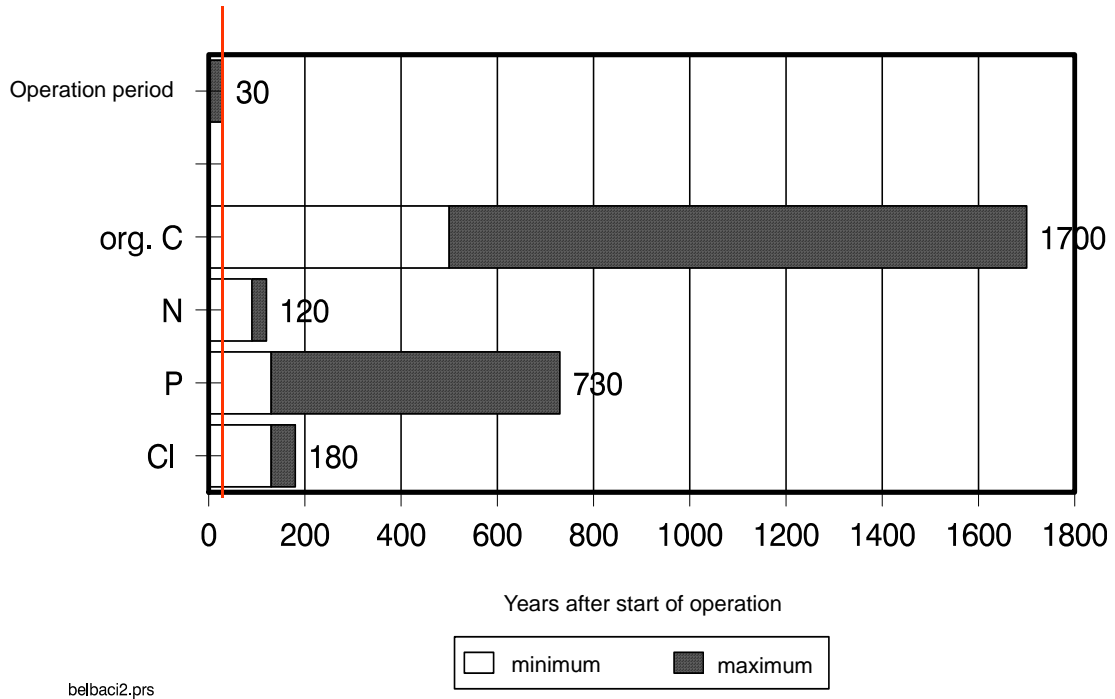


10. Waste Depositing I Waste Depositing II

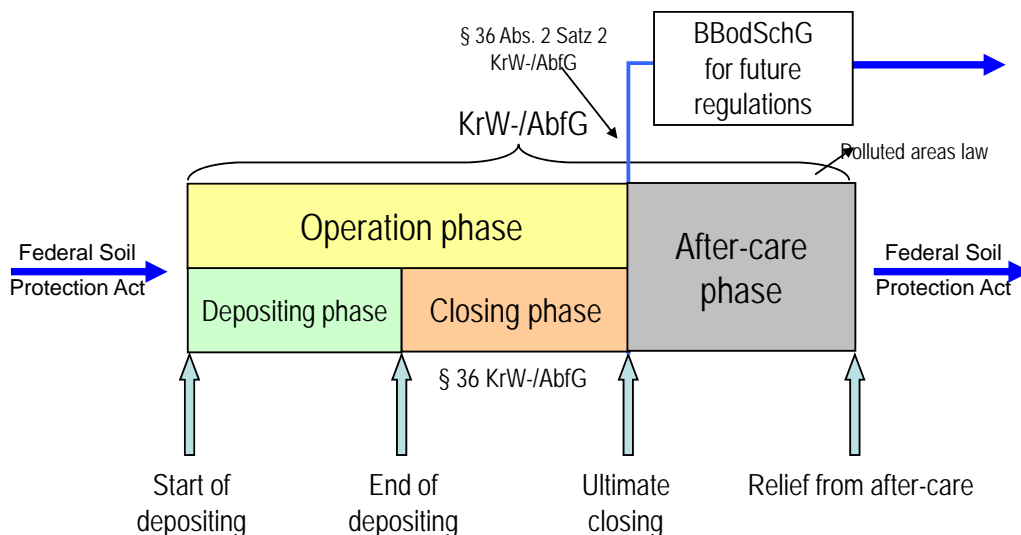
Definitions – Ecological Consequences of the Depositing of Raw Waste

- **Depositing** = no time limit
- **(intermediate) storage** = time limit
- Consequences of the depositing of raw waste:
 - **Leaching** through rainfall → leachate → groundwater pollution if the dumping ground bottom is permeable, or – if the bottom is leak-proof – accumulation of leachate + treatment efforts
 - **chemical reactions + bio-chemical conversions**; decomposition in aerobic boundary areas; ageing in the aerobic landfill interior;
 - emergence of **landfill gas** + odour emissions;
 - **noise emissions** (delivery trucks; possibly waste comminution; installation devices);
 - **dust emissions** (delivery trucks; possibly waste comminution), drift-off (particularly plastic foils);
 - infestation with birds and vermin (cause: food supply) → hygienic hazards



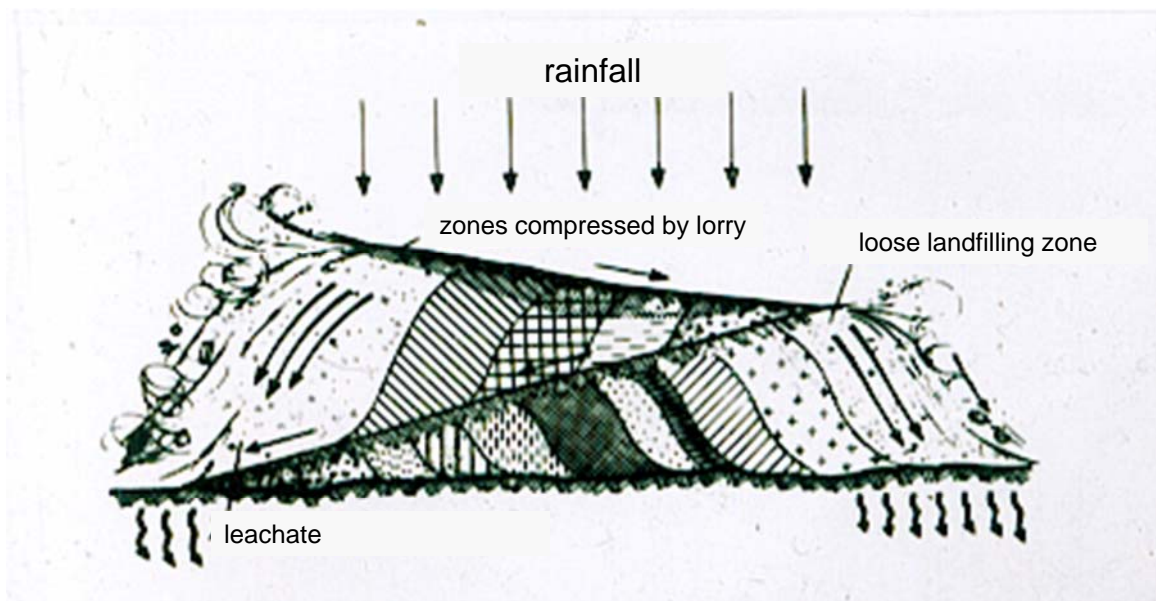
belbaci2.prs

Relation of Waste Law (Landfill Directive) to Soil Protection Law



- §3 Section 1, No. 2 BBodSchG (Federal Soil Protection Act) states that the BBodSchG is applied for regulations of the KrW-/AbfG (Recycling Waste Management Law) on the licensing and operation of waste depositing plants and on the closing of landfills as far as these directives do not regulate effects on soils.

Loose Landfilling



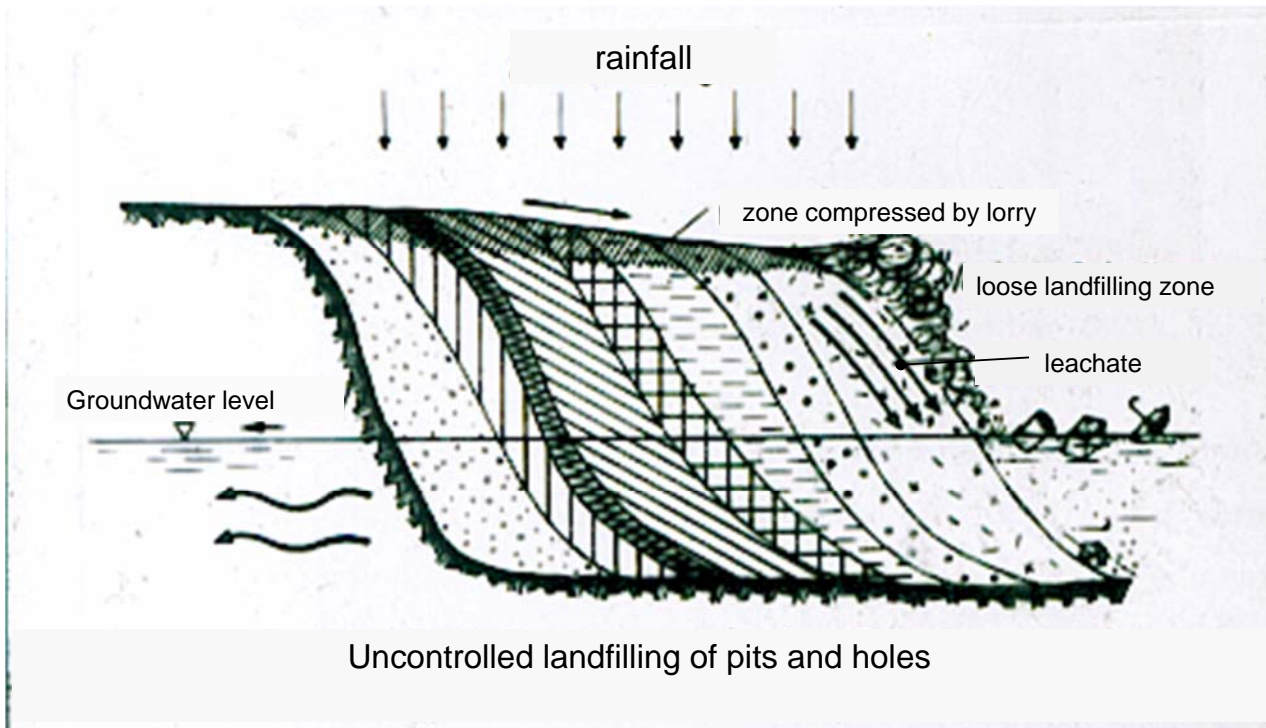
Without closing layer, drainage into the groundwater,

-> impact on the environment and the water supply

Dump site in Thuringia 1991



„Waste Swimming Pool“



Dump site in water body 1971 East Frisia



Unseparated MSW after 10 years in a landfill



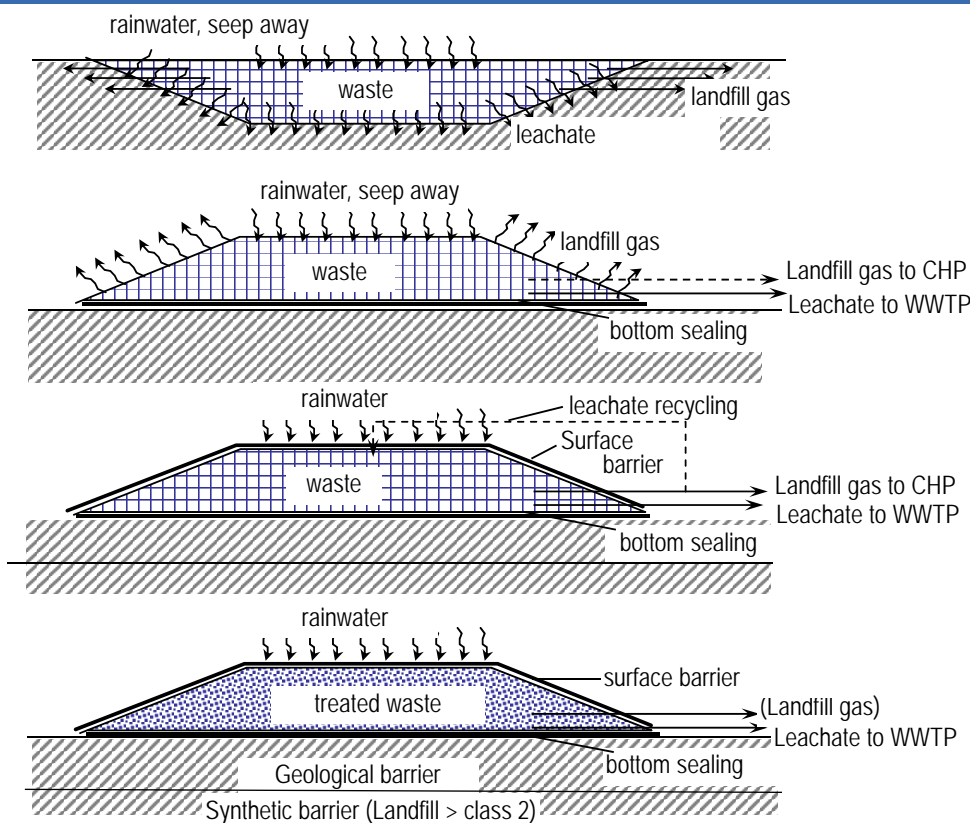
Newspapers after 10 Years in a Landfill



Strategies to Reduce or Prevent Landfill Emissions

- Purposeful inciting and temporal concentration of the reactions
 - **"Reactor Landfill "**: fixing of the water contents; leachate circulation
 - Elution = **"flushing bed reactor"**
 - **Aerobisation**
- Artificial barriers and architectural solutions
 - the enclosing of landfills is efficient only for a limited time, but necessary „forever“ if organic and elutable waste would be preserved in the landfill in a „dry rigour“.
- Compacting of elutable waste
- Waste barrier: only low-reactive or elutable waste → preliminary treatment

Development of the Landfilling Concepts in Germany



till 1970: predominantly open and uncontrolled disposal; often in holes or valleys

from 1970: bottom sealing; observation of leachate and gas emissions; start of landfill leachate treatment

from 1975: Development of landfill degassing

from 1980: surface barriers; disposal in stockpiles; „landfill reactor“ trials; minimization of gas and leachate emission

from ca. 1990/1993
ban of the disposal of untreated waste
– Incineration with slag recycling
– Mechanical+ Biological Treatment and Incineration of high caloric value

from 06/2005:
realization of the EU standard of treatment and only disposal of harmless remains

Definition according to §2 AbfAbIV - Waste Depositing Ordinance

- Landfill
Waste depositing plant for the dumping of waste on the earth' s surface (aboveground dumping site)
- Landfill section
Separately operated part of a landfill. Landfill sections are allowed to overlap only at acclivities
- Old Landfill
 - a. landfill under construction or in operation, or landfill section under construction or in operation, the construction and operation of which had been permitted as of 01.06.1993, or which were permissible according to § 35 of the Recycling Waste Management Law, and
 - b. landfills for the licensing of which the project approval procedure had been opened and made public as of 1. 6.1993.



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Definition according to §2 AbfAbIV - Waste Depositing Ordinance

- **Landfill Category I:**
Landfill for waste which contains very low organic ratios and for which leaching trials have shown only very low releases of pollutants.
- **Landfill Category II:**
Landfill for waste, including waste from mechanical-biological treatment, which contains a higher organic ratio than that which is permitted to be deposited on landfills of Category I and which in leaching trials release higher amounts of pollutants than that of Category I. Thus, for Category II the requirements on the landfill location and the landfill sealing are higher.



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Definition according to §2 DepV - Landfill Ordinance

- **Landfill of Category 0 (Landfill Category 0, LC 0):**

Aboveground landfills for waste which complies with the allocation values of Landfill Category 0 according to Appendix 3 (inert waste)

- **Landfill of Category I (Landfill Category I, LC I):**

Aboveground landfill according to § 2 No. 8 of the Waste Depositing Ordinance

- **Landfill of Category II (Landfill Category II, LC II):**

Aboveground landfill according to § 2 No. 9 of the Waste Depositing Ordinance.



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Definition according to §2 DepV - Landfill Ordinance

- **Landfill of Category III (Landfill Category III, LC III):**

Aboveground landfill for waste which has a higher ratio of pollutants than that which may be deposited on a landfill of Category II and which in the leaching trials showed a higher pollutant release than that of LC II. Thus, the requirements on the landfill construction and operation are higher than in LC II.

- **Landfill of Category IV (Landfill Category, LC IV):**

Underground landfill in which the waste is deposited completely enclosed in rock, either

- a.) in a mine with independent depositing areas which is constructed or planned separately from the mineral recovery areas, or
- b.) in a cavern.



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Multi-Barrier Concept

- According to Landfill Directive (DepV2009)
 - Qualification of location, underground, environmental conditions,
 - Multi barrier system
 - Safety assessment
- 5 Barriers
 - geological barrier
 - **waste barrier** (type, preliminary treatment, control; observation of allocation values)
 - artificial barrier (top, lateral, and bottom sealing)
 - disposal (leachate and gas)
 - operation (installation technology) and after-care

(TASi 1993, Waste Depositing Ordinance 2001 and Landfill Ordinance 2002 are replaced by Landfill Directive 2009, DepV 2009) - after 1.6.2005 only waste which observes the limit values is allowed to be deposited

Directive 1999/31/EU of the Council from April 26, 1999, on waste dumping ground (Landfill Directive), contains similar targets with considerably lesser requirements

Decision 2003/33/EU Determination of criteria and methods for the acceptance of waste on landfills according to § 16 Appendix II 1999/31/EU effective as of 16.07.2004

Diagram of the options provided in the Landfill Directive for the depositing of waste

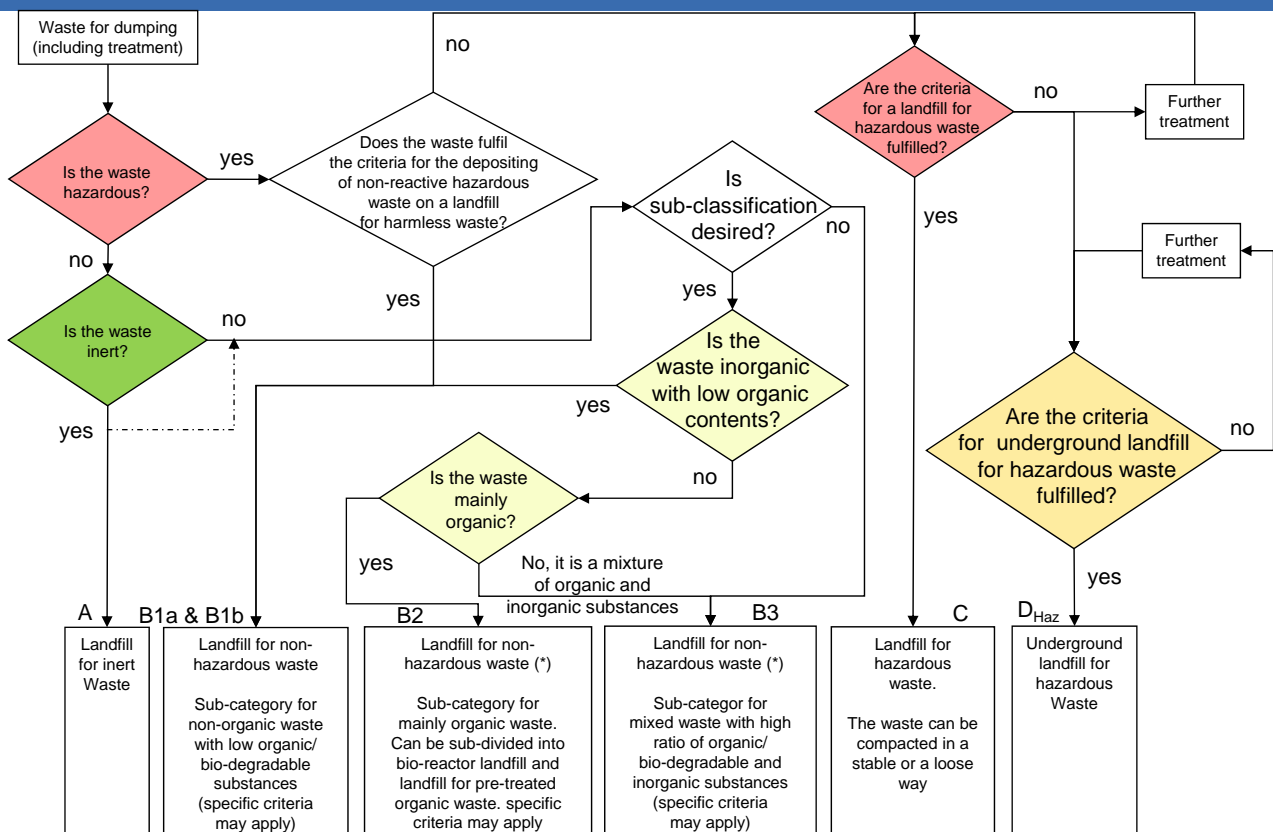


Table 1 from Appendix B of Decision 2003/33/EU Determination of criteria and methods for the acceptance of waste at landfills

Survey of the Landfill Categories and Examples of Sub-Categories

| Landfill Category | Main sub-categories (underground landfill, mono landfills and landfills for compacted, monolithic (*) waste which is acceptable for all landfill categories) | ID | Acceptance criteria |
|---|---|------------------|---|
| Inert waste landfill DK 0 | Landfill which accepts inert waste | A | Criteria for the leaching behaviour and for the contents of organic components have been determined on an EU level (Section 2.1). Criteria for the inorganic ratios can be determined on the member state level. |
| Landfill for non-hazardous waste DK I DK II | Landfill for inorganic, non-hazardous waste with low organic/bio-degradable contents, with the waste not fulfilling the criteria laid down in Section 2.2.2 for that inorganic non-hazardous waste which can be deposited together with stable non-reactive waste | B1a | Criteria for the leaching behaviour and criteria for the entire contents have not been determined on an EU level yet |
| | Landfill for inorganic, non-hazardous waste with low organic, bio-degradable contents | B1b | Criteria for the leaching behaviour and for the entire carbon contents (TOC) and other properties have been determined on an EU level; they apply for the grainy, non-hazardous waste and for the stable, non-reactive hazardous waste (Section 2.2). For the latter, the member states have to determine additional stability criteria. Criteria for monolithic waste must be agreed upon on the member state level. |
| | Landfill for organic, non-hazardous waste | B2 | Criteria for the leaching behaviour and criteria for the entire contents have not been determined on an EU level yet. |
| | Landfill for mixed non-haz. waste with high ratio of both organic/bio degradable & inorganic substances | B3 | Criteria for the leaching behaviour and criteria for the entire contents have not been determined on an EU level yet. |
| Landfill for hazardous waste DK III | Surface landfill for hazardous waste | C | Criteria for the leaching behaviour of granulated waste and criteria for the entire contents of some parts are determined on an EU level. Criteria for monolithic waste must be agreed upon on the member state level. More criteria for the content of haz. waste can be determined on the member state level. |
| DK IV | Underground landfill | D _{HAZ} | Particular requirements on EU level are listed in Appendix A. |

(*) Sub-categories for monolithic waste are only relevant for B1, C and D, possibly also for A



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Public Plants for Municipal Waste Disposal

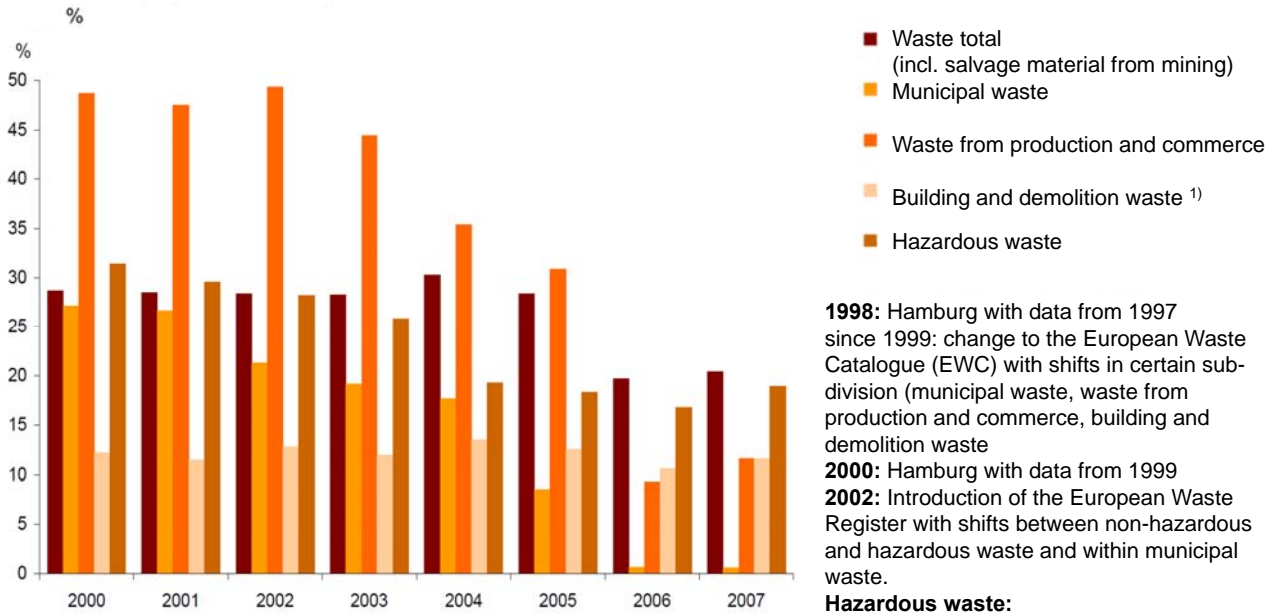
| Year | Plants for the disposal of municipal waste | | | | | | | | Reloading stations and collection points for commercial waste | | |
|-------|--|--------------------|--------------------|-------------------|--------------------|------------------|---------------------------------|-----------|---|--------------------------|----------------|
| | Total number | Landfills | | Thermal treatment | | Composting (MBT) | | together | Reloading stations | Collection points for CW | |
| | | Total Number/(MSW) | Weight ratio % MSW | Number | Weight ratio % MSW | Number | Weight ratio % | | | | |
| 1975 | 4616 | 4526 | | 83,1 | 47 | 13,5 | 21 | 1,1 | | | |
| 1977 | 2865 | 2756 | (1355) | 80,3 | 43 | 17,7 | 17 | 1,7 | 82 | 76 | 6 |
| 1980 | 3033 | 2918 | (530) | 79,1 | 44 | 19,2 | 16 | 1,4 | 110 | 106 | 4 |
| 1982 | 3176 | 3060 | (439) | 75,8 | 44 | 21,4 | 15 | 1,6 | 122 | 118 | 4 |
| 1984 | 3211 | 3118 | (385) | 73,3 | 46 | 24,3 | Composting only for utilization | | 136 | 127 | 9 |
| 1987 | 3220 | 3082 | (332) | 69,3 | 47 | 25,4 | | | 157 | 152 | 5 |
| 1990 | 3231 | 2874 | (290) | 69,8 | 50 | 22,8 | MBT prior to depositing | | 172 | 147 | 25 |
| 1990* | 7692 | 7314* | (2622) | 82,2 | 52 | 15,0 | | | 172 | 150 | 28 |
| 1993* | 3586 | 2948 | (550) | 69,6 | 56 | 21,3 | 10 | | 243 | 161 | 82 |
| 1998 | | 2341 | (350) | 62 | 60 | 33,7 | 25 | 3 | | Sorting plants | Demolition WEE |
| 2000 | | 2228 | (358) | | 64 | 38,2 | | | | | |
| 2005 | | 1948 | (162) | | 72 (155) | 41,2 | 1682+ (47) | (5,9) | | 897 | 313 |
| 2006 | | 1740 | | | (153+595) | | 1742+ (45) | | | 905 | 312 |
| 2007 | | 1706 | | | (157+589) | | 1793+(50) | | | 958 | 301 |
| 2008 | | 1645 | | | (158+632) | | 2041+(51) | | | 995 | 307 |
| 2009 | | 1553 | | | (160+633) | | 2047+(55) | | | 996 | 304 |
| 2010 | | 1165 | (94) | 21 | (163+644) | (≈ 25) | 1993+(54) | 7,8+(2,5) | | 1011 | 301 |



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Depositing Rates



Salvage material from mining is deposited at a 100%

Source: Federal Statistical Office, <http://www.destatis.de>, (State: August 2007); Federal Environment Agency, our own calculations

1998: Hamburg with data from 1997
since 1999: change to the European Waste Catalogue (EWC) with shifts in certain sub-division (municipal waste, waste from production and commerce, building and demolition waste)

2000: Hamburg with data from 1999

2002: Introduction of the European Waste Register with shifts between non-hazardous and hazardous waste and within municipal waste.

Hazardous waste:

since 2002, the waste which needs particular supervision is contained in the main streams.

¹⁾ Since 2004 without used amounts of excavation, building rubble and roadway rubble in public building and recultivation projects.

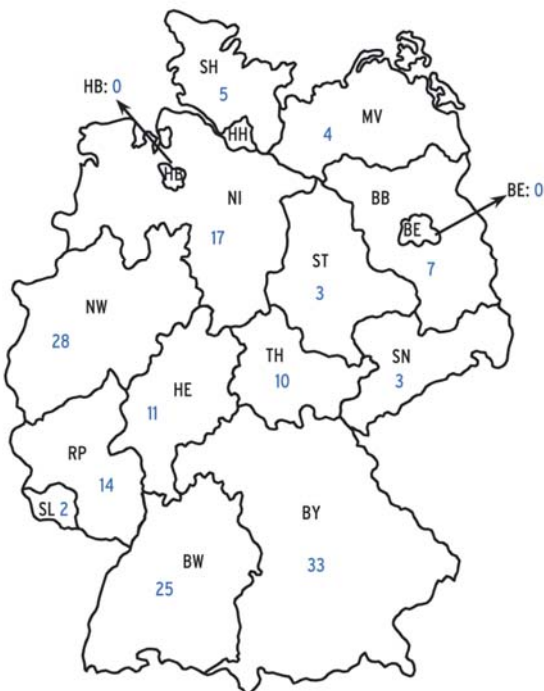


Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

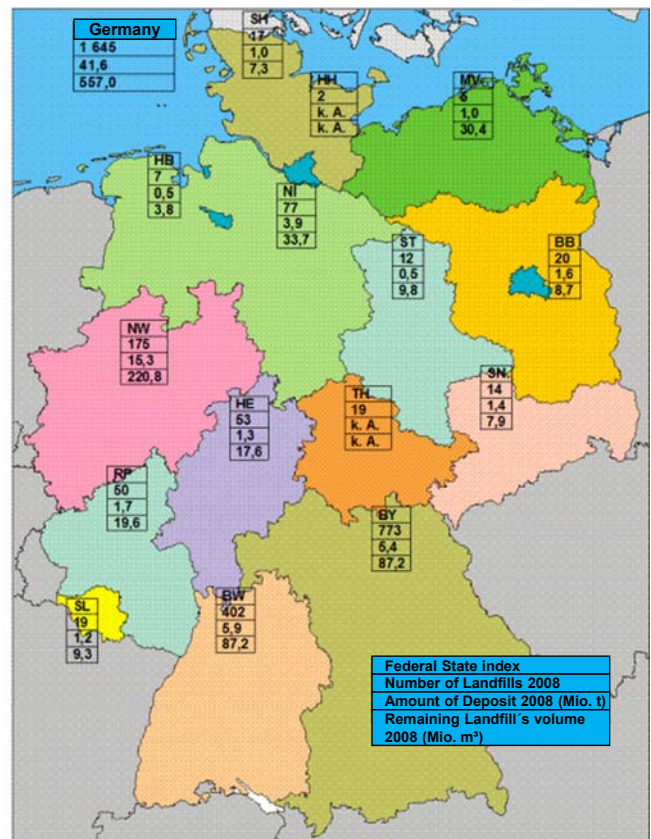
111
102
1004
Leibniz
Universität
Hannover

Distribution of Category II landfills (formerly: predominantl domestic waste landfills) among the federal lands

Total number: 162 Landfills of Category II (State: 6/2005)



Source: Federal Environment Agency – FEA; survey in the federal states, Jun 2005



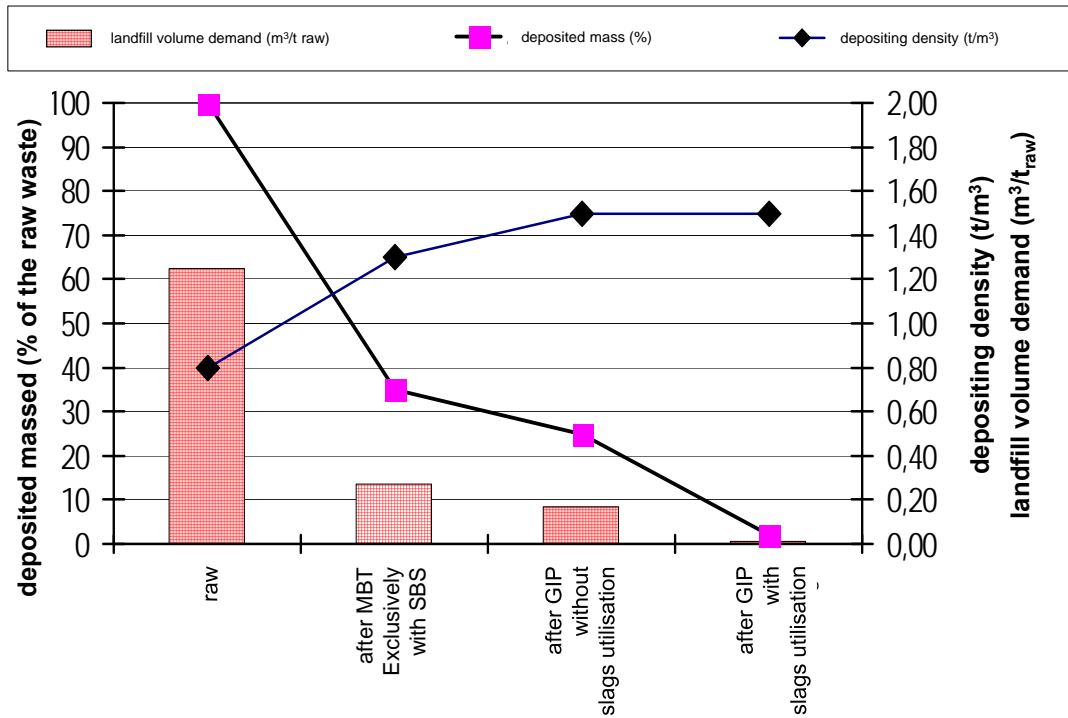
Source: Germany Federal Statistic Agency - 2010



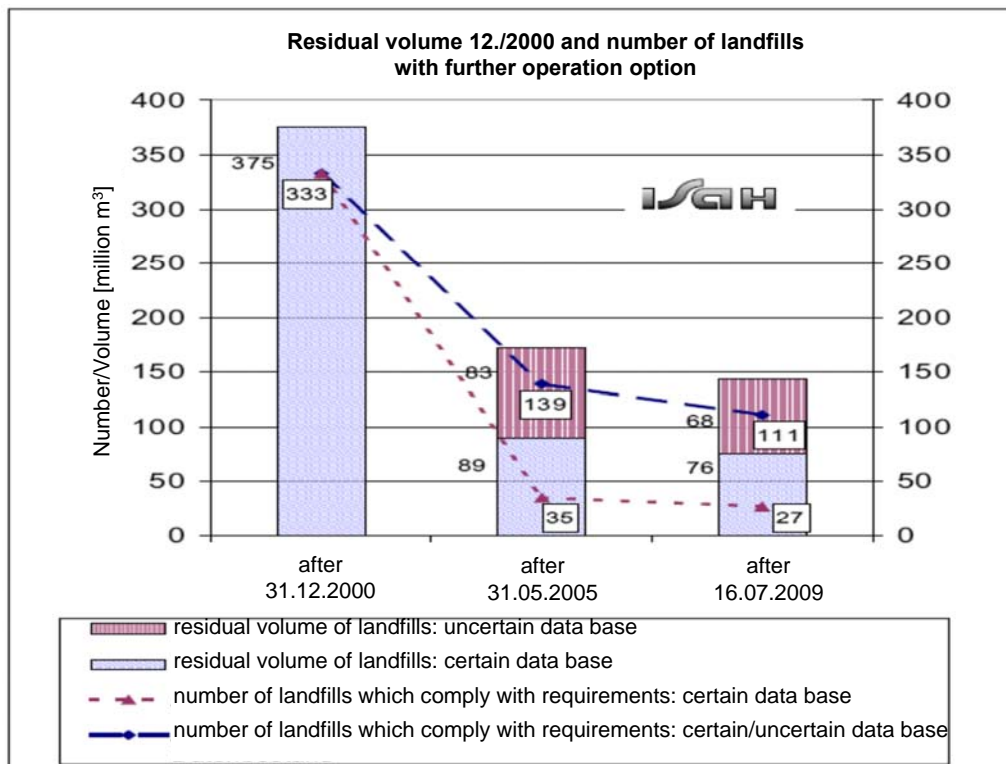
Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

111
102
1004
Leibniz
Universität
Hannover

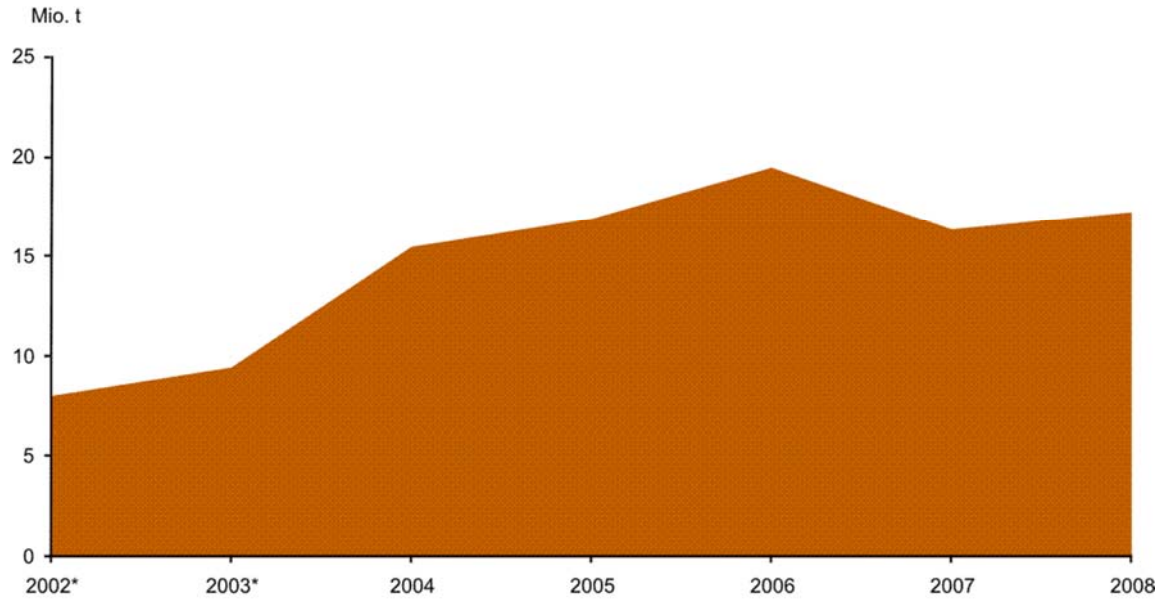
Landfill Volume Demand with Different Kinds of Preliminary Treatment



Residual volume 12./2000 and number of landfills with further operation option



Reuse of Waste on Landfills 2002 - 2008



* Einschließlich gefährlicher Abfälle, die nicht nach dem Begleitscheinsystem erfasst werden

* Incl. hazardous waste, which is not recorded with dispatch note

Source: Germany Federal Statistic Agency - 2010



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Tests for the Leaching Behaviour

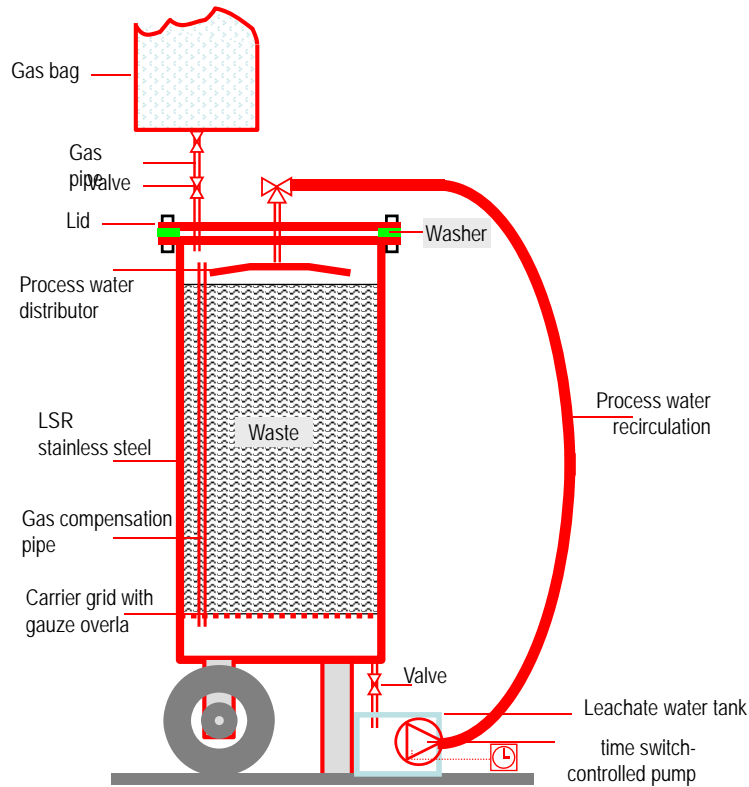
| Type of the tests | Waste sample weight kg | Water/ Solids - | Elution - | Waste | | Leaching rate m/a | Test period d or a | Temperature °C |
|--|---------------------------|-----------------------|--|---------|-------|----------------------|-----------------------|-------------------|
| | | | | at rest | moved | | | |
| DEV-Elution DIN 38014 S4; shaking test | ca. 0,1 | 10 | once | | X | - | 24 h | 20 |
| pH-Stat-Elution | ca. 0,1 - 0,2 | 10 | once | | X | - | 24 /48 h | 20 |
| Cascade elution test | ca. 0,1 - 0,2 | 5-30 | multiple | | X | - | | 20 |
| DSR; percolation column | 50-100 | 10-50 /a | multiple with ...bei SiW-recirculation | X | | 10-50 | ca. 100 - 1000 d | 35 |
| Lysimeter | | 1-2 | multiple with ...bei SiW-recirculation | X | | 1-5 | ca- 1 - 5 a | 20-35 |
| Open landfill trial field | | ca. 0,015 per a | once | X | | natural 0,1-0,5 | ca- 1 - 20 a | natural |



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Landfill Simulation Reactor (LSR)



Limit Values acc. to AbfAbIV, DepV and VersatzV

| No. | Parameter | | LC 0 | LC I | LC II Municipal waste App. 1 App. 2 | LC III hazardous waste | LC IV except Evaporate |
|------|--|-------------------------|-----------------------|-----------------------|---|------------------------------|------------------------------|
| 1 | Tensile Strength¹ | | | | | | |
| 1.01 | Lateral shearing strength | kN/m ² | ≥ 25 | ≥ 25 | ≥ 25 | ≥ 25 | |
| 1.02 | Axial deformation | % | ≤ 20 | ≤ 20 | ≤ 20 | ≤ 20 | |
| 1.03 | Mono-axial pressure resistance | kN/m ² | ≥ 50 | ≥ 50 | ≥ 50 | ≥ 50 | |
| 2 | Organic ratio of the dry residues of the original substance (OS) | | | | | | |
| 2.01 | determined as ignition loss | Mass % | ≤ 3 ²⁾³⁾⁴⁾ | ≤ 3 ²⁾³⁾⁴⁾ | ≤ 5 ²⁾³⁾⁴⁾ | ≤ 10 ²⁾³⁾ | ≤ 12 |
| 2.02 | determined as TOC | Mass % | ≤ 1 ²⁾³⁾ | ≤ 1 ²⁾³⁾ | ≤ 3 ²⁾³⁾ ≤ 18 ⁴⁾ | ≤ 6 ²⁾ | ≤ 6 |
| 3 | Extractable lipophile substances of the OS | Mass % | ≤ 0,1 | ≤ 0,4 | ≤ 0,8 | ≤ 4 ⁷⁾ | |
| 4 | Eluate criteria | | | | | | |
| 4.01 | pH-value | | 5,5 - 13 | 5,5 - 13,0 | 5,5 - 13,0 | 4-13 | 5,5 - 13 |
| 4.02 | Conductivity | µS/cm | ≤ 1.000 ⁸⁾ | ≤ 10.000 | ≤ 50.000 | ≤ 100.000 | ≤ 500 |
| 4.03 | TOC | mg/l | ≤ 5 | ≤ 20 ⁵⁾ | ≤ 100 ≤ 250 | ≤ 200 | ≤ 5 |
| 4.04 | Total phenol | mg/l | ≤ 0,05 | ≤ 0,2 | ≤ 50 | ≤ 100 | |
| 4.05 | Arsenic ⁹⁾ | mg/l | ≤ 0,04 | ≤ 0,2 | ≤ 0,5 | ≤ 1 | ≤ 0,010 |
| 4.06 | Lead ⁹⁾ | mg/l | ≤ 0,05 | ≤ 0,2 | ≤ 1 | ≤ 2 | ≤ 0,025 |
| 4.07 | Cadmium ⁹⁾ | mg/l | ≤ 0,004 | ≤ 0,05 | ≤ 0,1 | ≤ 0,5 | ≤ 0,005 |
| 4.08 | Chromium-VI ⁹⁾ | mg/l | ≤ 0,03 | ≤ 0,05 | ≤ 0,1 | ≤ 0,5 ¹⁰⁾ | ≤ 0,008 |
| 4.09 | Copper ⁹⁾ | mg/l | ≤ 0,15 | ≤ 1 | ≤ 5 | ≤ 10 | ≤ 0,05 |
| 4.10 | Nickel ⁹⁾ | mg/l | ≤ 0,04 | ≤ 0,2 | ≤ 1 | ≤ 2 | ≤ 0,05 |
| 4.11 | Mercur ⁹⁾ | mg/l | ≤ 0,001 | ≤ 0,005 | ≤ 0,02 | ≤ 0,1 | ≤ 0,001 |
| 4.12 | Zinc ⁹⁾ | mg/l | ≤ 0,3 | ≤ 2 | ≤ 5 | ≤ 10 | ≤ 0,5 |
| 4.13 | Fluoride | mg/l | ≤ 0,5 | ≤ 5 | ≤ 25 | ≤ 50 | |
| 4.14 | Ammonium-N | mg/l | ≤ 1 | ≤ 4 | ≤ 200 | ≤ 1.000 | |
| 4.15 | Cyanide, easily purgeable | mg/l | ≤ 0,01 | ≤ 0,1 | ≤ 0,5 | ≤ 1 | ≤ 0,01 |
| 4.16 | AOX | mg/l | ≤ 0,05 | ≤ 0,3 | ≤ 1,5 | ≤ 3 | |
| 4.17 | Water-soluble ratio (evaporation residue) | Masse-% | ≤ 1 | ≤ 3 | ≤ 6 | ≤ 10 | ≤ 3 |
| 5 | Biological degradability of the dry residue of the original substance | | | | | | |
| | Respiration activity (AT ₄) | mg O ₂ /g DM | | | | ≤ 5 | |
| | or gas production rate in the digestate (GB ₂₁) | NI/kg DM | | | | ≤ 20 | |
| 6 | Upper caloric value (H_u) | kJ/kg | | | | ≤ 6000 ⁹⁾ | |

- LC 0
aboveground landfill
for lowest-elutable
waste

- LC I
mostly unpolluted
waste

- LC II
low-polluted,
non-hazardous waste

- LC III
for hazardous waste

- LC IV
underground landfill
(ULF)

- Comprehensive selection out of all possible landfill sites of a disposal area (negative and positive mapping, site evaluation)
- Safety Distance to residential areas (TASi: 300 m)
- No sites in karst areas, subsidence areas caused by mining, flood plains, certain water protection areas
- Sites in pits only if leachate can be discharged outside by free gradient;
→ stockpile landfills;
→ no shafts in landfill
- For LCs II + III: Underground as geological barrier slightly permeable loose or solid rock with high pollutant retention potential ; for details, see picture. Alternatively, also architectural measures with a corresponding bottom layer.
- Surface of the landfill plain with compacting degree complying with Table 4 of the Prescriptions and Directives for Excavation Work in Road Construction (ZTVE). Distance of the landfill plain after settling: 1,00 m over the highest groundwater level.

Technical Barriers / Pollutant Transport

- Technical barriers as emission brakes
- For mineral sealing layers according to Holzlöhner et al.,1994

$$\frac{\partial(\Theta \cdot R \cdot c)}{\partial t} = \frac{\partial}{\partial x} \left[\underbrace{(\Theta \cdot d_0 \cdot \gamma + \alpha \cdot v)}_{\text{Diffusion Dispersion}} \frac{\partial c}{\partial x} - \underbrace{v \cdot c}_{\text{Advection}} \right] - \underbrace{\mu \cdot \Theta \cdot c}_{\text{Degradation}}$$

| | |
|----------------|---|
| R | = 1 + (ρ _d ·k _d) / Θ as retardation coefficient, which after the + sign considers the sorption |
| c | Concentration of the water-soluble substance (kg/m ³) |
| d ₀ | Diffusion coefficient of the water-soluble substance in the free water (m ² /s) |
| k _d | Coefficient of the linear equilibrium isotherm (distribution coefficient) (kg/m ³) |
| t | Time (s) |
| x | Longitudinal ordinate (m) |
| v | Filter velocity in x-direction (m/s) |
| α | Dispersion length (m) |
| γ | Impedance factor (-) |
| Θ | Water contents (m ³ /m ³) |
| μ | Degradation coefficient |
| ρ _d | Dry density of the depositing material (kg/m ³) |

- For plastic liners, diffusion according to Fick's 1st Law

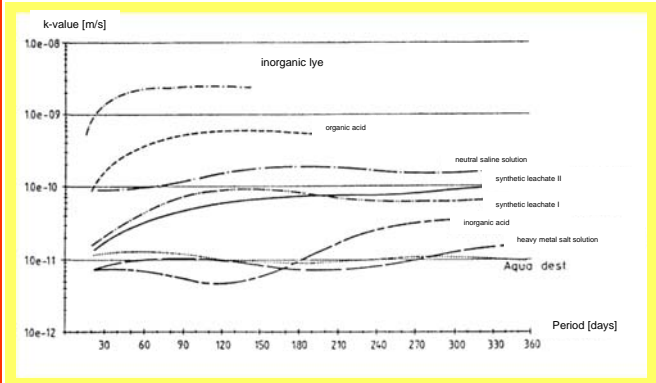
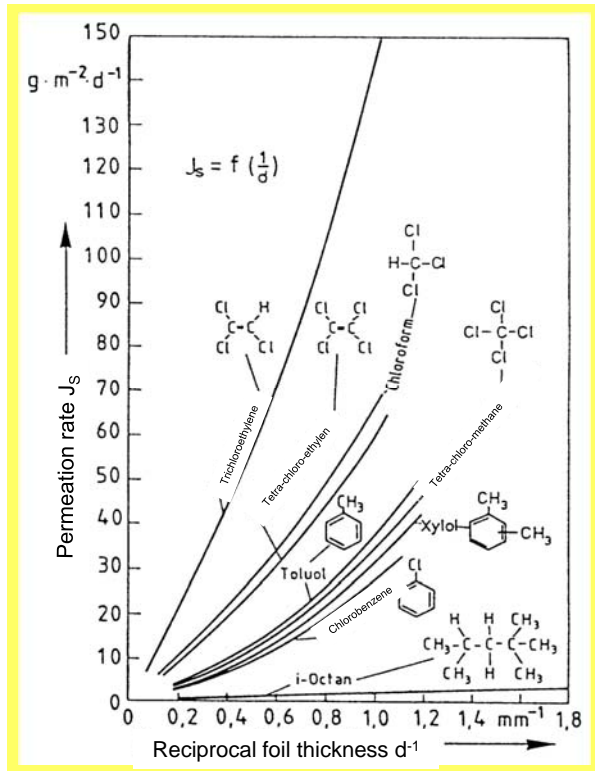


$$J_S \text{ (kg / m}^2 \cdot \text{s)} = \frac{d_0}{x} \cdot c$$

d₀ = Diffusion coefficient;
c = Concentration
x = Diffusions path; material thickness

- Plastic liners for salts and heavy metals are almost ideally leak-proof; for other components mineral sealings → Combination sealing for bottom and slopes

Permeation through Plastic Liners and Mineral Sealings



Standard Assembly of the Geological Barrier and the Bottom Sealing System

according to DepV

The permanent protection of soil and groundwater is to be achieved through the geological barrier according to No. 1.2 and a basis sealing system according to 1 Nos. 2-4 of Table 1. If two sealing components are necessary, the convection barrier (synthetic liner (geo-membrane) or asphalt liner) has to be set above the mineral component. The mineral components has to be multi-layered. All sealing components should be protected against load-caused damages.

| Nr | System Components | LC 0 | LC I | LC II | LC III |
|----|---|--|--|--|--|
| 1 | Geological barrier ^{1) 2)} | $k \leq 1 \cdot 10^{-7}$ m/s $d \geq 1,0$ m | $k \leq 1 \cdot 10^{-9}$ m/s $d \geq 1,0$ m | $k \leq 1 \cdot 10^{-9}$ m/s $d \geq 1,0$ m | $k \leq 1 \cdot 10^{-9}$ m/s $d \geq 5,0$ m |
| 2 | First sealing component ²⁾ | Not necessary | necessary | necessary | necessary |
| 3 | Second sealing component ²⁾ | Not necessary | Not necessary | necessary | Necessary |
| 4 | Mineral dewatering layer ³⁾ , granularity according DIN 19667 | $d \geq 0,3$ m | $d \geq 0,5$ m | $d \geq 0,5$ m | $d \geq 0,5$ m |

1) The permeability k must be kept at a pressure gradient of $i = 30$ (lab value).

2) If sealing components are made from mineral substances, a thickness of $d \geq 0,5$ m and a permeability of $k \leq 1 \cdot 10^{-9}$ m/s with pressure gradient of $i = 30$ should guaranteed. If plastic liner is used (HDP), the thickness should be $d \geq 2,5$ mm.

3) The responsible authority may on application of the landfill owner permit deviations in the layer thickness and granularity of the dewatering layers if it is proven that the hydraulic capacity will in the long term be sufficient to prevent any damming of water within the landfill body for LCs I, II and III.

In the closedown stage of the landfill or the landfill section, a surface sealing system must be constructed according to Table 2 or with equivalent system components or a combination of equivalent system components.

| Nr. | System Components | LC 0 | LC I | LC II | LC III |
|-----|---|---------------|------------------------------|------------------------------|------------------------------|
| 1 | Equalisation layer ¹⁾ | not necessary | If so ⁷ necessary | If so ⁷ necessary | If so ⁷ necessary |
| 2 | Gas filter layer ¹⁾ | not necessary | not necessary | If so ⁸ necessary | If so ⁸ necessary |
| 3 | First sealing component | not necessary | necessary ²⁾ | necessary ²⁾ | necessary ³⁾ |
| 4 | Second sealing component | not necessary | not necessary | necessary ²⁾ | necessary ³⁾ |
| 5 | Leak control system | not necessary | not necessary | not necessary | necessary |
| 6 | Dewatering layer ⁴⁾ $d \geq 0,3 \text{ m}; k \geq 1 \cdot 10^{-3} \text{ m/s}$, incline > 5 % | not necessary | necessary | necessary | necessary |
| 7 | Recultivation layer/ functional layer | necessary | necessary | necessary | necessary |

- 1) The equalisation layer can be used as gas filter layer too, if it fulfilled the function regarding gas permeability and thickness .
- 2) If mineral substances are used for the sealing component, the calculational permeability should be less than of mineral layer of $d = 50 \text{ cm}$ with $k \geq 1 \cdot 10^{-9} \text{ m/s}$ with pressure gradient of $i = 30$ and permanent water afflux of 30 cm. Deviant of clause 1 mineral sealing components can be used, which show a flux less than 20 mm/year as average over five years.
- 3) If mineral substances are used for the sealing component, the calculational permeability should be less than of a mineral layer of $d = 50 \text{ cm}$ with $k \geq 1 \cdot 10^{-10} \text{ m/s}$ with pressure gradient of $i = 30$ and permanent water afflux of 30 cm. Deviant of clause 1 mineral sealing components can be used, which show a flux less than 10 mm/year as average over five years. If plastic liner is used (i.e. HDPE), the thickness should be $d \geq 2,5 \text{ mm}$.
- 4) The responsible authority may permit deviations of the minimum thickness, permeability and inclination of the dewatering layer, if the hydraulic capability of the dewatering layer as well as the stability of the recultivation layer is ensured permanent.
- 5) Instead sealing component, dewatering layer and recultivation layer a recultivation layer designed as water balancing layer can be applied; if deviant to the requirements regarding number 2.3.1.1 cipher 3 the flux of the water balancing layer is no more than 20 mm/year.
- 6) Instead the second sealing component and the recultivation layer a recultivation layer designed as water balancing layer regarding number 2.3.1.1 can be applied. If the first seal component is carried out as a convection barrier, also a control system can be incorporated instead of the second seal component for the convection barrier. In this case has to be installed a second seal component or an equivalent systems direct under the convection barrier in the area from places at which the drainage water is collected and carried off. The clauses 1 to 3 are valid within the case of dumps or dump sections on which household waste, household waste similar trade waste, sewage sludge and other waste with high organic quantity were deposited, with the possible specification, that the dump operator carries or has carried out measures successfully according to §25 paragraph 4 to the acceleration of biological degradation processes and for the improvement of the long-time behaviour.
- 7) Requirement depend on number 2.3 clause 2.
- 8) Requirement depend on Appendix 5 number 7.

Recultivation layer

- **Thickness, material selection and vegetation being calculated according to the protection requirements of the system components beneath**
- **Least thickness 1 m**
- **usable field capacity $\geq 140 \text{ mm}$ (related to the total thickness)**
- **suitable vegetation**
 - **Protection of the surface from wind and water erosion**
 - **evapotranspiration as high as possible**
- **Material according to appendix 3 Nr. 2 (Allocation criteria)**
- **Drainage of grabbed water from the dewatering layer according to the water-legal rules**



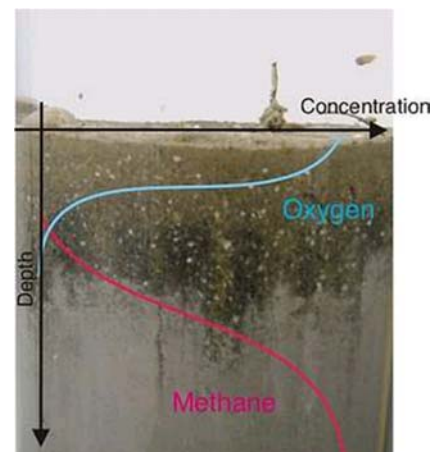
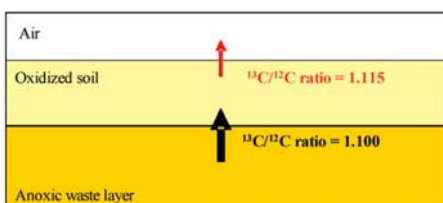
Water balancing layer

- least thickness 1,50 m
- usable field capacity of at least 220 mm (related to the total thickness)
- Percolation
 - at most 10 percent of the long-standing average of the fallout (generally 30 years),
 - at most 60 mm per annum, at the latest five years after construction
- Exception possibility of the usable field capacity near fallout-poor locations (less than 600 mm per annum), if it is proved by rise of the thickness that an equivalent sealing and protection effect is achieved.



Methane oxidation layer

“If the recultivation layer should take over tasks of a methane oxidation of residual gases at the same time, additional requests on the layer construction are to be agreed with the responsible authority. Interactions of the methane oxidation and the water balance of the recultivation layer are to be evaluated.”



Technical functional layer

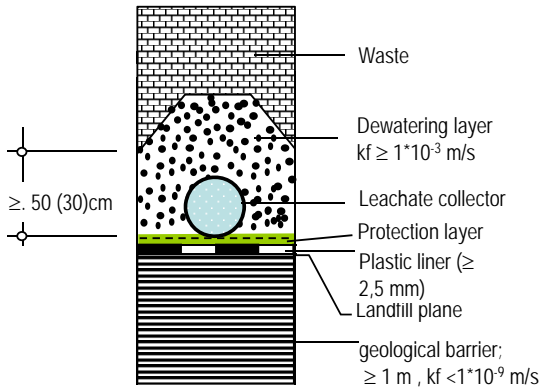
- Material with regard to pollutant content and leachability as at use outside of the landfill under comparable limiting conditions
- Thickness being calculated according to the protection requirements of the system components beneath
- Drainage of grabbed water from the dewatering layer according to the water-legal rules.
- Construction of the layer according the tasks of the technical functionality
 - to fulfill the natural function of the location and
 - to preserve the protection requirements of the system components beneath

Dewatering layer

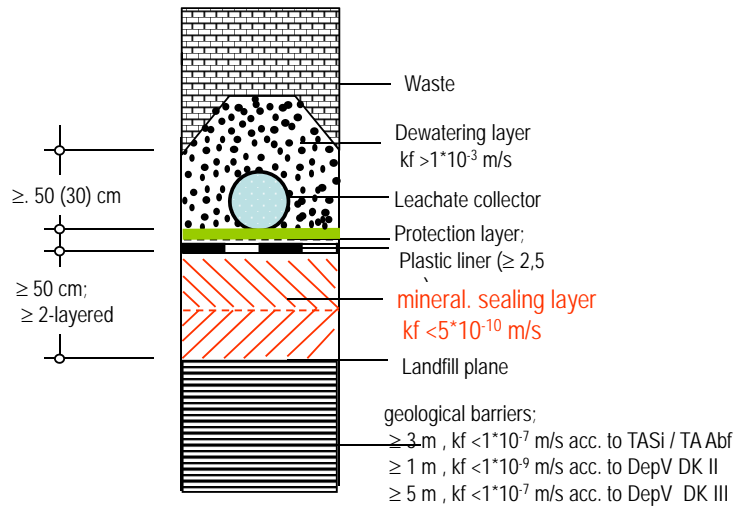
- Deviations allowed for
 - Least thickness, Permeability and Inclination
- Proofs
 - hydraulic efficiency of the drainage layer and
 - durable stability of recultivation layer



Landfill Bottom Sealing according to DepV (and TASI)

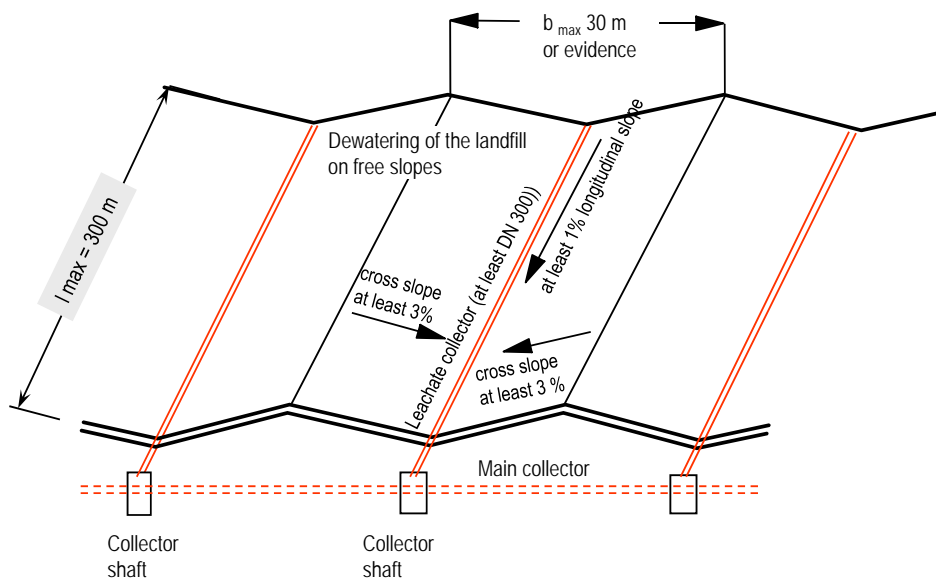


Bottom sealing
Landfill Category I



Bottom sealing
Landfill Categories II and III

Landfill Bottom and Dewatering according to TASI / DepV





Central Landfill Pohlsche Heide:

Plastic liner Carbofol® 2,5 mm thick and admitted by the authority was laid over the mineral sealing.

Secutex® protection fleece as protection against the 16/32 mm mineral layer.

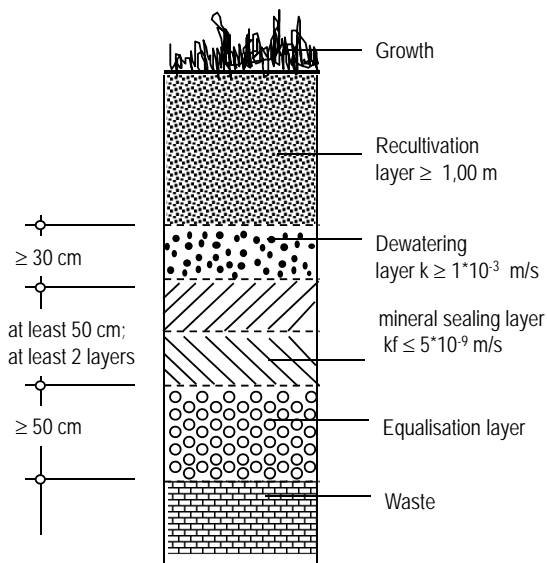


Regional landfill Lachengraben:

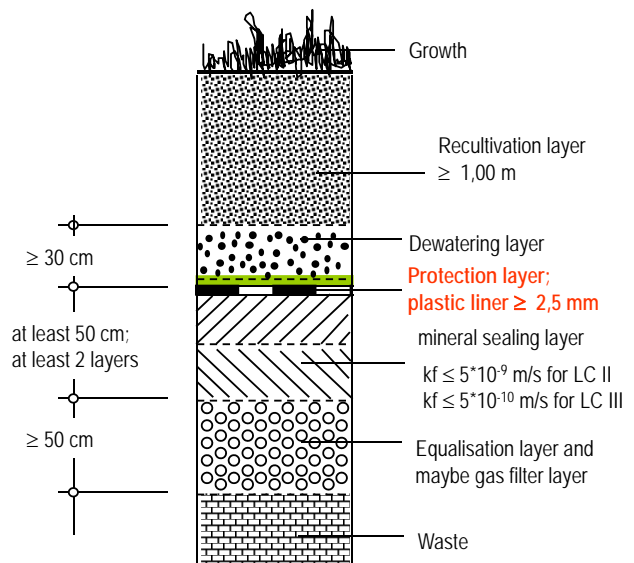
- asphalt bottom sealing 15.000 m²
- mineral sealing 20.000 m²
- landfill leachate tubes 1.100 m
- plastic liner 2.500 m²



Landfill Surface Sealing according to DepV



Surface sealing
LC I

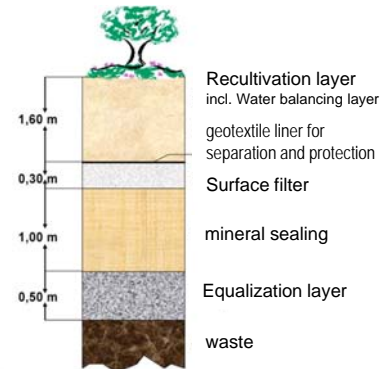


Surface sealing
LCs II and III

Construction of the surface sealing of landfill Ibbenbüren



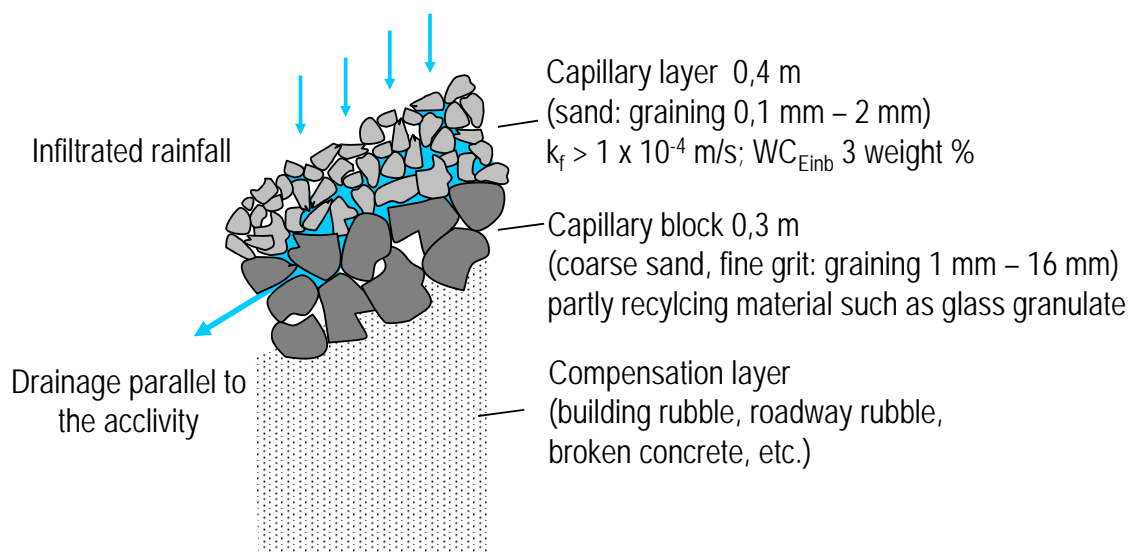
<http://www.egst.de/index.php>



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

1 1
1 0 2
1 0 0 4
Leibniz
Universität
Hannover

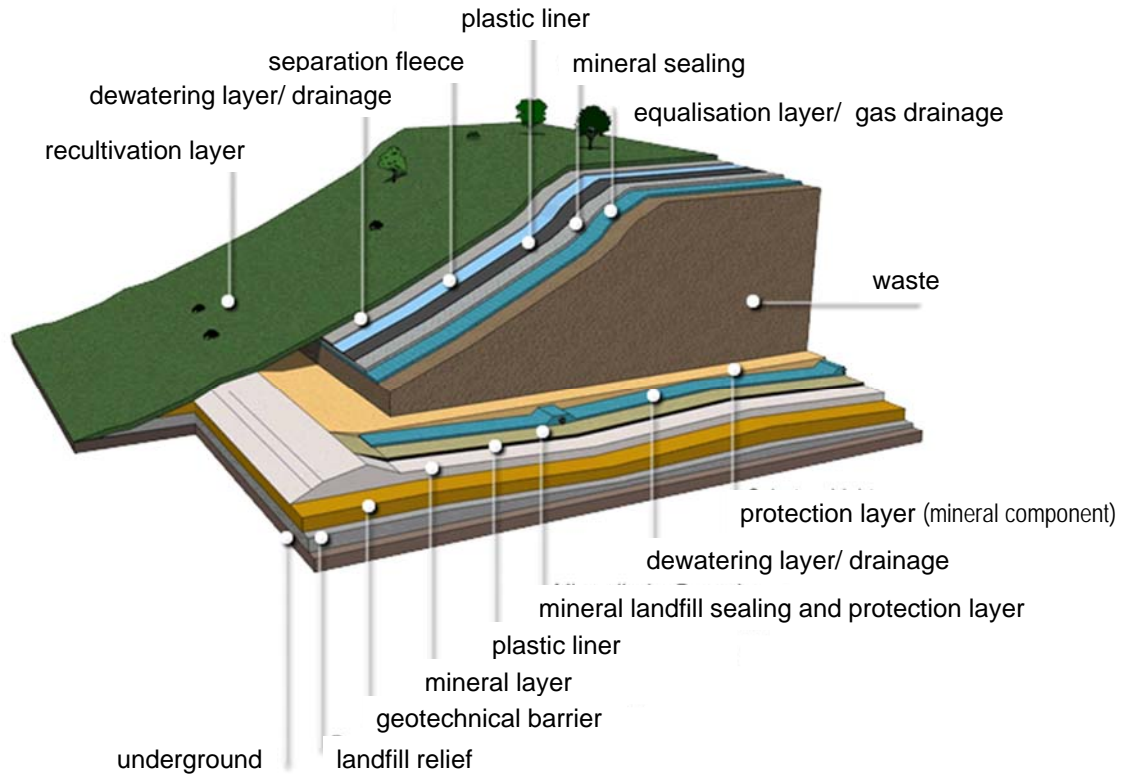
Dewatering Layer + Equalisation Layer



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

1 1
1 0 2
1 0 0 4
Leibniz
Universität
Hannover

sectional drawing of a landfill



Elements of Surface Sealing

- A: 0,06 m Landfill asphalt concrete sealing layer (DAD)
- B: 0,06 m Landfill asphalt concrete sealing layer (DAD)
- C: 0,08 m Landfill asphalt concrete base layer (DAT)

A: Hollow chamber contents < 3 volume %
Mineral material mixture with graining 0 – 11 mm
Filler < 0,09 mm between 12 and 16 weight %
Split > 2,00 mm between 40 and 55 weight %

20 mm Drainage mats(dewatering)
15 mm Bentonite mat
20 mm Drainage mats (degassing)

B: Hollow chamber contents < 3 volume %
Mineral material mixture with graining 0 – 11 mm
Filler < 0,09 mm between 12 and 16 weight %
Split > 2,00 mm between 40 and 55 weight %

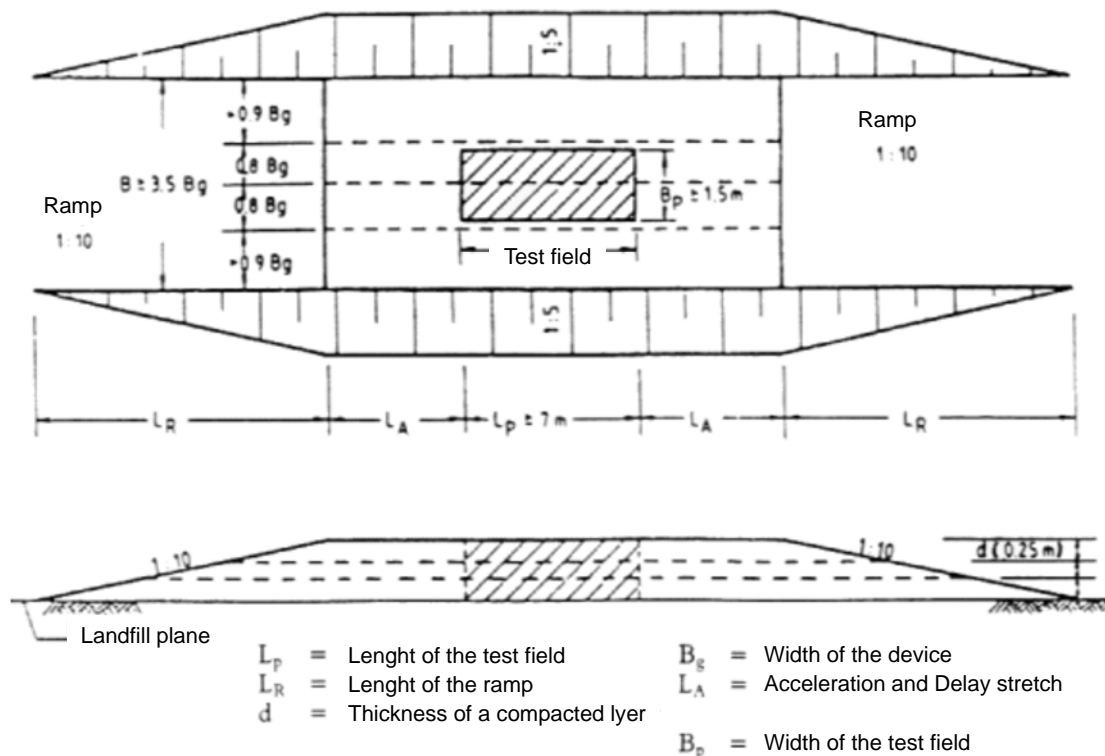
Trisoplast®
(89,1 % sand
10,7 % Bentonite
0,2 % Polymer)

C: Hollow chamber contents < 5 volume %
Mineral material mixture with graining 0 – 16 mm
Filler < 0,09 mm between 9 and 4 weight %
Split > 2,00 mm between 50 and 65 weight %

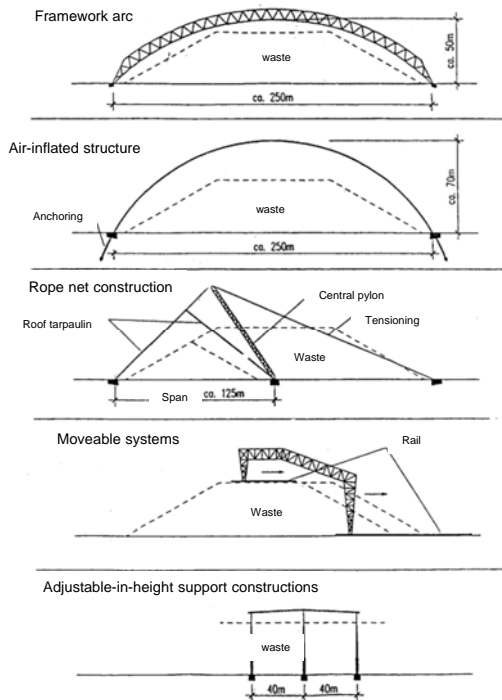
Additional Requirements on Landfill Sealings

| | |
|---|---|
| Bottom sealing (TASI 10.4.1.3) | <ul style="list-style-type: none"> Quality management plant according to DIN 55350; vertical permeation of the sealing not permissible for mineral sealing: <ul style="list-style-type: none"> clay ratio 10 weight %; organic substance ≤ 5 weight %; carbonate contents ≤ 15 weight %; built-in water contents above the Proctor water contents and $D_{pr} \geq 95\%$; evidence of the suitability through lab-tests and on an industrial scale through implementation of a trial field (cf. Foil). During execution: attention to the extensive prescriptions on quality management and approval. |
| Dewatering | <ul style="list-style-type: none"> After the subsiding of the settling, bottom with roof-shaped profile with cross slope $\geq 3\%$, longitudinal slope $\geq 1\%$; Trickling pipes according to DIN 19967, rinseable and controllable; perforated or slit on 2/3 of the circumference; reach length max. 300 m; hydraulic evidence on 6 l/s*ha; dewatering via a free gradient; shafts outside the landfill area or walk-in tunnels; pipe statics according to ATV Leaflet M127 |
| Dewatering layer | <ul style="list-style-type: none"> Preferably made of washed (round) grain and preferably within the particle size distribution curve range 16/32 mm |
| Surface sealing (TASI 10.4.1.4; TI Waste) | <ul style="list-style-type: none"> Cushion = equalisation layer $d \geq 0,50$ m of cohesion-less material; Maybe additional $d \geq 0,3$ m gas filter layer with CaCO_3 contents ≤ 10 weight % Roof-shaped; after subsiding of the settling cross slope $\geq 3\%$ and longitudinal slope $\geq 1\%$ Recultivation layer $d \geq 1,00$ m with arable soil; growth to minimise the infiltration of rainfall |

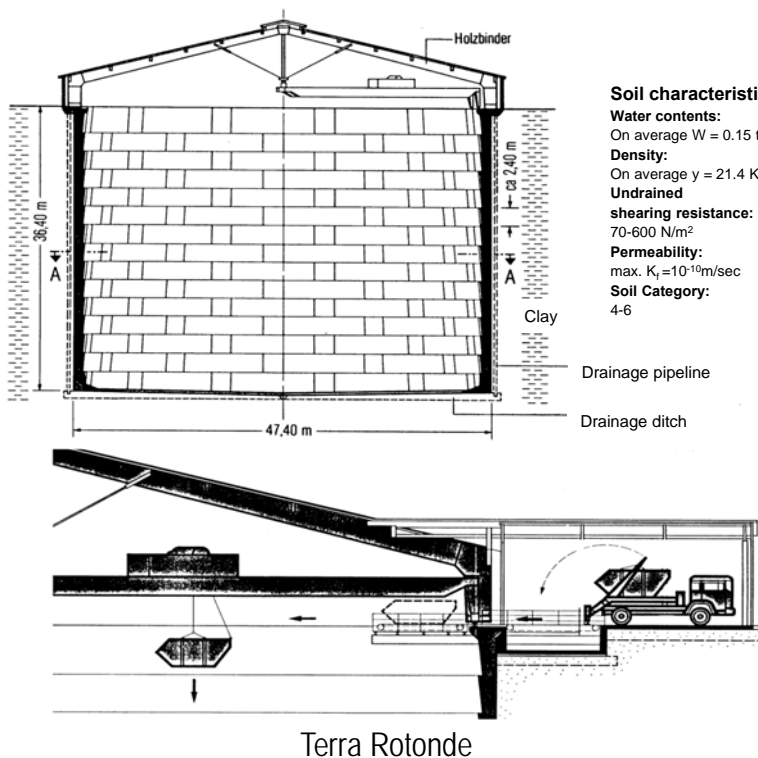
Test Field for minimum Sealing according to TI Waste, Part 1, Appendix E



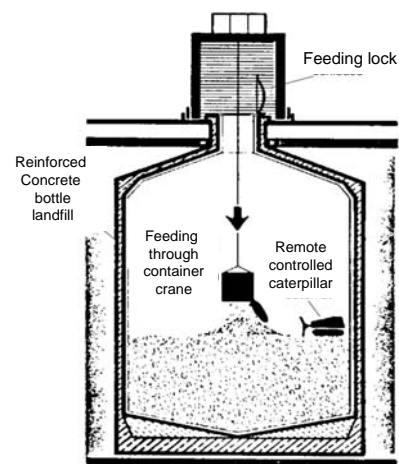
High Security Landfills – Indoor Depositing



High Security Landfills – Architectural Solutions

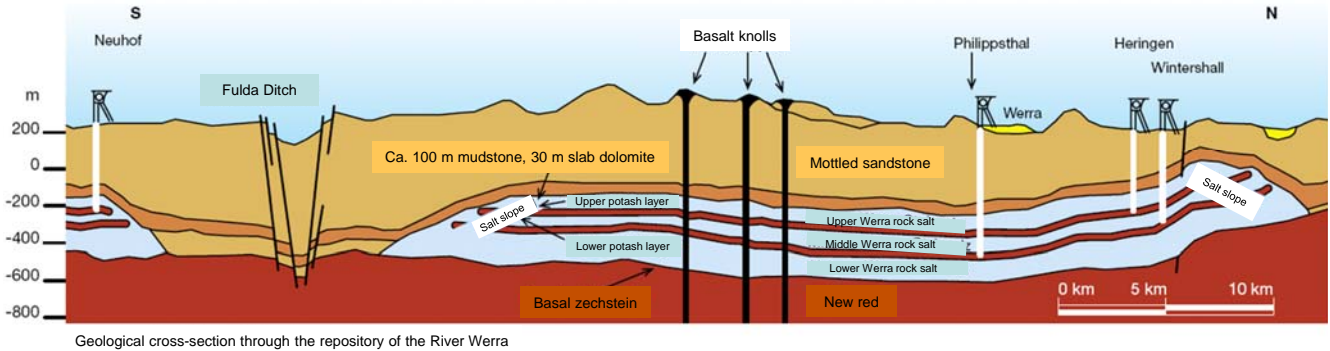


Soil characteristics:
Water contents:
 On average $W = 0.15$ to 0.17
Density:
 On average $\gamma = 21.4 \text{ KN/m}^3$
Undrained shearing resistance:
 $70-600 \text{ N/m}^2$
Permeability:
 max. $K_f = 10^{-10} \text{ m/sec}$
Soil Category:
 4-6



Bottle Landfill

UTD (Underground Landfill) in Herfa Neurode



Depositing Conditions for an UTD

Under depositing conditions, the waste must not be

- explosive
- self-igniting
- automatically combustible

If deposited, the waste must not

- Be prone to reactions which will entail autonomous degassing or gas production in the vessel

Waste must not

- have a pungent stench
- Be liquid, but have at least a semisolid consistency
- React in any hazardous way with the salt rock strata
- Grow in volume
- Be radioactive
- Contain or be able to bring forth pathogens of transmissible diseases
- Waste must be packaged in tightly sealed containers (barrels, containers or protective containers or Big Bags in a design which is harmless in regard to mining hygiene, dust-proof and flame-retardant).

PCB-contaminated transformers may be deposited without further packaging if the directives for hazardous goods have been observed.

Underground Landfill at Herfa-Neurode near Kassel



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

11
102
1004

Leibniz
Universität
Hannover

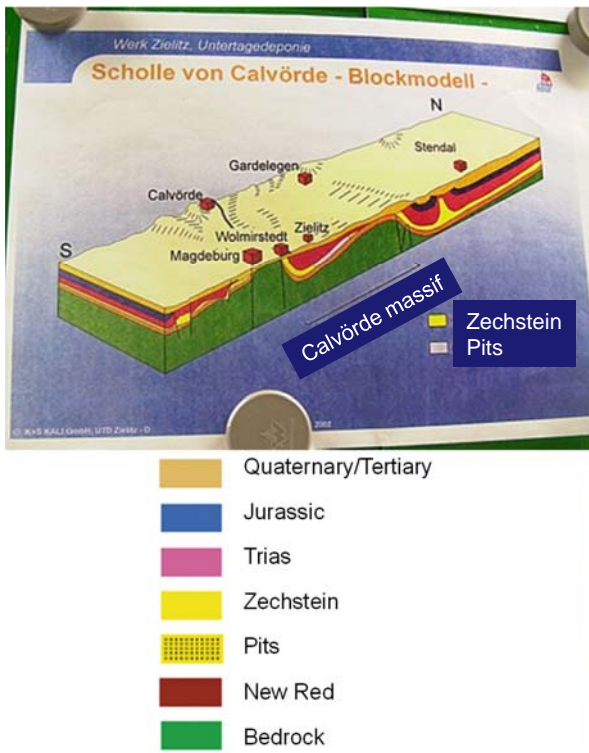
Filling at the Underground Landfill Herfa



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

11
102
1004

Leibniz
Universität
Hannover



Examples of Waste Types

- Residues from incineration plants for special waste and domestic waste
- Galvanisation residue
- Hardening salt residues
- Arsenical waste
- Chemical distillation residues
- Mercurial waste
- PCB-containing condensators/transformators
- Fluorescent lamp cullet
- Filtration and filter bed residues
- Contaminated soils and building rubble
- Evaporation residues from landfill leachate

Examples of Sectors:

- Combustion plants
- Metallurgical plants
- Metal processing industry
- Chemical industry
- Pharmaceutical industry
- Electrical industry
- Glass industry
- Lands and Municipalities
- Sanitation of abandoned polluted areas
- Waste Management Industry

Safety and Depositing Conditions

Ordinance on the underground depositing of waste, Stowing Ordinance as of 24. Jul 2002

- not explosive (under stowing conditions)
- not self-igniting (under stowing conditions)
- not automatically combustible (under stowing conditions)
- the waste must after depositing not incline to any reactions which would cause the autonomous degassing or gas production in the vessel
- the waste must not exude a pungent stench
- the waste must not be liquid and must at least have a semisolid texture
- the waste must not react with the rock salt strata in any hazardous way
- the waste must not grow in volume
- the waste must not be radioactive
- the waste must not contain or be able to generate pathogens or transmittable diseases
- the waste must be packed into tightly sealed repositories (dust-proof barrels, containers, or Big Bags with a low inflammability which comply with the requirements of mining hygiene). PCB-contaminated transformers can be deposited without further packaging if they comply with the requirements for hazardous goods.

Waste which does not fulfil these requirement must not be deposited.

In individual cases, one has to examine if the waste fulfils the conditions for the depositing on underground landfills (possibly after preliminary treatment).

The packaging must comply with the requirements for underground landfill depositing and the ADR/RID regulations. All repositories must be stored on palettes.



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Underground Landfill Zielitz & Herfa Neurode



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Water Balance of Landfills

- Water = **negative** as source of emissions;
positive as accelerator of the stabilisation
- Minimum water contents for degradation:

for aerobic processes:

suppressed from ca. <15 % water contents
 inhibited from ca. <30 % water contents and ca. >60 % water contents
 optimal ca. 40 - 60 % water contents

for anaerobic processes:

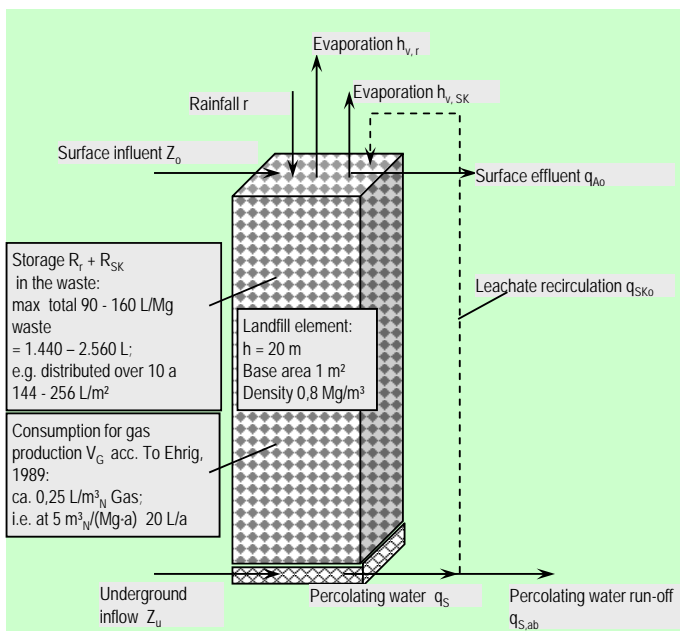
suppressed from ca. <15 % water contents
 inhibited from ca. <30 % water contents
 optimal ca. >40 % water contents

- As little leachate as possible,
but as much water as necessary for the residual stabilisation
- Water/solids ratio as measure for the stabilisation of a landfill

| Specific leachate amounts (m ³ /ha*d) | sealed areas (combined sealing) | | covered areas (sparse vegetation) | | Open operation areas with leachate recirculation without | | | | New open landfill sections without charging | |
|---|------------------------------------|---------|--------------------------------------|---------|---|---------|---------|---------|---|---------|
| | average | maximal | average | maximal | average | maximal | average | maximal | average | maximal |
| SUGGESTION | 1,5 | 3,5 | 7,5 | 20 | 7,5 | 15 | 10 | 40 | 20 | >50 |

Water Balance of a Landfill Element for Raw Municipal Waste

$$q_{S,ab} [m^3 / (ha \cdot a)] = r - h_{V,r} - h_{V,Sk} - \frac{M}{\rho_M \cdot A} \cdot (R_r + R_{Sk}) - V_G + Z_o - q_{A_o} + Z_u$$



$q_{S,ab}$ leachate contribution to be discharged in m³/(ha·a)
 r rainfall contribution in m³/(ha·a)
 $h_{V,r}$ evaporation of the rainfall in m³/(ha·a)
 $h_{V,Sk}$ evaporation from leachate recirculation in m³/(ha·a)
 M deposited waste amount in t/a
 ρ_M depositing thickness in t/m³
 A depositing area in ha

Influences on Leachate Amounts

- Storage potential of raw MSW is usable only once:
→ low initial leachate amounts
- On unsealed landfill areas, evaporation can considerably reduce the leachate amounts (according to, MHB 4623):

| Soil surface, Vegetation layer | TOTAL EVAPORATION | | EFFLUENT | |
|-----------------------------------|---------------------|--------|---------------------|--------|
| | (L/m ²) | % of N | (L/m ²) | % of N |
| Naked soil | 265 | 40 | 398 | 60 |
| Sparse vegetation | 345 | 52 | 318 | 48 |
| Field | 431 | 65 | 232 | 35 |
| Grass | 497 | 75 | 166 | 25 |
| Forest | 597 | 90 | 66 | 11 |

- Leachate recirculation on landfills with bio-degradable waste if
 - the leachate is low-odour
 - leachate storage capacity is available
 - the rainfall amount is low ≤ 5 mm/d
- Upper sealing/covering; if need be, secondary moistening for water consumption during degradation and moisture extracted with the landfill gas (ca. 35 l / Mg moist matter)

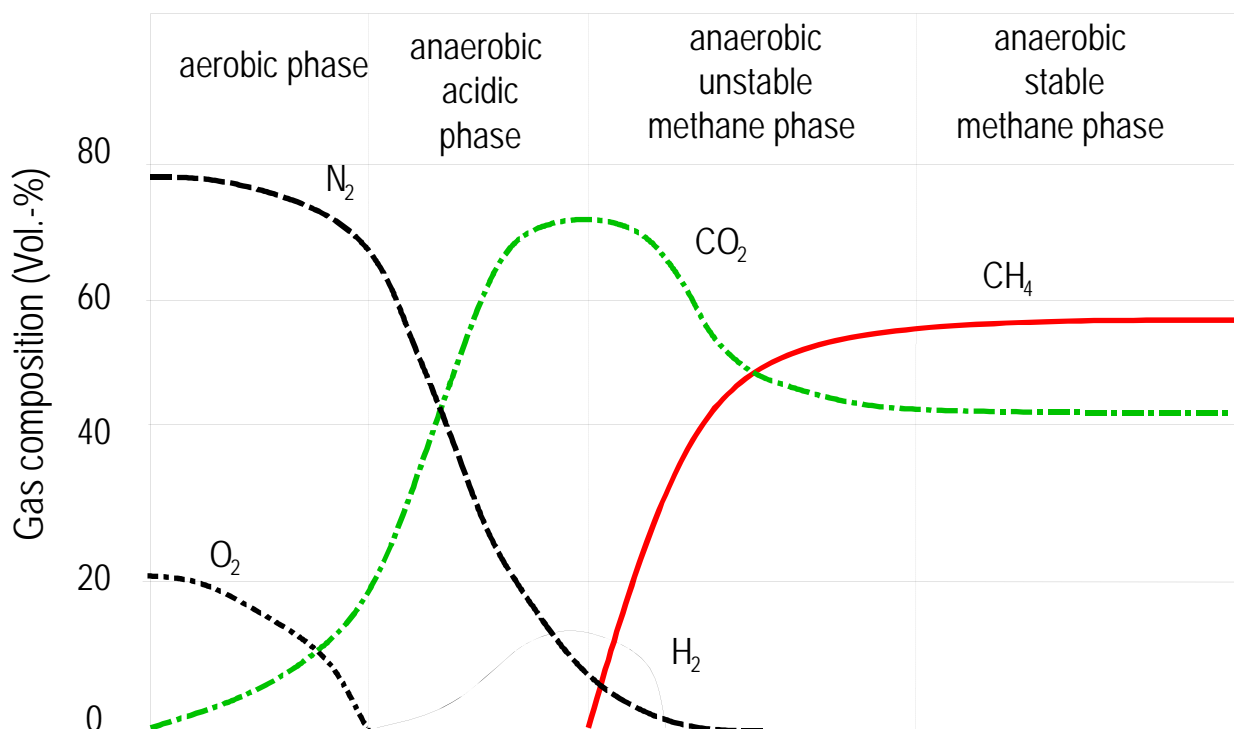
Leachate Quality

| | | Raw leachate concentrations from landfills for | | | | | | Discharge limit values Appendix 51 Direct discharge |
|---|----------------------|--|---------|---------------|---------|--|---|---|
| | | Raw municipal waste (EHRIG, 1986 and ATV, 1988) | | | | MBT-Output appendix 2 AbfAbIV DK II | waste acc. app 1 AbfAbIV DK II | |
| | | acidic phase | | methane phase | | | | |
| | | range | average | range | average | | | |
| pH | | 4,5 - 7,5 | 6,1 | 7,5 - 9 | 8 | | | |
| COD | mg O ₂ /l | 6.000-60.000 | 22.000 | 500-4.500 | 3.000 | 1.500 | < 1.000 | ≤200 at ≤ 4.000 raw or >95% at ≥ 4.000 |
| BOD ₅ | mg O ₂ /l | 4.000-40.000 | 13.000 | 20-550 | 180 | < 150 | < 100 | |
| SO ₄ | mg/l | 70-1.750 | 500 | 10-420 | 80 | | | |
| Zn | mg/l | 0,1-120 | 5 | 0,03-45 | 0,6 | | | ≤2,0 |
| Fe | mg/l | 20-2100 | 780 | 3-280 | 15 | | | |
| Parameter without significant changes (acidic/methane) | | | | | | | | |
| | | range | | average | | | | |
| NH ₄ -N | mg/l | 30-3.000 | | 1.500 | | 0-250 | ≤150 | |
| ΣN | mg/l | | | 1.500 | | | | ≤ 70 |
| Waste steam residue | mg/l | 10.000 | | 10.000 | | 10.000 | 500 - 30.000 | |
| Pb | mg/l | 0,008-1 | | 0,09 | | | | ≤0,5 |
| Cd | mg/l | 0,0005-0,140 | | 0,006 | | | | ≤0,1 |
| Cu | mg/l | 0,0044-1,4 | | 0,08 | | | | ≤0,5 |
| Ni | mg/l | 0,02-2 | | 0,2 | | | | ≤1,0 |
| Hg | mg/l | | | | | | | ≤0,05 |
| Cr | mg/l | 0,030-1,6 | | 0,3 | | | | ≤0,5 (CrVI ≤0,1) |
| AOX | mg/l | 0,3-3,3 | | 2 | | 0,1 - 1,5 | | ≤0,5 |
| GF | - | | | | | | | ≤2 |

Leachate Treatment

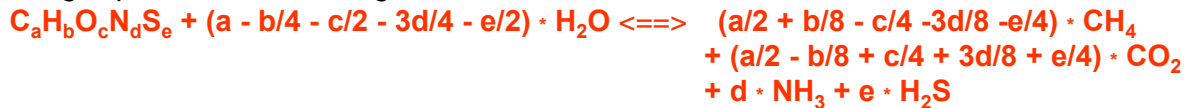
- Both for the indirect discharge into the public sewage system and for the direct discharge into bodies of water, the leachate must be treated on the landfill location.
- Limit values according Appendix 51 of the Wastewater Ordinance, particularly
 - (non-biodegradable) COD
 - N
 - AOX
 - (heavy metals)
- Lecture Prof. Rosenwinkel

Landfill Gas Composition according to Rovers, 1977 (Original Micrografx Picture) Micrograf bild



Landfill Gas Production from Organic Waste

- Bio-gas production according to BOYLE



- From the contents of, for instance, 200 kg C/t of moist waste, $200 \cdot 22,4/12 = 200 \cdot 1,868 = 373 \text{ m}^3$ gas /t waste would develop in case of complete C degradation, as CO_2 and CH_4 . The theoretical gas potential is practically never achieved and not completely collectable, either. The actually collectible landfill gas volume is:

- $G_{\text{collectible}} (\text{m}^3/\text{t}) = 1,868 \cdot \text{TOC} \cdot f_{\text{oa}} \cdot f_a \cdot f_o \cdot f_s$

- with **1,868** = m^3_n gas per kg TOC (m^3/kg) = $22,4 \text{ (L/Mol)}/12$ (atomic weight C)
- TOC = organic carbon contents kg/t of untreated moist waste, for instance

| | | | |
|--------------------------|---------|------------------|---------|
| Domestic waste | ca. 180 | Bulky waste | ca. 255 |
| Commercial waste | ca. 270 | Industrial waste | ca. 195 |
| Mixed construction waste | ca. 75 | Digested sludge | ca. 300 |
- f_{oa} = Initial time factor for the consideration of the gas production or conversion before depositing (e.g. also during preliminary treatment)
- f_a = Degradation factor as ratio of TOC gasifiable under optimal test conditions to total TOC (f_a 0,5 -0,9)



Gas Production (2)

- f_o = Optimisation factor as ratio of TOC gasified under practical landfill conditions to TOC gasified under optimal degradation test conditions ($f_o = 0,5 -0,9$; typically $f_a \cdot f_o = 0,5$ in humid climate)
- f_s = system-inherent capacity as ratio of the gas amount collected under landfill conditions with current degassing to the actually produced gas amount ($f_s = 0 -1,00$; high values with fast degassing start and upper combination sealing), also for losses at the beginning of a collection and after the end of a purposeful collection.
- Gas production – gas collection = gas loss
- With open or only covered landfills, a maximum of 50% of the produced gas amount will be collected also with suction operation (active degassing); the rest is emitted into the air.
- Gas production is time-dependent according to degradation kinetics, e. g. monomolecular reaction:

$$dc/dt = k \cdot c, \text{ or } c_t = c_o \cdot e^{-k \cdot t}$$
 - c_t Mass or concentration of degradable substances at point of time t;
 - c_o Mass or concentration of degradable substances at oint of time t = 0;
 - k Velocity coefficient
- Half-time $c_o / c_t = 2$
 - $\rightarrow t_H = \ln 2 / k = 0,693/ k$ or
 - $\rightarrow k = \ln 2 / t_H = 0,693/ t_H$



Gas Production (3)

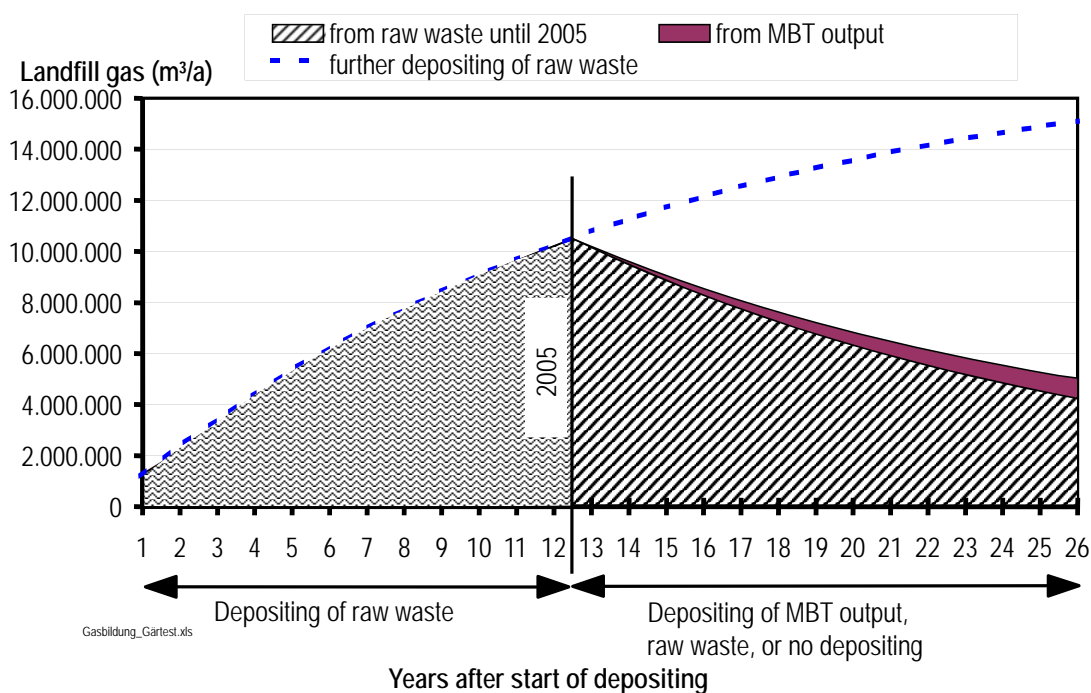
- Raw municipal waste with components with different degradation speeds, for instance
 - easily degradable (e.g. food leftovers, leaves, cut grass): half-life values 0,5 to 2 a
 - medium-heavily degradable (e.g. paper): half-life values 5 to 10 a
 - hardly degradable (e.g. books, cardboards, leather, wood, rags): half-life values 10 to 100 a
- Either for total waste 1 average k value, for instance for landfills with raw municipal waste $k = 0,05-0,15$; for digested sludge landfills $k = 0,01-0,03$, or for single types of waste differentiated values for f_a , TOC and k
- Collectible gas amount of a waste amount M (t) within t years after depositing:

$$G_{\text{collectible}} (\text{m}^3) = 1,868 \cdot M \cdot \text{TOC} \cdot f_{\text{ao}} \cdot f_a \cdot f_o \cdot f_s \cdot (1 - e^{-k \cdot t})$$
- or in year t after depositing

$$G_{t,\text{collectible}} (\text{m}^3/\text{a}) = 1,868 \cdot M \cdot \text{TOC} \cdot f_{\text{ao}} \cdot f_a \cdot f_o \cdot f_s \cdot k \cdot e^{-k \cdot t}$$
- Through MBT, about 40-60% of the oDM are degraded: thus – because not the entire oDM is degradable – gas production in the ensuing MBT landfill reduced by ca. 70-90% ($f_{\text{ao}} = 1 - (0,7 \text{ to } 0,9) = 0,3 \text{ to } 0,1$) compared to the raw waste landfill.
- Slags of thermal treatment after sufficient ageing without significant gas production

Gas Production over Time – Example for the Depositing of 100.000 Mg/a

Utilisation from 50 m³/h onwards (utilisation is mandatory)



Landfill Gas Components

| COMPONENT | | CONCENTRATION RANGE | |
|------------------------------|--|---------------------|-------------------|
| Methane | CH₄ | 0- 70 | Vol.-% |
| Carbon dioxide | CO₂ | 0- 50 | Vol.-% |
| Hydrogen | H ₂ | 0- 3 | Vol.-% |
| Oxygen | O ₂ | 0- 21 | Vol.-% |
| Nitrogen | N ₂ | 0- 78 | Vol.-% |
| Carbon monoxide | CO | 0- 3 | Vol.-% |
| Ammoniac | NH ₃ | 0-100 | Vol.-ppm |
| Ethene | C ₂ H ₄ | 0- 65 | Vol.-ppm |
| Ethane | C ₂ H ₆ | 0- 30 | Vol.-ppm |
| Acetaldehyde | CH ₃ CHO | 0-150 | Vol.-ppm |
| Acetone | C ₂ H ₆ CO | 0-100 | Vol.-ppm |
| other HCs, without aromatics | C ₂ -C ₁₁ | each 0- 50 | Vol.-ppm |
| Hydrosulphide | H ₂ S | 0-100 | Vol.-ppm |
| Ethyl mercaptan | C ₂ H ₅ SH | 0-120 | Vol.-ppm |
| Benzol, Toluol, Xylol | C _n H _m | 0- 15 | Vol.-ppm |
| HFC | C _w H _x Cl _y F _z | 0-600 | mg/m ³ |



Properties of Landfill Gas Components

- * from trace substances
- 1) at 0°C, 1013 mbar (according to KUCHLING, Taschenbuch der Physik, 1979)
 - 2) related to air = 1; composition of the air: 21% O₂; 78% N₂; 0,03% CO₂
 - 3) at 0°C, 1013 mbar, lower or upper explosion threshold
 - 4) dependent on the air dilution factor
 - 5) at 40% CO₂ ratio in the landfill gas

| Properties | | LANDFILL GAS COMPONENTS | | | | | | |
|------------------------------|--------------------|----------------------------|--------------------------------------|----------------------------|---|--------------------------|----------------------------|---|
| | | Methane CH ₄ | Carbon dioxide CO ₂ | Hydrogen H ₂ | Hydro- sulphide. H ₂ S | Carbon monoxide CO | Nitrogen N ₂ | Landfill gas with 60%CH ₄ and 40 % CO ₂ |
| Standard density 1) | kg/Nm ³ | 0,717 | 1,917 | 0,090 | 1,52 | 1,25 | 1,251 | 1,20 ⁵⁾ |
| relative density 2) | | 0,555 | 1,520 | 0,069 | 1,190 | 0,967 | 0,967 | 0,962 |
| Combustibility | - | yes | no | yes | yes | yes | no | yes |
| Explosiveness in air 3) | Vol.-% | 5-15 | no | 4-75,6 | 4,3-45,5 | 12,5-74 | no | yes 4) |
| Ignition temperature | °C | ≈ 650 | - | 560 | 270 | 605 | - | ≈ 650 |
| Smell | | no | no | no | yes | low | no | yes* |
| Toxicity | | no | yes | no | yes | yes | no | yes* |
| MAC value | Vol.-ppm | - | 5.000 | - | 10 | 50 | - | (12.500) ⁵⁾ |
| Caloric value H _u | kJ/Nm ³ | 35.790 | 0 | | | | | 21.582 |



Environment Pollution and Hazards Through Landfill Gas

| | Source | Emission path | Impact location | Effect | Measures |
|----|--|---------------------------|--|--|---|
| 1 | Original landfill gas | Landfill, soil, leak-ages | Shafts, cellars | Suffocation | Optimised gas collection; ventila-tion; compartment air measuring |
| 2 | Air-diluted landfill gas | like 1. | Shafts, cellars, closed rooms + vicinity | Danger of explo-sion | Ventilation; com-partment air control |
| | | - | Interior of the de-gassing imple-ments | Danger of explo-sion | active and passive explosion protec-tion |
| 3 | Gas migration | Soil | Covering soil, am-bient soil | Plant damages (displacement of air oxygen) | active degassing, maybe combined with (upper) seal-ing |
| 4a | Trace gases H ₂ S, CO, CFC | like 1. + 5 | like 1.-3. | Toxicity generally superposed by 1. | like 1.-3. |
| 4b | Carbon dioxide | like 1. + 5 | like 1.-3. | Toxicity, MAC 5‰ | like 1.-3. |
| 5 | Smell of the gas | Spreading in the air | Landfill vicinity | Annoyance through odours | active degassing, upper sealing |

Collection of Landfill Gas (1)

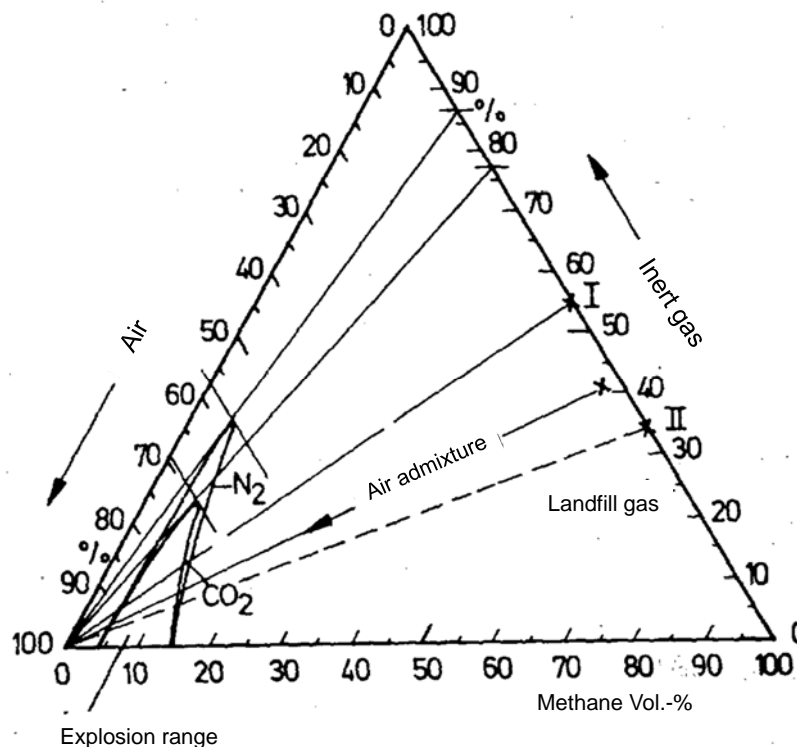
- Gas collection and utilisation are a necessary part of each landfill for raw municipal waste (otherwise emission problems, explosion risks; cf. Appendix C of TASI).
Greenhouse gas potential of methane is ca. 25 times higher than that of CO₂ → purposeful oxidation
Degassing actively (with low pressure), only on old landfills passively (through auto-overpressure)
Degassing of a charging field at the latest 6 months after the start of the depositing, to keep initial losses and emissions low (odour, greenhouse gas potential)
- Bottom leachate drain and leachate shafts must not be used for active degassing!
- Vertical gravel or rubble columns to be topped on the „waste cushion“ (10%-15% of the final column height, or 2,00 m) draining of the column; drainage pipe DN 200
- Drilled gas wells (on waste cushion); drainage pipe DN 200;
Telescope lengths for settling of 10%-20% of the entire waste depositing height

Collection of Landfill Gas (2)

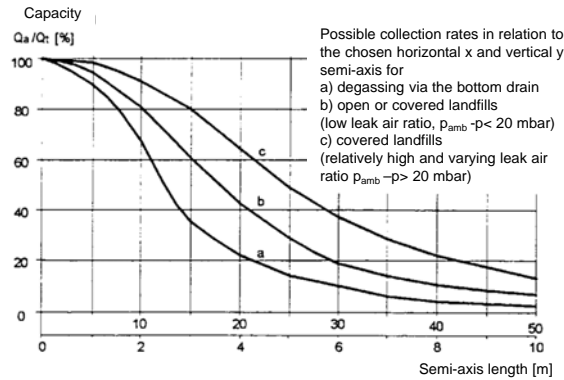
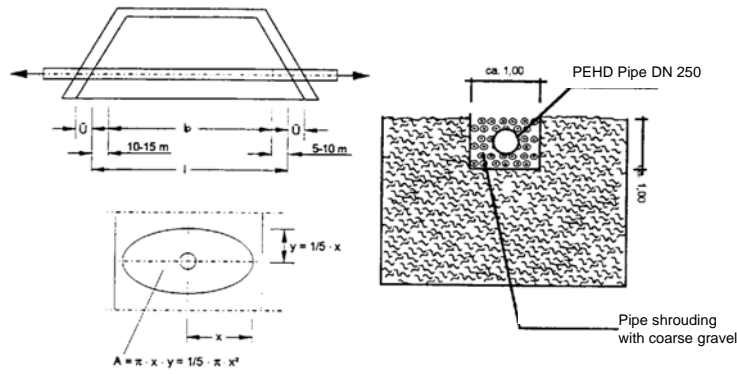
- Horizontal gas drainage layers (e.g. under surface sealing) 5% inclination
- Horizontal gas drainage ditches and pipelines
 - Initial inclination 7%; vertical drainage; pipes DN 250;
 - if exclusively horizontally: horizontal distance 30 m, vertical distance 5-10 m
- Gas pipelines
 - $DN \geq 100$; $v \leq 10$ m/s;
 - inclination underground $\geq 5\%$, aboveground $\geq 2,5\%$ (condensate production, prevention of „water bags“)
 - flexible pipeline connections (due to the settling of the landfill)
- Condensate from cooling of the water-saturated gas from, for instance, 40°C to 10°C should be separated, discharged, and treated like leachate

Explosion Triangle for Landfill Gas

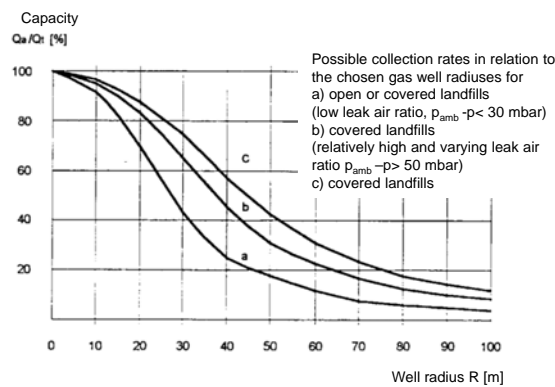
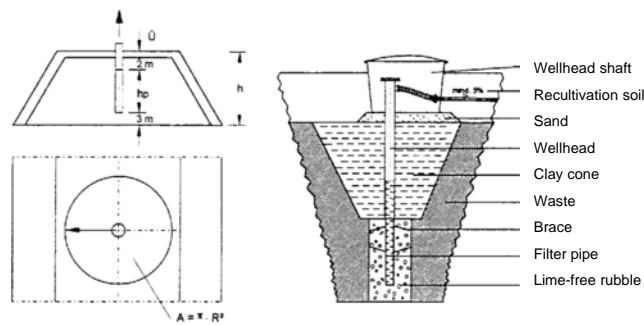
according to MÜLLER / RETTENBERGER (1986) "Gasabsauge- und Gasverwertungsanlagen an Mülldeponien" MFT/UBA, 183 S.



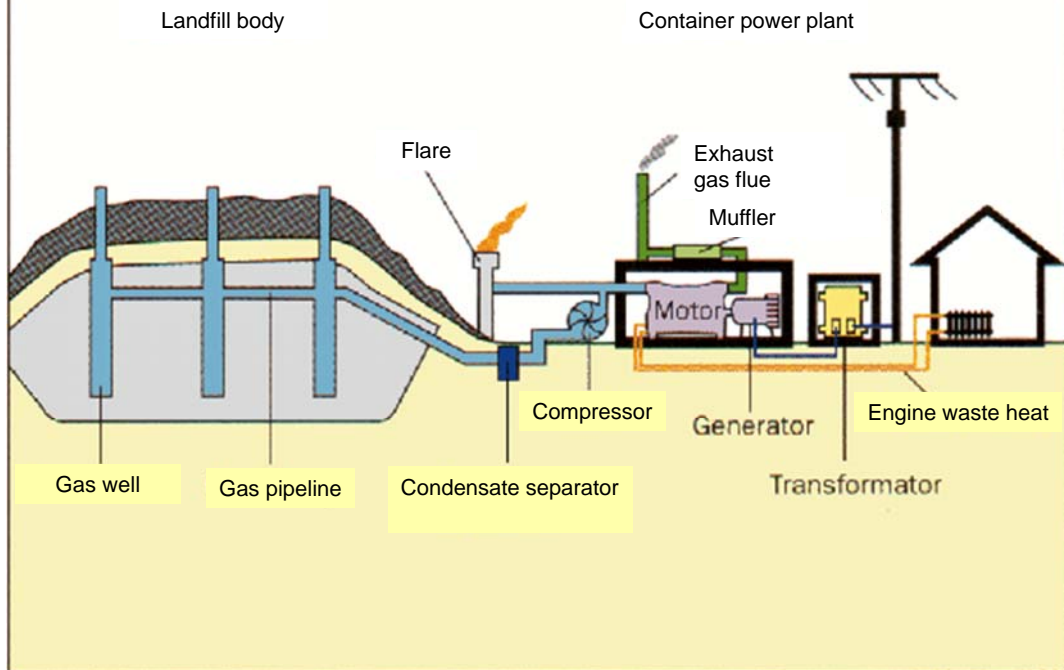
Horizontal Gas Collectors



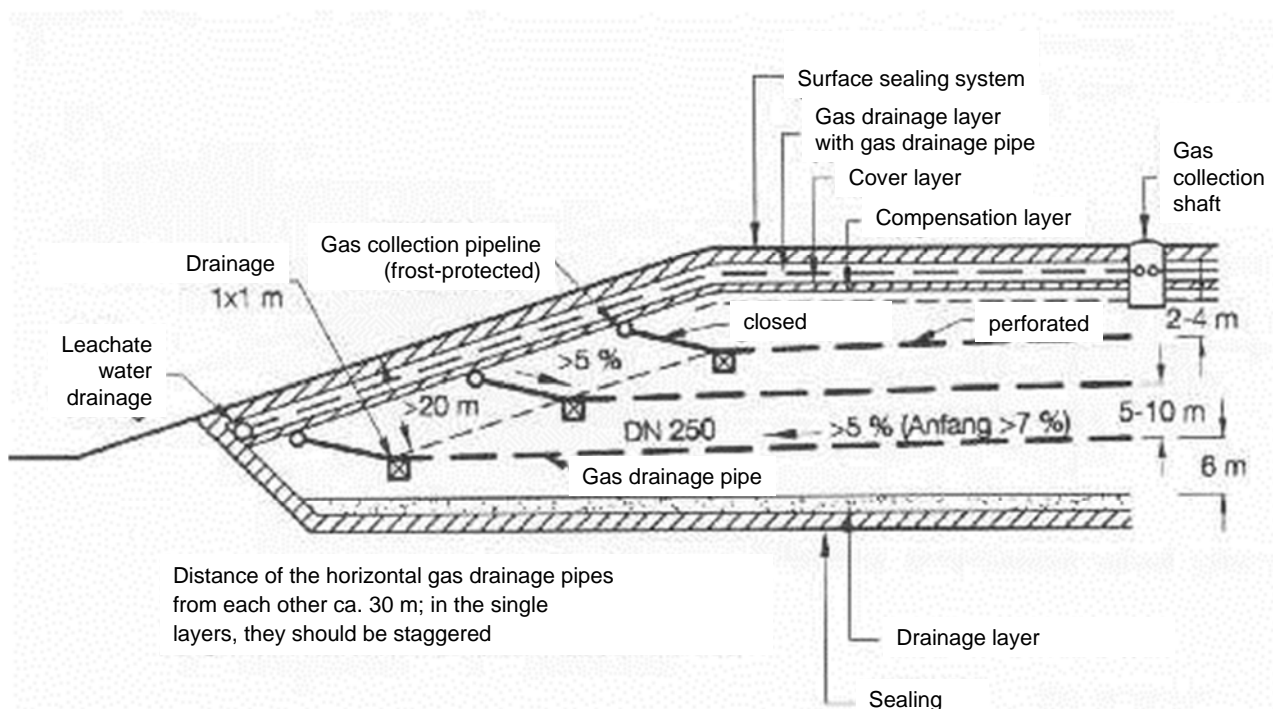
Vertical Gas Collectors



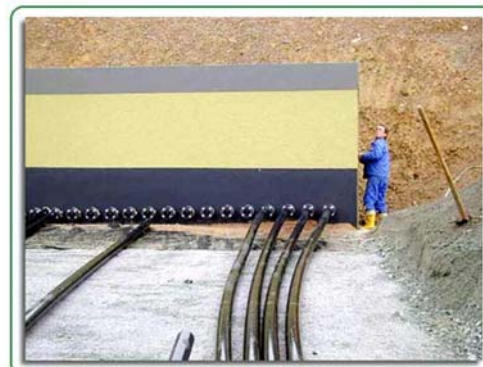
Electric Energy from Landfill Gas



Landfill Structure



Drilling of a Gas Well



Flexible Gas Well Connections



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Leibniz
Universität
Hannover

Landfill Gas Collection Station



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Leibniz
Universität
Hannover



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

11
102
1004
Leibniz
Universität
Hannover

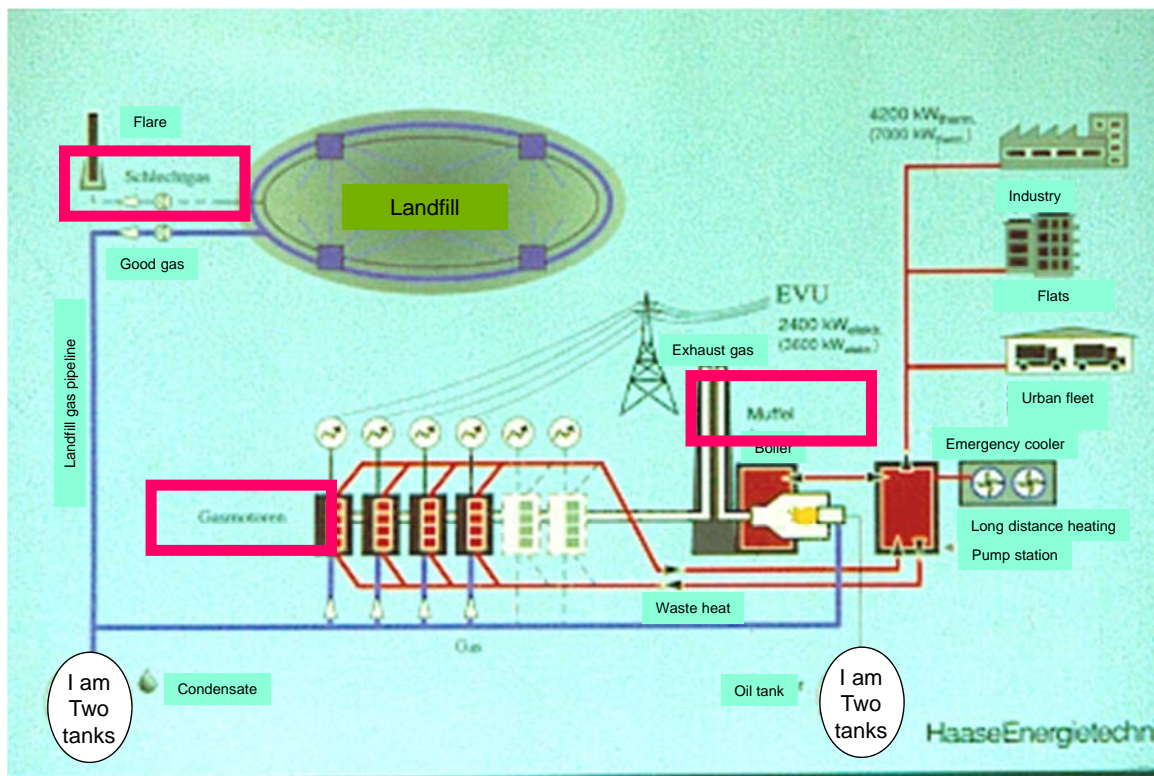


Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

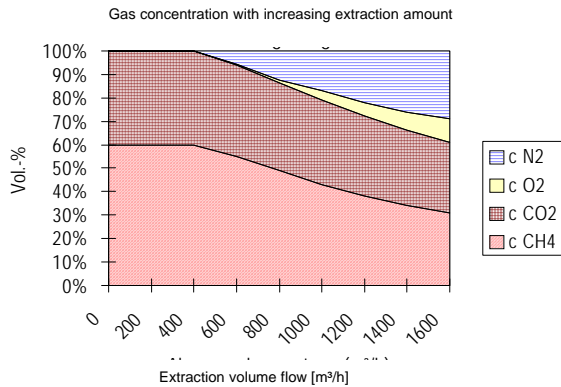
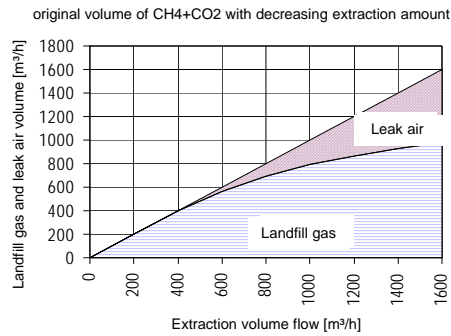
11
102
1004
Leibniz
Universität
Hannover



Landfill Gas Utilisatoin in Lübeck



Gas Concentration in Relation to the Extraction Volume Flow

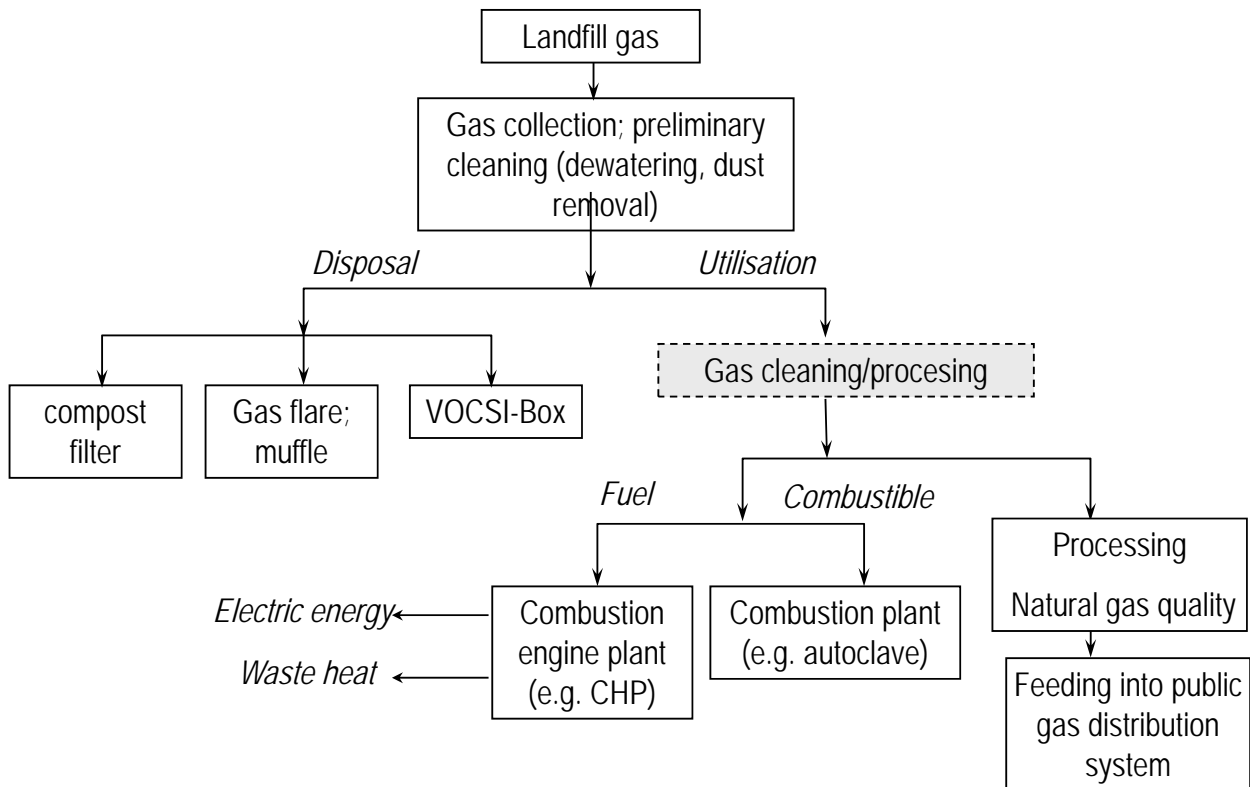


- Collection rate f_s often only up to 50 vol.-% of the produced landfill gas
- In case of excessive extraction:
 - Leak air
 - O₂ partly consumed for oxidation
 - O₂/N₂ ratio shifted from 0,26 (air)

Crucial Components of a Degassing Station

- pressure surge protected gas conveyance aggregate
- continuous (safety) analysis (CH₄, CO₂, O₂)
- Measuring technology (temperature, pressure)
- Aeration and ventilation
- safety fittings (valves, rapid action valves, deflagration implements, etc.)
- connecting pipeline
- electric technology including switching station
- building/containers with compartment air control

Disposal of Landfill Gas



Emission Limit Values for Landfill-Gas Driven Combustion Plants according to 1st BImSchV / TI Air

- 1) related to dry exhaust gas in the standard state at 5 Vol.-% O₂
- 2) related to dry exhaust gas in the standard state at 3 Vol.-% O₂
- 3) related to dry exhaust gas in the standard state at 15 Vol.-% O₂

| | Gas-Otto-Engine ¹⁾ (mg/m ³) | Combustion ²⁾ (mg/m ³) | Gas turbine ³⁾ (mg/m ³) |
|---|---|--|---|
| Dust | 5 | 5 | Smoke number <4 |
| Carbon monoxide | 650 | 100 | 100 |
| Nitrogen oxides (NO + NO ₂) measured as NO ₂ | 500 | 200 | 350 |
| Sulphurous oxides (SO ₂ + SO ₃) measured as SO ₂ | 500 | 500 | 500 |
| Inorganic chlorine compounds as gas of steam, measured as HCl | 30 | 30 | 30 |
| Inorganic fluoride compounds as steam or gas, measured as HF | 5 | 5 | 5 |
| Organic substances according to classi- fication | 20-150 | 20-150 | 20-150 |

Landfill Gas Flare and CHPs



Flare in Lübeck



Container-CHP in Borken



stationary CHPs in Mechernich 6x600 kW_{el}



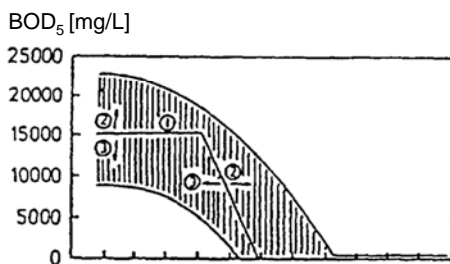
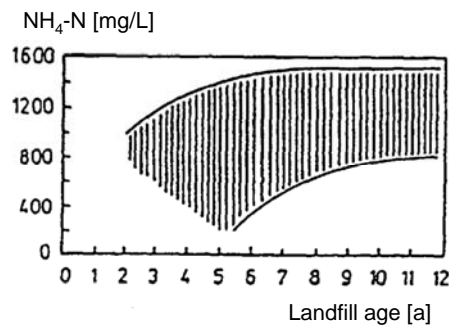
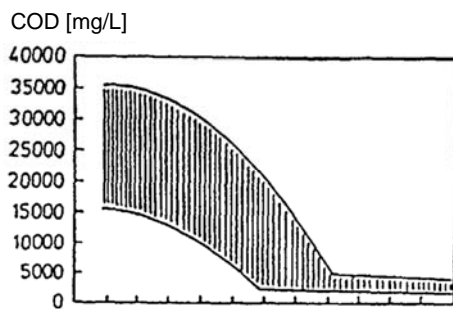
6,5 MW CHP in Seoul/South Korea



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

11
102
1004
Leibniz
Universität
Hannover

General Development of the COD, BOD₅ and NH₄-N Concentrations in Relation to the Landfill Age and the Landfill Operation



General development of the COD, BOD₅ and NH₄-N concentrations in relation to the landfill age
1 = average development with 2 m layers and 2-4 m build-up per year
2 = tendency with faster build-up
3 = tendency with slower build-up or recirculation



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

11
102
1004
Leibniz
Universität
Hannover

Requirements on the Effluent Quality

1. Minimum requirements according to the 51st Appendix of the Wastewater Ordinance (valid version of 1999) for direct and indirect dischargers as well as 23rd Appendix of the Waste Depositing Ordinance (2001), updated on 15.10.2002
2. additional requirements according to municipal sewage statutes for indirect discharge, which are often geared to the ATV Leaflet M 115,
3. more extensive requirements based on the situation of local receiving waters for direct discharge.



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Requirements on Wastewater for the Discharge Point

(Appendix 51 of the Wastewater Ordinance, 15.10.02)

| | | Qualified random sample or 2-hour mixed sample | Common concentration in the raw leachate |
|--|------|--|--|
| Chemical oxygen demand (COD) ¹⁾ | mg/L | 200 | 1.000 – 60.000 |
| Bio-chemical oxygen demand in 5 days (BOD ₅) | mg/L | 20 | 50 – 40.000 |
| Nitrogen, total, as sum of ammonium, nitrite, and nitrate nitrogen ²⁾ | mg/L | 70 | 400 – 4.000 |
| Phosphorous, total | mg/L | 3 | 0,01 – 1,0 |
| Hydrocarbons, total | mg/L | 10 | 200 – 30.000 (TOC) |
| Nitrogen from nitrite (NO ₂ -N) | mg/L | 2 | < 1 |
| Fish toxicity | mg/L | 2 | 8 - > 64 |

¹⁾ If it can be assumed that the contents of chemical oxygen demand (CDO) of a given wastewater amounts to more than 4,000 mg/l prior to treatment, there applies for the COD an effluent value of the qualified random sample or the 2-hour mixed sample which is equivalent to a reduction of the COD b at least 95%. The reduction refers to the ratio of the pollutant load in the influent of the wastewater treatment plant to that in the effluent of the WTP within 24 hours.

²⁾ The requirements on Nitrogen total applies for a wastewater temperature of 12°C or more in the effluent of the biological reactor of the wastewater treatment plant.



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe



Requirements on the Wastewater before Admixing

(Appendix 51 of the Wastewater Ordinance, 1999)

| | | Qualified random sample or 2-hour mixed sample | Common concentration in the raw leachate |
|--|------|--|--|
| Adsorbable organically bound halogenes (AOX) | µg/L | 500 | 500 – 5.000 |
| Mercury | µg/L | 50 | < 1 – 50 |
| Cadmium | µg/L | 100 | 0,5 - 140 |
| Chromium | µg/L | 500 | 30 – 1.600 |
| Chromium VI | µg/L | 100 | k. A. |
| Nickel | µg/L | 1.000 | 20 – 2.000 |
| Lead | µg/L | 500 | 10 – 1.000 |
| Copper | µg/L | 500 | 4 – 1.400 |
| Zinc | µg/L | 2.000 | 500 – 3.000 |
| Arsenic | µg/L | 100 | < 0,1 – 1.000 |
| Cyanide, easily releasable | µg/L | 200 | k. A. |
| Sulphide | µg/L | 1.000 | k. A. |



Solid Waste Management

Dr.-Ing. Dirk Weichgrebe



Leibniz
Universität
Hannover

Factors Influencing the Leachate Treatment Plants

The crucial parameters for the planning and realisation of leachate treatment plants are the **leachate amount** and the **leachate composition**.

Both dimensioning parameters are influenced by the following factors:

1. Waste composition:

- influenced by separate resource collection, pre-sorting, preliminary treatment and residual waste treatment

2. Landfill operation:

- Filling of the waste (thin layer filling or fast build-up of single landfill sections; intermediate covers)
- integration of an "aerobic" bottom layer of pre-rotted domestic waste in order to reduce the concentration peaks of organic components (see also WEBER, 1990)
- management of the closed areas and operation surfaces

3. Leachate management:

- storage to compensate amounts and concentrations,
- leachate recirculation (optimal water contents)
- strict separation of unpolluted surface water and leachate

4. Meteorological conditions:

- rainfall volumes, rainfall distribution, general weather data



Solid Waste Management

Dr.-Ing. Dirk Weichgrebe



Leibniz
Universität
Hannover

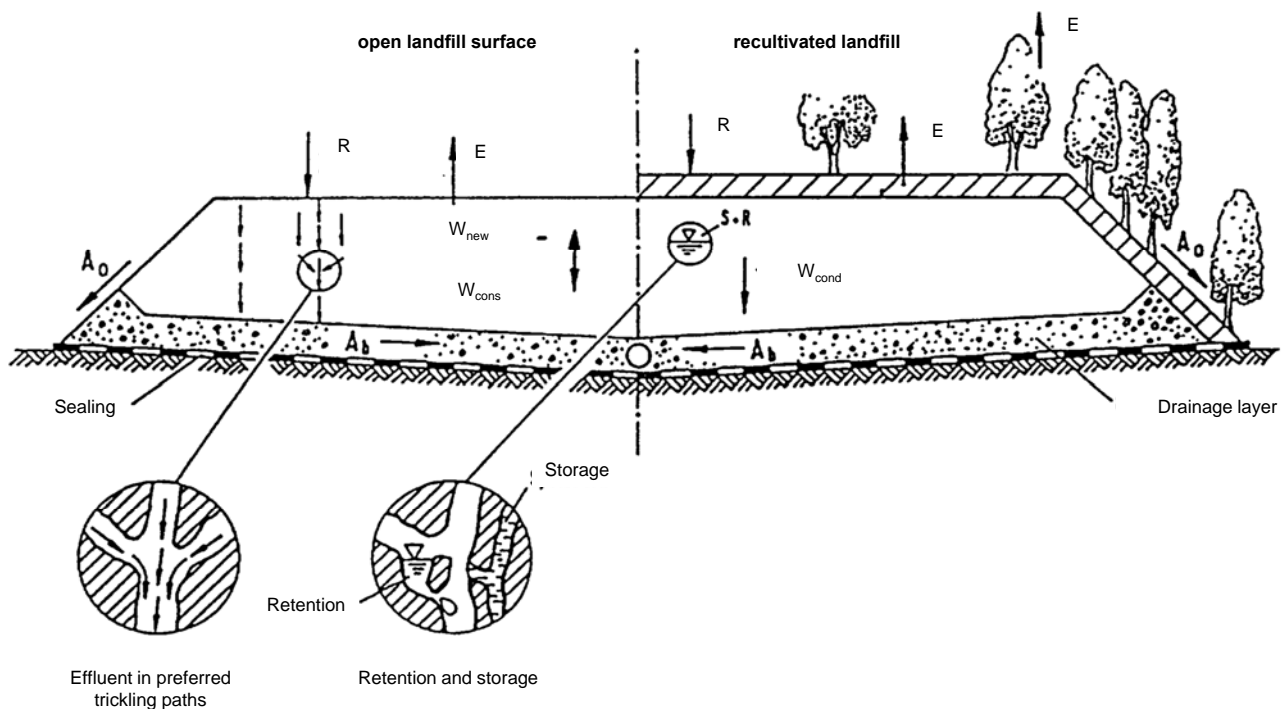
Leachate Production

$$Q_{\text{leach}} = R - E - E_s - R - S + W_{\text{new}} - W_{\text{cons}} + W_{\text{cond}}$$

with

- Q_{leach} Leachate production
- R Rainfall
- E Evaporation and Transpiration
- E_s Surface effluent (unpolluted) without mixing with the leachate
- R Retention
- S Storage
- W_{new} Water production due to microbial processes
- W_{cons} Water consumption due to microbial processes
- W_{cons} Water discharge due to consolidation processes (e.g. with sewage sludge)

Schematic Presentation of the Water Management of a Landfill (RAMKE, 1993)



Data from Reference Literature on Specific Leachate Amounts (THEILEN,1995)

| | Sealed surfaces | | Covered surfaces | | Operation surfaces | | | | New landfill sections | |
|---|------------------------------------|------------|---------------------------------------|-----------|-----------------------------|-----------|--------------------------------|-----------|-----------------------|----------------|
| | Combined sealing | | Thin Vegetation | | with Leachate recirculation | | without Leachate recirculation | | without pouring | |
| | average | max. | average | max. | average | max. | average | max. | average | max. |
| EHRIG, 1980 | nda | nda | nda | nda | nda | nda | 4 | 20 | nda | nda |
| LAGA, 1984 | nda | nda | nda | nda | nda | nda | 4,8 | > 48 | nda | nda |
| EHRIG, 1989 | nda | nda | nda | nda | nda | nda | 5 | 20 | nda | nda |
| DOEDENS / THEILEN, 1990 | 1 | 2,5 | nda | nda | 3 | 8 | 5 | 20 | nda | nda |
| | | | | | (irrigation) | | | | | |
| THEILEN, 1992 | 2 | 3,5 | nda | nda | 6 | 9 | 7,5 | > 20 | nda | nda |
| | | | | | (trickling) | | | | | |
| RAMKE, 1993 | 3,4 | 6,6 | 7,6 | nda | nda | nda | 10,8 | 100 | nda | nda |
| | (from sewage sludge consolidation) | | (withouth sewage sldge consolidation) | | | | | | | |
| CAPTAIN / RIEGLER, 1994 | 1,2 | nda | nda | nda | nda | nda | 12,8 | nda | 19 | nda |
| Dimensioning suggestion [m³/(ha*d)] | 1,5 | 3,5 | 7,5 | 20 | 7,5 | 15 | 10 | 40 | 20 | > 50 |

TASI had forbidden it, the Landfill Ordinance of 2002 permits it again, with the pertaining controls (bottom sealing necessary)



Leachate concentrations of conventional Municipal Waste Landfills (without waste management measures)

| | | Acidic Phase | | Methanogenic Phase | |
|------------------|----------------------|--------------|---------|--------------------|---------|
| | | Range | Average | Range | Average |
| pH-value | --- | 4,5 -7,5 | 6,1 | 7,5-9 | 8 |
| COD | mg O ₂ /L | 6.000-60.000 | 22.000 | 500-4500 | 3.000 |
| BOD ₅ | mg O ₂ /L | 4.000-40.000 | 13.000 | 20-550 | 180 |
| Ca | mg/L | 10-2.500 | 1.200 | 20-600 | 60 |
| SO ₄ | mg/L | 70-1.750 | 500 | 10-420 | 80 |
| Zn | mg/L | 0,1-120 | 5 | 0,03-45 | 0,6 |
| Fe | mg/L | 20-2.100 | 780 | 3-280 | 15 |

| | | Parameter without significant changes | |
|--------------------|------|---------------------------------------|---------|
| | | Range | Average |
| TKN | mg/L | 50-5.000 | 1.350 |
| NH ₄ -N | mg/L | 30-3.000 | (750) |
| Cl | mg/L | 100-5.000 | 2.100 |
| Pb | µg/L | 8-1.020 | 90 |
| Cd | µg/L | 0,5-140 | 6 |
| Cu | µg/L | 4-1.400 | 80 |
| Ni | µg/L | 20-2.050 | 200 |
| Hg | µg/L | | |
| Cr | µg/L | 30-1.600 | 300 |
| AOX | µg/L | 320-3.350 | 2.000 |

[EHRIG, 1980]



Comparison of various Method Combinations

| | SS | BOD ₅ | COD | Total N _{min} | NH ₄ -N/ NH ₃ -N | Heavy metal | AOX | Salt | Fish toxicity |
|---|----|------------------|-----------------|------------------------|---|-----------------|-----------------|---------------|------------------|
| Biological treatment | | + | + ²⁾ | + | + | - | - | - | 7) |
| Adsorption | - | | + ³⁾ | - | - | | + | - | 7) |
| Sedimentation/ Flotation ⁸⁾ | | - | - | - | - | - | - | - | 7) |
| Flocculation/ Precipitation | - | | + ³⁾ | - | - | + ⁵⁾ | + | - | 7) |
| Filtration | + | - | - | - | - | - | - | - | 7) |
| Reverse osmosis | + | + ¹⁾ | + ¹⁾ | + | + | + | + ¹⁾ | + | 7) |
| Nano-filtration | + | + | + | - | - | ⁹⁾ | + | ⁹⁾ | 7) |
| Stripping | - | - | - | + | + | - | - ⁶⁾ | - | 7) |
| Chemical oxidation | - | | + | - | - | - | + | - | 7) |
| Evaporation | + | | + ⁴⁾ | + | - | + | + ⁴⁾ | + | 7) |
| Incineration | + | + | + | + | + | + | + | + | |

+ generally suitable

1) less suitable for small molecule sizes

3) less suitable for bio-degradable substances

5) only with special heavy metal precipitation

7) reaching of a limit value cannot be evaluated safely

9) separation done for bivalent or superior ions

- generally unsuitable

2) only suitable for degradable organic substances

4) less suitable for substances which are volatile under the process conditions

6) not suitable for hardly volatilisable substances

8) separation of solids in combination with other methods



Solid Waste Management

Dr.-Ing. Dirk Weichgrebe



Leibniz
Universität
Hannover

Effluent Values and Discharged Loads of the Various Method Combinations for Direct Discharge

| Effluent concentrations (C _e) and effluent loads (B _a) of various combinations | | | | | | | | | | | |
|--|-------|-------------------------------|----------------------|----------------|----------------------|----------------|----------------------|----------------------|----------------------|----------------------|----------------------|
| Q _d = 150 m ³ /d | | Raw leachate (influent) | Combination I | | Combination II | | Combination III | | Combination IV | | |
| Parameter | Unit | | UO/ED/TR/NA | BIO/UO/ED/TR | BIO/CHO/BIO | BIO/AC | C _e | B _a (t/a) | C _e | B _a (t/a) | |
| | | C _e | B _a (t/a) | C _e | B _a (t/a) | C _e | B _a (t/a) | C _e | B _a (t/a) | C _e | B _a (t/a) |
| COD | mg/L | 2500 | 15 | 0,821 | 25 | 1,369 | 150 | 8,213 | 150 | 8,213 | |
| BOD ₅ | mg/L | 250 | 5 | 0,274 | 10 | 0,548 | 5 | 0,274 | 5 | 0,274 | |
| TKN | mg/L | 1300 | 10 | 0,548 | 30 | 1,643 | 70 | 3,833 | 100 | 5,475 | |
| NH ₄ -N | mg/L | 1100 | 7 | 0,383 | 0,5 | 0,027 | 1 | 0,055 | 1 | 0,055 | |
| NO ₃ -N | mg/L | <10 | 0,1 | 0,005 | 60 | 3,285 | 60 | 3,285 | 60 | 3,285 | |
| inorg. N | mg/L | 1110 | 7 | 0,383 | 62 | 3,395 | 62 | 3,395 | 62 | 3,395 | |
| AOX | μg/L | 2500 | 50 | 2,738 | 100 | 5,475 | 300 | 16,425 | 300 | 16,425 | |
| LF | mS/cm | 15 | 0,40 | | 0,30 | | 12,50 | 0,684 | 12,50 | 0,684 | |
| Cl ⁻ | mg/L | 2000 | 50 | 2,738 | 150 | 8,213 | 2000 | 109,500 | 2000 | 109,500 | |
| TR | % | 1,00 | 0,01 | 5,475 | 0,09 | 49,275 | 0,9 | 492,750 | 0,9 | 492,750 | |



Solid Waste Management

Dr.-Ing. Dirk Weichgrebe



Leibniz
Universität
Hannover

Further Emissions; Vermin

- Pertaining to noise and dust: Federal Emission Control Act, TI Noise and TI Air
- Pertaining to odours: Odour Emission Protection Directive (GIRL)
- Vermin:
 - Insects
 - Rats
 - Birds (seagulls, crows, but also protected species, like the red kite)
 - generally no or very small problems with treated waste



Landfill Operation / Operating Plan

- Landfill sections,
 - maybe separation into types of waste which react differently
- Grids for landfill land register
 - $\leq 1.000 \text{ m}^2$ (for dangerous waste; for mono-landfill also larger)
or $\leq 2.500 \text{ m}^2$ (for harmless waste (TASi N0. 10.6.1)) and $\leq 2\text{m}$ height
- Documentation; annual topographic survey of the landfill and explanations on the landfill behaviour
- Filling in a stable way without many hollows
 - Compactors
- Intermediate covers for single landfill layers with bottom often required abroad ???
- Dust, noise, wind drifts



Working Face and Thin Layer Operation

Tipping edge operation

—Unloading—Comminution through overrunning—Tipping edge—

Landfilling until 31.05.2005 MBA Output

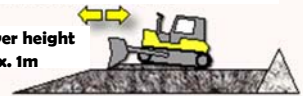


Taking MBA Output



Filling and compacting in thin layers

Layer height max. 1m



Intermediate cover after max. 2m



Further filling



Thin Layer Operation

—Unloading—Comminution through overrunning—Filling layer—

Filling of MBA Output-Material



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

111
102
1004
Leibniz
Universität
Hannover

Compressed Filling with Compactors

Waste compactor

BC 1172 RB

The new dimension of waste compacting

The BC 1172 is the heaviest completely hydrostatically waste compactor. It is particularly suitable for the use on landfills with waste amounts of up to 1500 Mg per day. Excellent efficiency degrees, high performance reserves and superior agility make for the best economic efficiency at highest compacting degrees.



| Type | Weight [kg] | Push blade/hovel width [mm] | Power [kW] |
|------------|------------------|--------------------------------|---------------|
| BC 572 RB | 25.900 to 26.700 | 3.800 | 214 (Deutz) |
| BC 672 RB | 32.100 to 32.700 | 3.800 | 314 (Deutz) |
| BC 772 RB | 36.500 to 37.100 | 3.800 | 330 (Deutz) |
| BC 772 RS | 36.500 to 37.100 | 3.800 | 330 (Deutz) |
| BC 972 RB | 45.100 to 46.700 | 5.200 | 381 (Deutz) |
| BC 1172 RB | 54.500 to 55.100 | 5.200 | 400 (Deutz) |



Solid Waste Management
Dr.-Ing. Dirk Weichgrebe

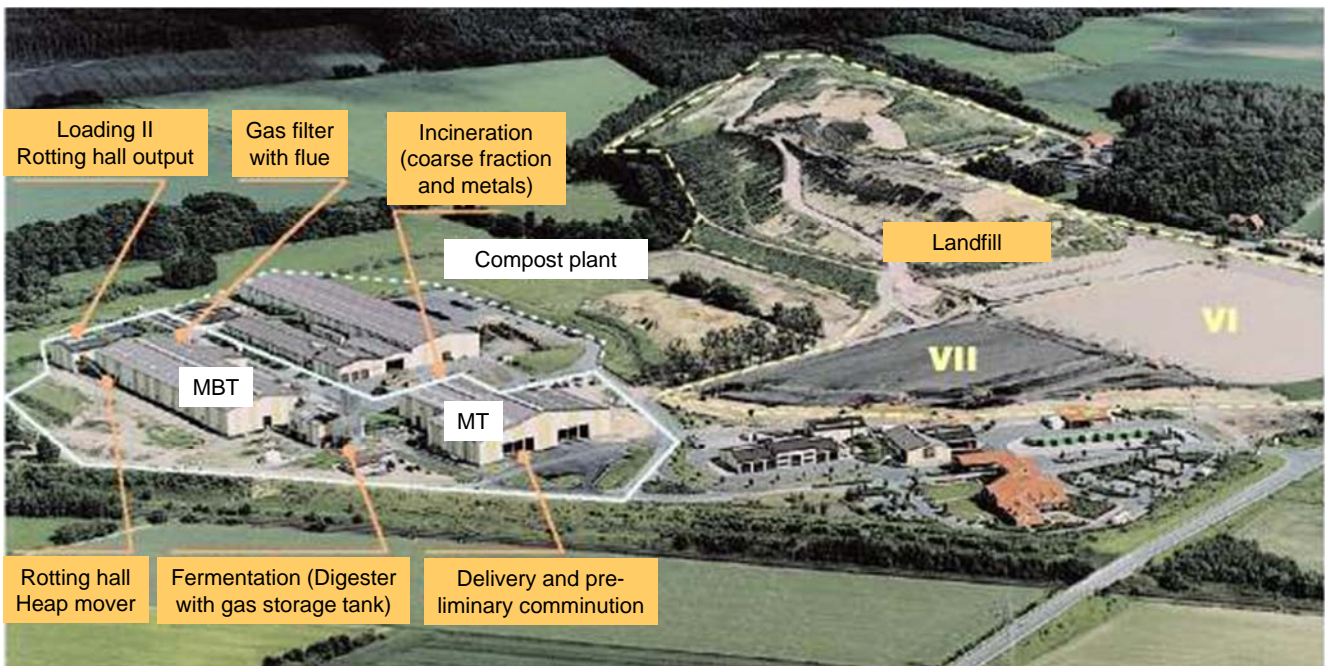
111
102
1004
Leibniz
Universität
Hannover

Landfill Operation 2

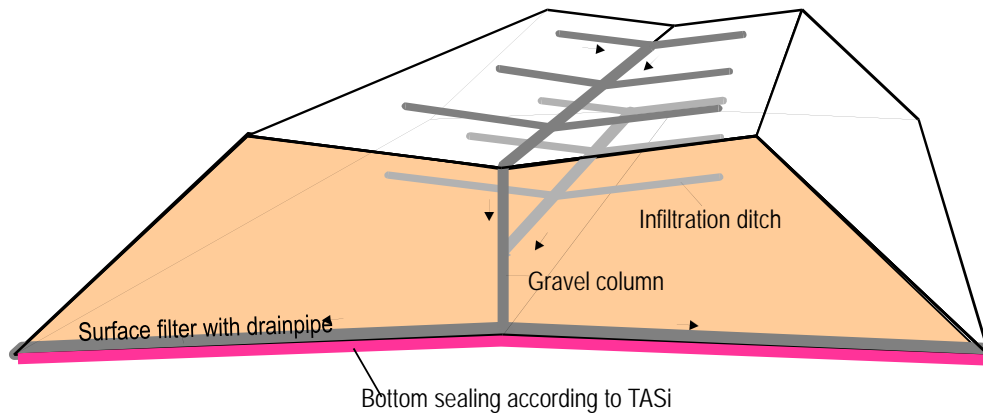
- Intermediate covers with bottom often required abroad???
- Dust, noise, wind drifts



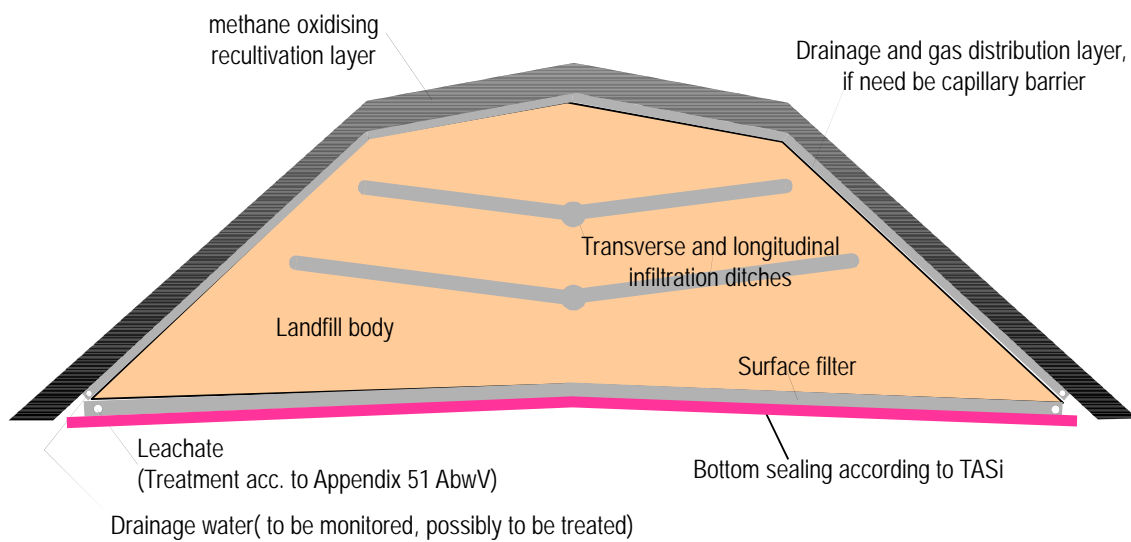
Waste Management Centre at State 2001



MBT Landfill – Internal Drainage



MBT Landfill Structure

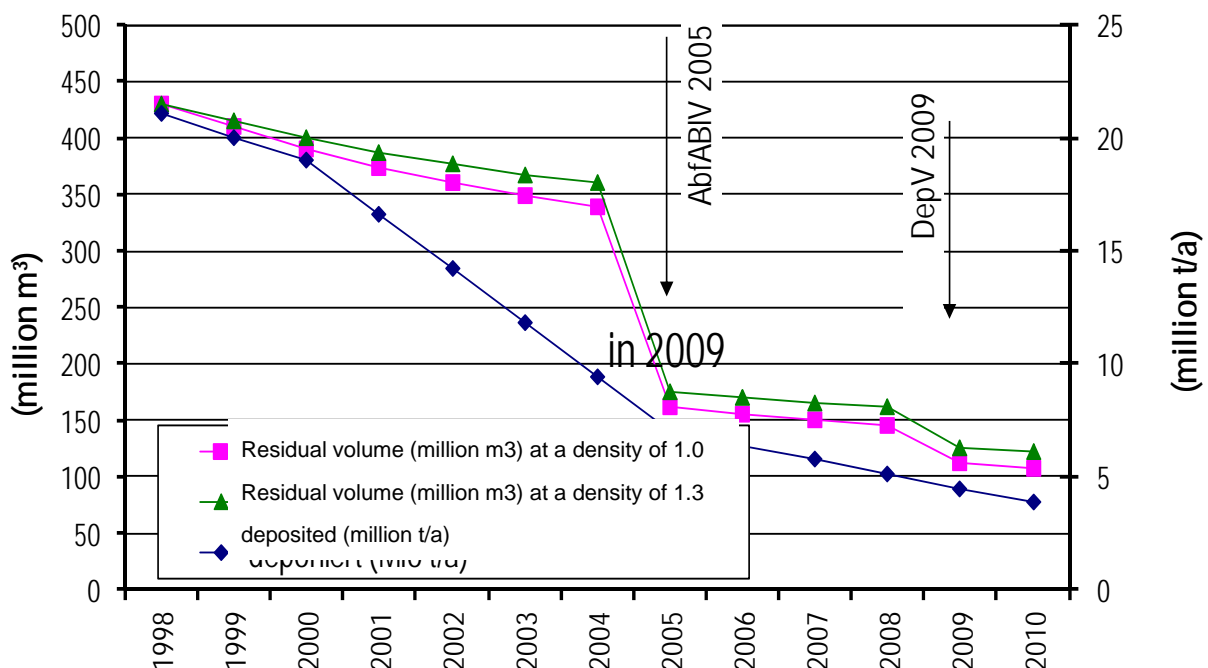


Milestones for the future depositing of municipal waste

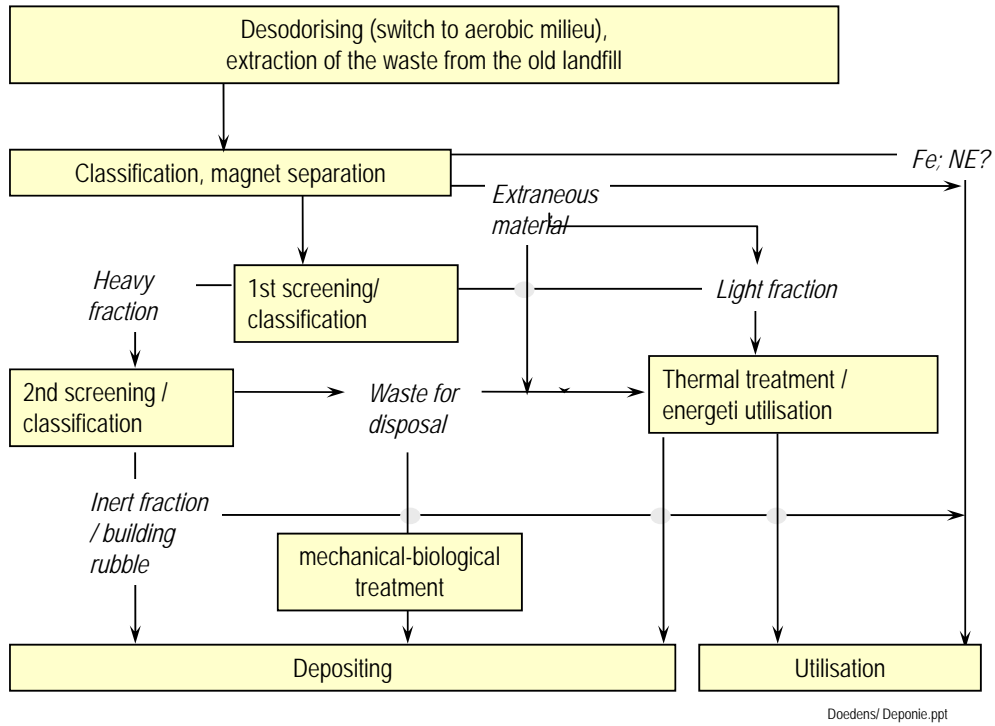
| Date | Basis | Consequences |
|------------|--|---|
| 31.05.2005 | Waste Depositing Ordinance → TASI | <ul style="list-style-type: none"> • Closing of landfills which do not comply with No. 10 TASI (without 10.3.1 and .2); • Terminating the depositing of waste which does not comply with Appendices 1 and 2 of the Waste Depositing Ordinance |
| 17.07.2009 | Waste Depositing Ordinance / EU Landfill Directive | Closing of all landfills which do not comply with the requirements of the Waste Depositing Ordinance (also location + geology) |
| 2020 | Political target of the FEA | No waste for disposal → End of <u>any</u> depositing |

Future LC II Depositing Demand and Residual Capacities Source 1998/99: UBA, 2001

Assumptions for closedowns: 50% in 2005, and 20% of the number of the previous year in 2009



Renaturalisation of Old Landfills for Raw Municipal Waste



Doedens/ Deponie.ppt