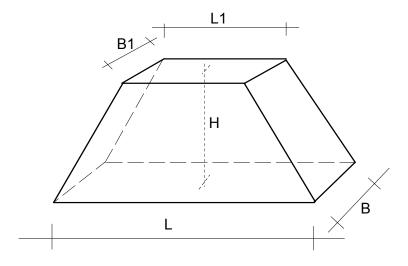
Basic Data				
Inhabitants	600,000			
		waste requiring treatmen	nt	waste not requiring
	domestic and bulky waste	domestic waste-like commercial waste	production specific waste	treatment
specific waste potential [kg/(lnh*a)]	300	125	150	20 % of waste requiring treatment
waste amount [Mg/a]	180,000	75,000	90,000	69,000
material utilization [%]	50	40	50	50
waste amount material utilization [Mg/a]	90,000	30,000	45,000	34,500
residual waste = MBT input [Mg/a]	90,000	45,000	45,000	0
MBT output to landfill [%]	30	30	30	0
landfill input [Mg/a]	27,000	13,500	13,500	34,500
landfill input [kg/(lnh*a)]	45	22.5	22.5	57.5
annual increase [%]	0.5	0.5	-1.0	-1.0



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## Task 2: Landfill Dimensioning



$$V_0 = \frac{1}{6} \cdot [(2 \cdot L + L_1) \cdot B + (2 \cdot L_1 + L) \cdot B] \cdot H$$



Landfill Dimensioning		
length L	m	600
width B	m	300
height H	m	30
general inclination	-	1:4
filling density $\rho_{\text{MBT-Output}}$ $\rho_{\text{n, treated raw waste}}$	Mg/m³ Mg/m³	1.5 1.8
construction waste ratio	Vol%	15
subtraction for ogees and offsets	Vol%	10
maximum size of a landfill section	ha	3.6
L <sub>1</sub>	m	
$B_1$	m	
$V_{o}$	$m^3$	
minus offsets $V_1 = V_{landfill}$	m³	
minus construction waste ratio $\mathrm{V}_{\mathrm{2}}$	m <sup>3</sup>	



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# Task 2: Landfill Dimensioning

Landfill Dimensioning		
length L	m	600
width B	m	300
height H	m	30
general inclination	-	1:4
filling density $\rho_{MBT\text{-}Output}$ $\rho_{n, \text{ treated raw waste}}$	Mg/m³ Mg/m³	1.5 1.8
construction waste ratio	Vol%	15
subtraction for ogees and offsets	Vol%	10
maximum size of a landfill section	ha	3.6
L <sub>1</sub>	m	360
$B_1$	m	60
$V_0$	m <sup>3</sup>	2,736,000
minus offsets $V_1 = V_{landfill}$	$m^3$	2,462,400
minus construction waste ratio V <sub>2</sub>	$m^3$	2,093,040



#### Operating Time of the Landfill

deposited waste in 1st year:

$$G_1 = \sum_{n=1} [G_{n,i}] \cdot Inh = \sum G_{1,i} \cdot Inh$$

Waste Amount in the 1st year		
G1,1 – domestic/bulky waste	Mg/a	27,000
G1,2 – commercial waste	Mg/a	13,500
G1,3 – production specific waste	Mg/a	13,500
G1,4 – not treated waste	Mg/a	34,500



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## Task 2: Landfill Dimensioning

Operating Time of the Landfill				
		waste requiring treatmer	nt	waste not requiring
	domestic and bulky waste	domestic waste-like commercial waste	production specific waste	treatment
waste amount				
1st year [kg/(Inh*a)]				
1st year [Mg/a]				
last year [kg/(lnh*a)]				
last year [kg/(lnh*a)]				
operating time				
deposited waste in $n^{th}$ year $G_n$				
deposited waste total $G_{\text{total}}$				



Operating Time of the Landfill				
		waste requiring treatmen	nt	waste not requiring
	domestic and bulky waste	domestic waste-like commercial waste	production specific waste	treatment
waste amount				
1st year [kg/(Inh*a)]	45	22.5	22.5	57.5
1 <sup>st</sup> year [Mg/a]	27,000	13,500	13,500	34,500
last year [kg/(lnh*a)]				
last year [kg/(lnh*a)]				
operating time				
deposited waste in $n^{th}$ year $G_n$				
deposited waste total G <sub>total</sub>				



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### Task 2: Landfill Dimensioning

Operating Time of the Landfill

deposited waste in nth year:

$$G_n = \sum_{n=1} \left[ G_{1,i} \cdot \left( 1 + \frac{p_i}{100} \right)^{n-1} \right] \cdot Inh$$

approximate total amount in n years:

$$G_{total} = \frac{G_1 + G_n}{2} \cdot n = V_2 \cdot \rho$$

Rearranging for n and solving iteratively. Start with n = 30 a.

$$n = \frac{2 \cdot V_2 \cdot \rho}{G_1 + G_n}$$

Averaged density:

$$\rho = 1.5 \ \frac{Mg}{m^3} \cdot \frac{54,000}{88,500} + 1.8 \ \frac{Mg}{m^3} \cdot \frac{34,500}{88,500} = 1.62 \ Mg/m^3$$



Operating Time of the Landfill				
		waste requiring treatmen	nt	waste not requiring
	domestic and bulky waste	domestic waste-like commercial waste	production specific waste	treatment
waste amount				
1st year [kg/(lnh*a)]	45	22.5	22.5	57.5
1 <sup>st</sup> year [Mg/a]	27,000	13,500	13,500	34,500
last year [kg/(lnh*a)]	54.5	27.25	15.3	39.09
last year [kg/(lnh*a)]	32,698.33	16,349.16	9,178.16	23,455.29
operating time		а		39,39
deposited waste in $n^{th}$ year $G_n$		Mg/a		81,680.94
deposited waste total $G_{\text{total}}$		Mg		3,351,975.33

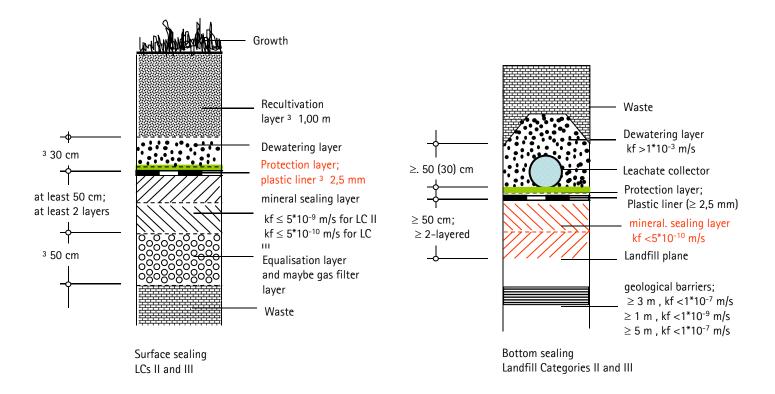


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## Info: Surface and Bottom Sealing





#### Task 3: Landfill Gas Calculation

Landfill Gas Calculation							
			waste requiring treatment was			aste not requiring treatment	
		domestic and bulky waste	domestic waste-like commercial waste	production specific waste	treat	tment	
waste to be	deposited G <sub>1,i</sub> [Mg/a]						
composition	[%]						
specC-Con	Content [kg TC / Mg]						
t <sub>h</sub>	half-life [a]				10		
k	degradation constant k= In 0.5/t <sub>h</sub>					0.069	
t time between the calculated begin and the considered year of the gas production [a]				variable			
f <sub>ao</sub>	f <sub>ao</sub> initial time factor to consider the gas production during the first half year after depositing [-]				0.8		
f <sub>a</sub>	degradation factor; ratio of TC gasifiable under optimal conditions to total TC [-]				0.7		
$f_o$	optimization factor [-]					0.7	



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55 %

#### Task 3: Landfill Gas Calculation

**Landfill Gas Production** 

system-related collection rate [%]

$$Q_{a,t} = 1.868 \cdot \textit{M} \cdot \textit{TC} \cdot f_{ao} \cdot f_a \cdot f_o \cdot f_s \cdot k \cdot e^{-kt}$$

$$M_1 \cdot TC_{1,i} = \sum G_{1,i} \cdot E \cdot spec.TC$$

Exercise "Landfill"

#### Task 3: Landfill Gas Calculation

Landfill Gas Production			
annual sum year 1	kg	TC <sub>1</sub>	31,725,000
annual sum year 2	kg	TC <sub>2</sub>	32,359,500
annual sum year 3	kg	TC <sub>3</sub>	33,006,690
annual sum year 4	kg	TC <sub>4</sub>	33,463,166



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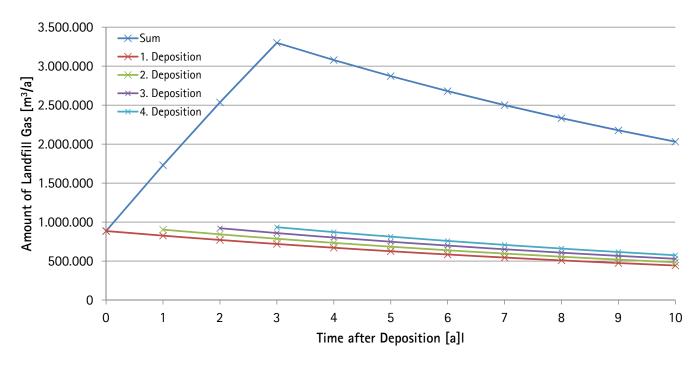
### Task 3: Landfill Gas Calculation

Landfill Gas Prode	uction				
Time t [a]	Year 1	Year 2	Year 3	Year 4	Σ
0	885.631	-	-	-	885.631
1	826.323	903.343	-	-	1.729.666
2	770.986	842.849	921.410	-	2.535.246
3	719.356	786.406	859.706	934.153	3.299.621
4	671.183	733.743	802.134	871.596	3.078.656
5	626.236	684.606	748.418	813.228	2.872.487
6	584.298	638.760	698.298	758.768	2.680.125
7	545.170	595.984	651.535	707.956	2.500.645
8	508.661	556.073	607.904	660.546	2.333.185
9	474.598	518.835	567.195	616.311	2.176.938
10	442.815	484.090	529.211	575.039	2.031.155



#### Task 3: Landfill Gas Calculation

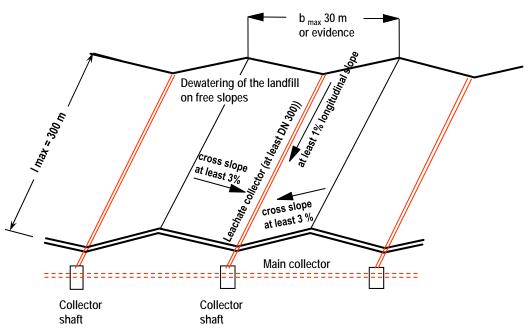
#### **Landfill Gas Production**





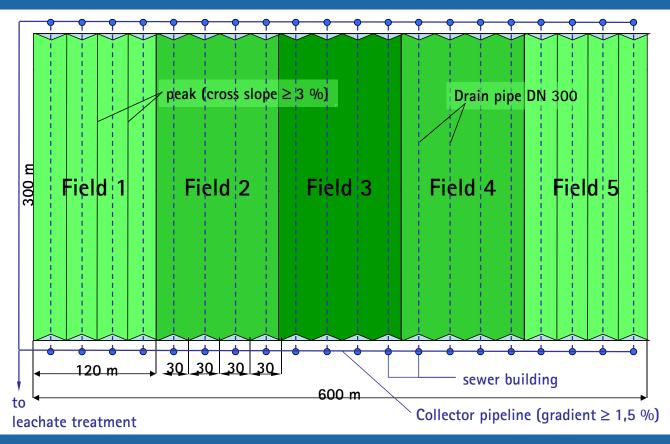
### Task 4: Drainage System

Landfill Drainage System





### Task 4: Drainage System

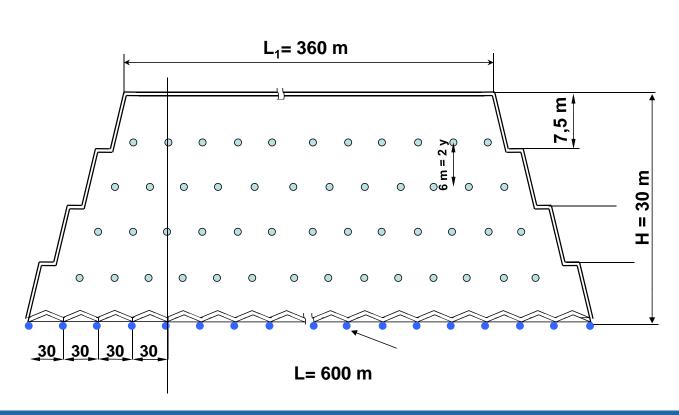


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Task 5: Degassing System





### Task 5: Degassing System

Degassing Capacity		
height H	m	30
length L	m	600
number of terraces		4
H <sub>1</sub>	m	
L <sub>1</sub>	m	
distance degassing layers	m	6
elliptic axis of degassing area x	m	
elliptic axis of degassing area y	m	
degassing area A	m <sup>2</sup>	
capacity $Q_a/Q_t$	%	

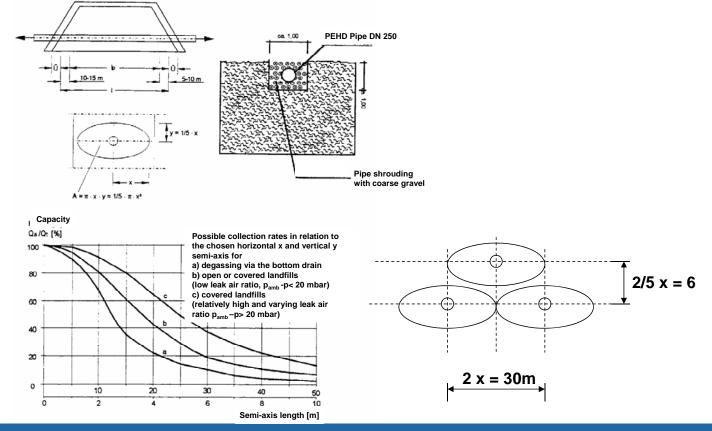


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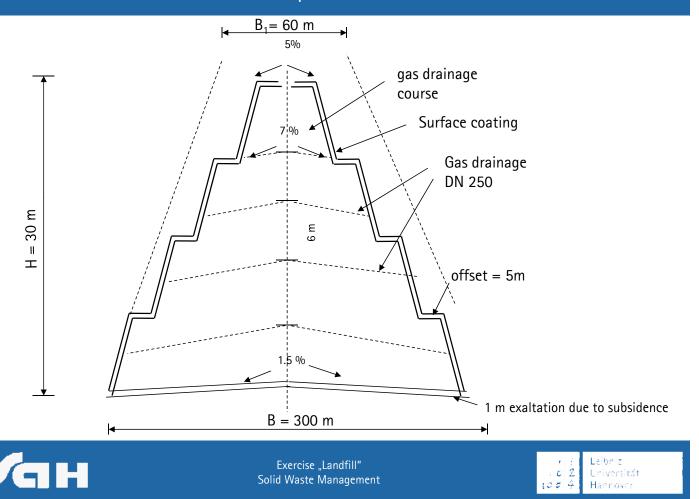
### Task 5: Degassing System





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#### Info: Effect of a Complete Enclosure of Landfills



### Info: Effect of a Complete Enclosure of Landfills

- The leachate amount and landfill gas amount will be reduced with an intact surface sealing.
- · Constructions for leachate and gas treatment can be less dimensioned
- · Lower costs of the treatment plants for investments and ongoing maintenance measures
- Better stability
- Lower environmental harm by uncontrolled emergent leachate and landfill gas
- Reform of the flora growth conditions above the sealing. Because of the flora damages emissions of landfill gas has to be stopped.
- Better oxygen supply for the flora
- Lower emissions of smell
- Better collection and alternative usages of the landfill gas
- · Biological degradation processes will be disrupted by missing water inflow,
  - i.e. reduced inertisation of the waste (-> long maintenance) and artificial moisturisation for gas formation
- Continuous potential of gas and eluation over a longer period. Possible mobilisation by degradation of sealing properties.
- Plastic liner (PL) is like a baffle
  - -> unhindered heat transport goes to seasoning of surface soil
  - -> seasoning of vegetation layer (-> bad vegetation)
  - -> danger by slipping of surface soil at the plastic liner in the berm
- · Higher investment and maintenance costs



## Task 5: Degassing System

Degassing Capacity		
height H	m	30
length L	m	600
number of terraces		4
H <sub>1</sub>	m	7.5
L <sub>1</sub>	m	360
distance degassing layers	m	6
elliptic axis of degassing area x	m	15
elliptic axis of degassing area y	m	3
degassing area A	m <sup>2</sup>	141.37
capacity $Q_a/Q_t$	%	60



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### **Task 6: Leachate amounts**

Landfill Leachate

treatment capacitiy 60 m³/d

plant availability 80 %

operating time 12 months/year

month	leachate amount Q <sub>t</sub> [m³/month]	sum of influent $\Sigma Q_z$ [m <sup>3</sup> ]	sum of effluent $\Sigma Q_S$ [m <sup>3</sup> ]	storage capacity [m³]
January	6.230	6.230		
February	2.540	8.770		
March	3.290	12.060		
April	1.200	13.260		
May	35	13.295		
June	290	13.585		
July	410	13.995		
August	725	14.720		
September	530	15.250		
October	640	15.890		
November	2.356	18.246		
December	3.210	21.456		



## Leachate influent and effluent

month	leachate amount Q <sub>t</sub> [m³/month]	sum of influent $\Sigma Q_z$ [m <sup>3</sup> ]	sum of effluent $\Sigma Q_S$ [m $^3$ ]	storage capacity [m³]
January	6.230	6.230	1.460	
February	2.540	8.770	2.920	
March	3.290	12.060	4.380	
April	1.200	13.260	5.840	
May	35	13.295	7.300	
June	290	13.585	8.760	
July	410	13.995	10.220	
August	725	14.720	11.680	
September	530	15.250	13.140	
October	640	15.890	14.600	
November	2.356	18.246	16.060	
December	3.210	21.456	17.520	



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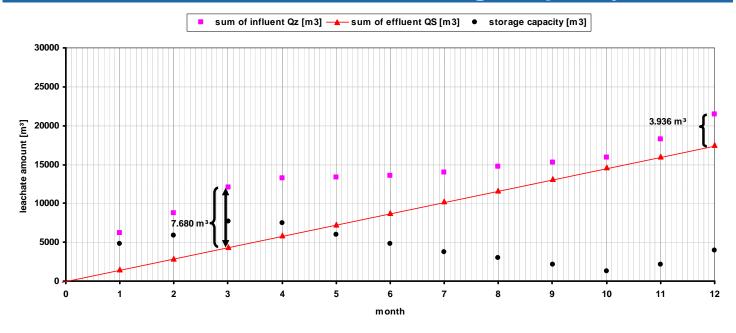
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# Leachate influent and effluent

sum of leachate amount sum of storage influent effluent Q<sub>t</sub> [m<sup>3</sup>/month] capacity month  $\Sigma Q_z$  [m<sup>3</sup>]  $\Sigma Q_{\rm S}$  [m<sup>3</sup>]  $[m^3]$ 6.230 January 6.230 1.460 4.770 February 2.540 8.770 2.920 5.850 March 3.290 12.060 4.380 7.680 1.200 **April** 13.260 5.840 7.420 35 May 13.295 7.300 5.995 June 290 13.585 8.760 4.825 410 July 13.995 10.220 3.775 August 725 14.720 11.680 3.040 September 530 15.250 13.140 2.110 October 640 15.890 14.600 1.290 November 2.356 18.246 16.060 2.186 3.210 December 21.456 17.520 3.936



## Determination of leachate storage capacity





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### Reduction of the storage volume at 3.000 m<sup>3</sup>

(max. leachate amount – storage volume) / number of month

 $(12.060 \text{ m}^3 - 3.000 \text{ m}^3) / 3 \text{ month} = 3.020 \text{ m}^3/\text{month} => 99,29 \text{ m}^3/\text{d}$ 

-> magnification of leachate treatment plant about 99,29/(60  $\cdot$  0,8)  $\cdot$ 100% = ca. 206,8 %

Dead time of the leachate treatment plant

biological treatment: reduction of the efficiency factor

membrane: conservationthermal treatement: energy loss

recommissioning costs, amortisation calculation



## Leachate influent and effluent

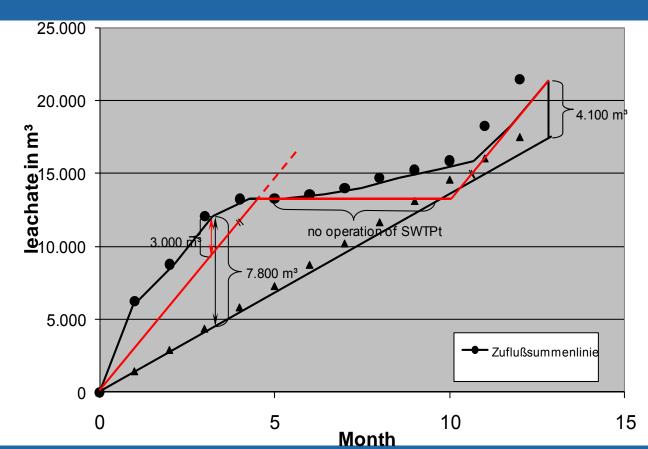
month	leachate amount Q <sub>t</sub> [m³/month]	sum of influent $\Sigma Q_z$ [m <sup>3</sup> ]	sum of effluent $\Sigma Q_S$ [m $^3$ ]	storage capacity [m³]
January	6.230	6.230	3.019	3.211
February	2.540	8.770	6.039	2.731
March	3.290	12.060	9.058	3.002
April	1.200	13.260	12.077	1.183
May	35	13.295	12.077	1.218
June	290	13.585	12.077	1.508
July	410	13.995	12.077	1.918
August	725	14.720	12.077	2.643
September	530	15.250	12.077	3.173
October	640	15.890	15.096	794
November	2.356	18.246	18.116	130
December	3.210	21.456	21.135	321



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# Reduction of the storage volume at 3.000 m<sup>3</sup>





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