The background of the slide is a grayscale, high-angle photograph of a large, ornate, multi-story building with many arched windows and a central tower, surrounded by trees. The image is semi-transparent, allowing the text to be overlaid.

# Lecture 6

# Water Distribution and Network

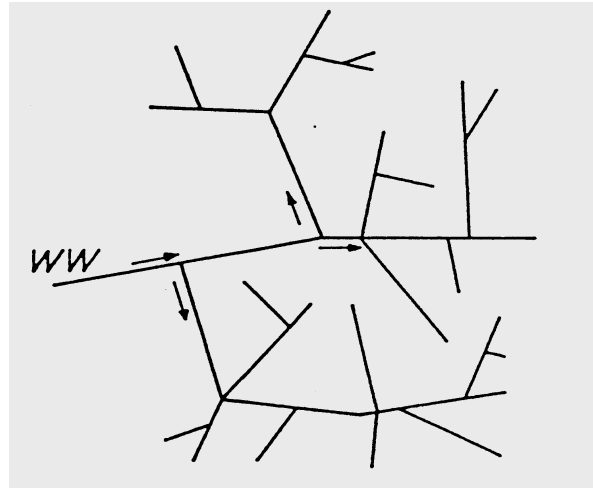
**Feeder pipings** (*Zubringerleitungen*) connect the area of water catchment (Wassergewinnungsgebiet) with the area of supply (*Versorgungsgebiet*) and lead usually to an elevated water tank (*Hochbehälter*).

**Distribution pipings** (*Verteilungsleitungen*) lead from the reservoir (*Speicher*) to the area of supply (*Verwendungsort*).

The distribution pipings network consists of **main-, supply- and connecting pipings** (*Haupt-, Versorgungs- und Anschlussleitungen*).

The main pipings begin at the reservoir or at a larger junction (*Knotenpunkt*) within the area of supply. The supply pipings connect the household with the water meter (*Wasserzähler*) and the main shutoff (*Hauptabsperrorgan*) device in the property.

## Branched Network (*Verästelungsnetz*)



### Disadvantages: therefore

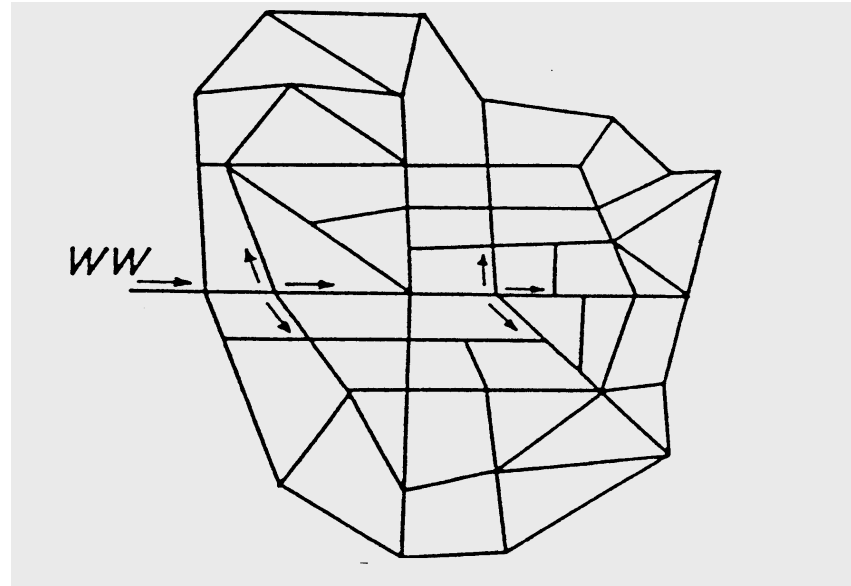
- Water consumption (*Wasserbezug*) only from one direction, low flexibility (*wenig anpassungsfähig*)
- Uneven pressure conditions (*Druckverhältnisse*)
- Interruption of the water supply (*Wasserlieferung*) in case of pipe bursts (*Rohrbrüchen*) and fires (*low operation security*)
- Degradation of the water quality (*Wasserbeschaffenheit*) and temperature in the final pipes (frequent flushing (*Spülen*) necessary)

### Advantages:

- Low costs

## Ring distribution network

(Ringnetz)



Advantages:

- High supply reliability (*Versorgungssicherheit*)
- Adjustment to varying water consumption (*schwankender Wasserverbrauch*)
- Favourable pressure conditions
- High water quality

The dimensioning of water pipings are commonly based on the following simplifications:

- **Steady flow**, i.e. velocity is constant (constant water discharge).
- **Uniform stream**, i.e. constant flow conditions (Bed gradient, friction, constant cross section).
- (Assumption that the middle velocity (*mittlere Fließgeschwindigkeit*) of flow is **uniformly distributed over the cross-section area**.
- **Incompressibility of the water**, as far as no larger amounts of gas are not contained in it.

## Continuity equation

$$Q = A_1 \cdot v_1 = A_2 \cdot v_2 = \text{constant}$$

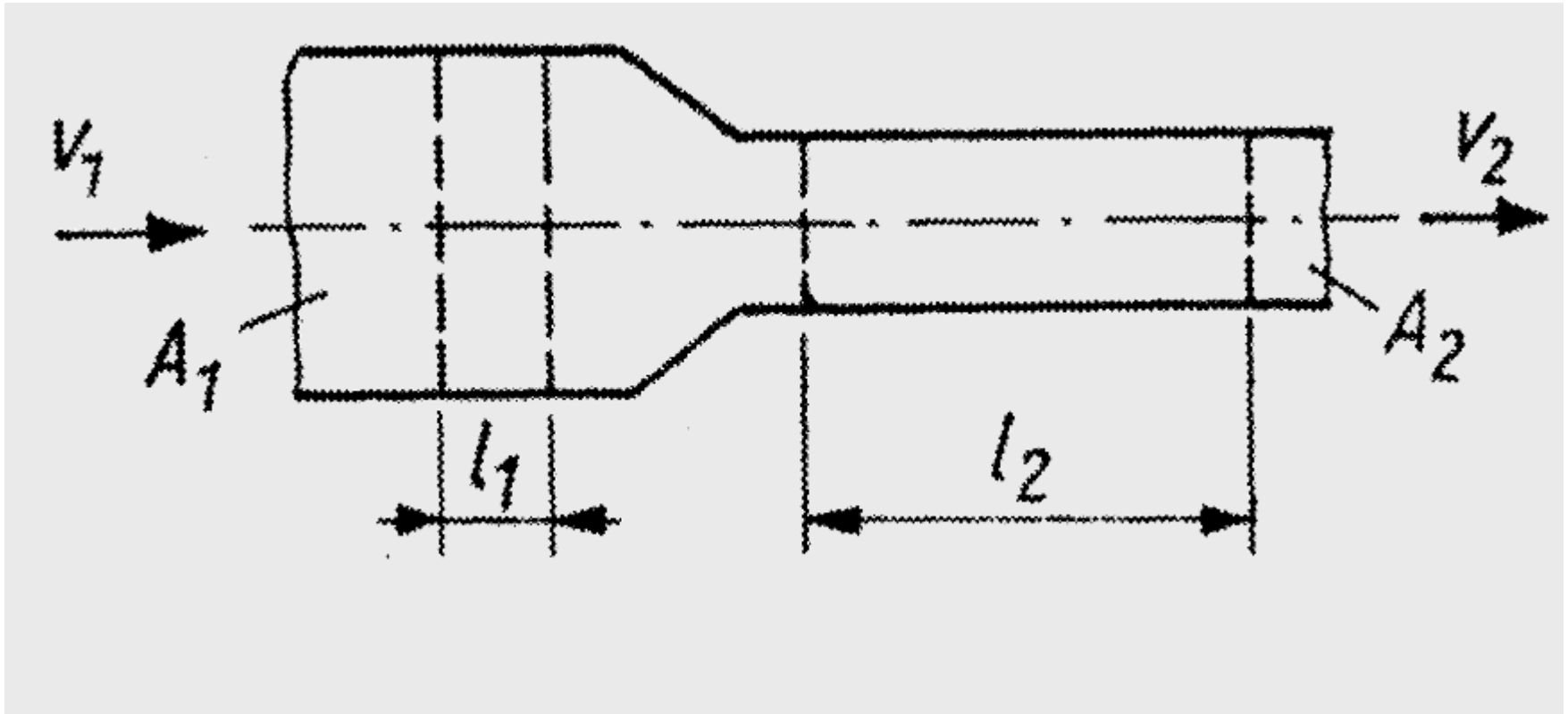
with:	Q	Volume flow [m <sup>3</sup> /s]
	v	Flow velocity [m/s]
	A	cross sectional area [m <sup>2</sup> ]

## Energy equation (Bernoulli equation)

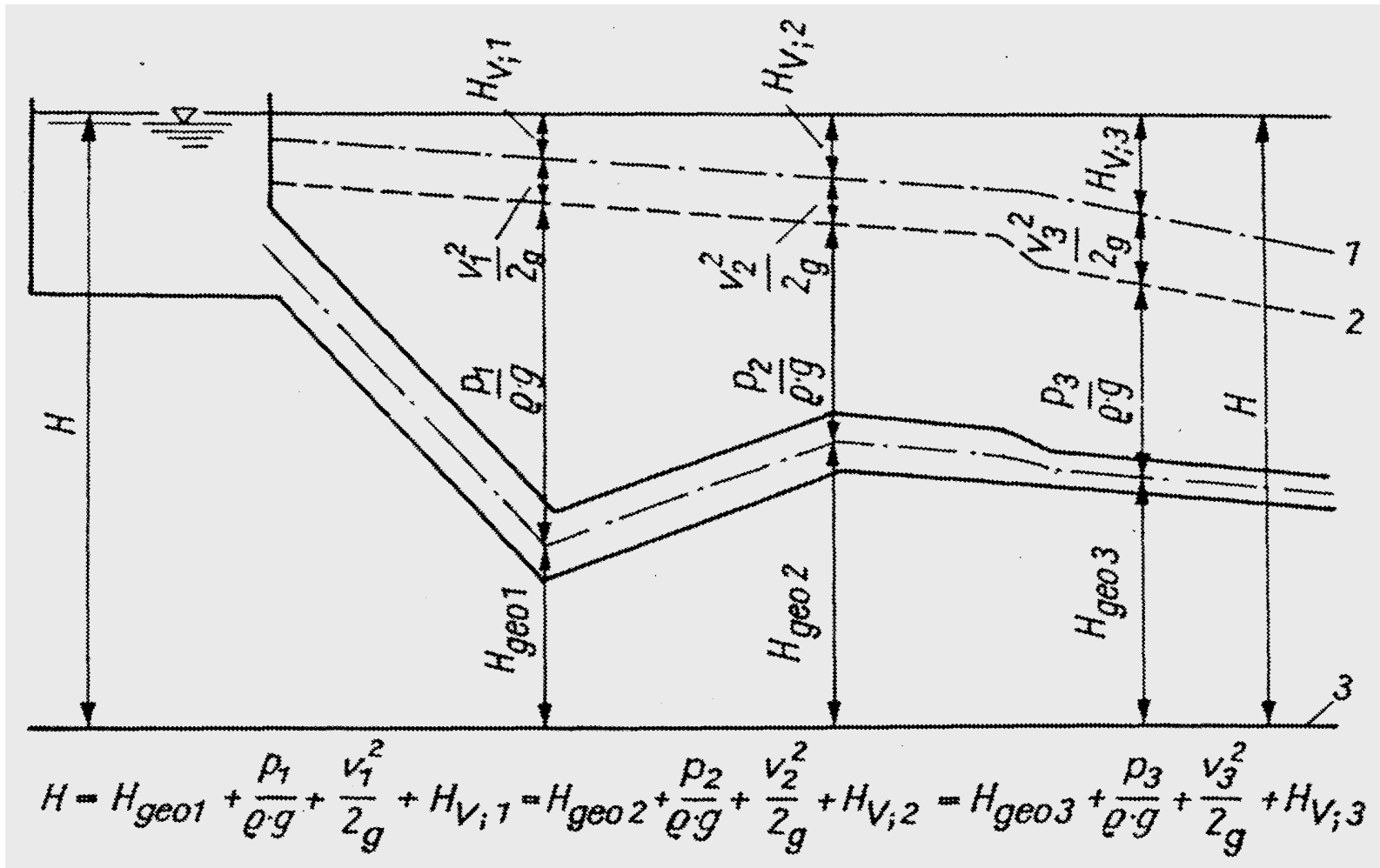
$$h_E = \frac{v_1^2}{2g} + \frac{p_1}{\rho \cdot g} + z_1 = \frac{v_2^2}{2g} + \frac{p_2}{\rho \cdot g} + z_2 + h_v$$

with:	$h_E$	Energy head [m]
	$p$	Pressure [bar]
	$\rho$	Density of the fluid [kg/m <sup>3</sup> ]
	$z$	Geodetic height [m]
	$h_v$	Energy loss through friction [m]

# Stream piping



# Bernoulli equation illustrated with a pressure pipeline





## Darcy-Weisbach equation

$$h_v = \lambda \cdot \frac{l}{d} \cdot \frac{v^2}{2g}$$

with:  $h_v$  Head loss due to friction [m]

## Friction coefficient

$$\lambda = f\left(\frac{k}{d}, \text{Re}\right) \quad \text{with: } \frac{k}{d} = \text{relative roughness}$$

for non circular pipes and channels the hydraulic diameter  $d_{hy}$  is used instead of the diameter  $d$

$$d_{hy} = 4 r_{hy} = \frac{4A}{l_p}$$

with:  $l_p$  Wetted perimeter [m]

For flow in a pipe or tube, the Reynolds number is generally defined as:

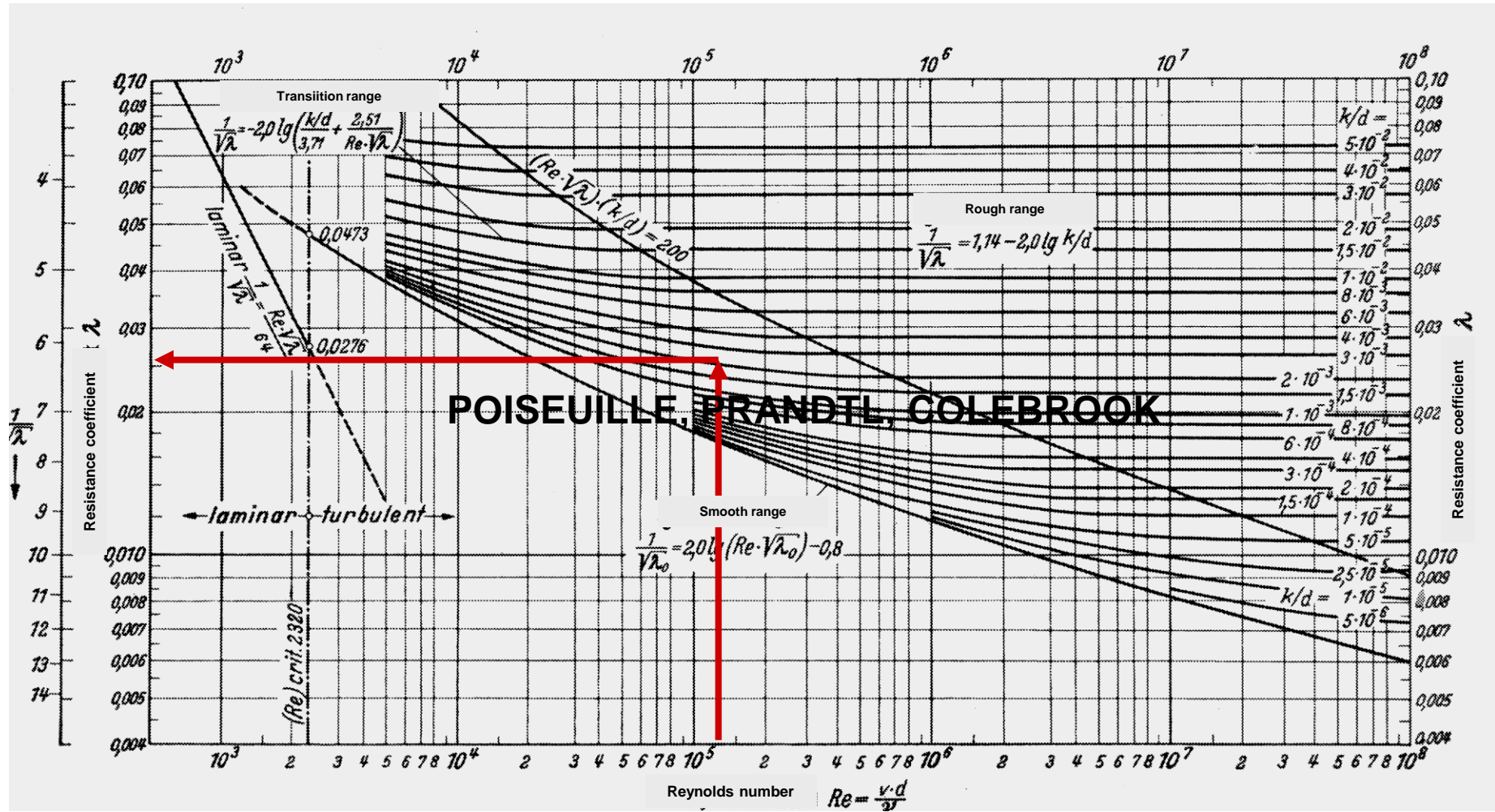
$$Re = \frac{v \cdot D}{\nu}$$

with:	$\nu$	kinematic viscosity	
	$\nu_{\text{water}}$	1,2 - 1,8*10 <sup>-6</sup>	[m <sup>2</sup> /s]
	$\nu_{\text{waste water}}$	1,31*10 <sup>-6</sup>	[m <sup>2</sup> /s]

For the **friction coefficient**  $\lambda$  there can be differentiated 3 ranges:

1. **Smooth range:**  $\lambda$  depends only on Re and is therefore independent of the condition of the pipe wall.
2. **Rough range:**  $\lambda$  depends only on the condition of the pipe wall, in other words on the so-called relative roughness k/d, however not on Re.
3. **Transition range:**  $\lambda$  is dependent on Re as well as on k/d.

# Friction coefficient for full circular pipes after POISEUILLE, PRANDTL, COLEBROOK



The calculation of **pipe friction loss** (*Rohrreibungsverlusten*) is based on the already presented Darcy-Weisbach equation:

$$h_v = h_f = \lambda \cdot L/D \cdot v^2/2g$$

with:

$\lambda$	friction factor [-]
L	length of the pipe [m]
D	pipe diameter [m]
g	gravitational acceleration = 9,81 [m/s <sup>2</sup> ]

If one refers the determined friction loss height  $h_v$  (m) on the projection length  $L'$  of the actual piping length L (km), then the **gradient of energy** (*Energieliniengefälle*) or **gradient of friction** (*Reibungsgefälle*)  $I_E$  can be calculated according to the following formula:

$$I_E = \frac{h_v}{L'}$$

Using the “individual concept”, the pipe friction losses  $h_r$  and the local losses  $h_{v,L}$  (curves, armatures, etc.) are calculated separately. The total losses  $h_v$  over the whole tubing distance amount to: :

$$h_v = h_r + h_{v,L} \quad [\text{m}]$$

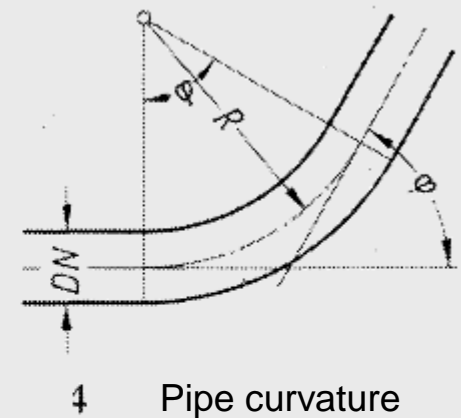
For the local losses  $h_{v,L}$ , the following relationship is valid:

$$h_{v,l} = \zeta_K * v^2/2g$$

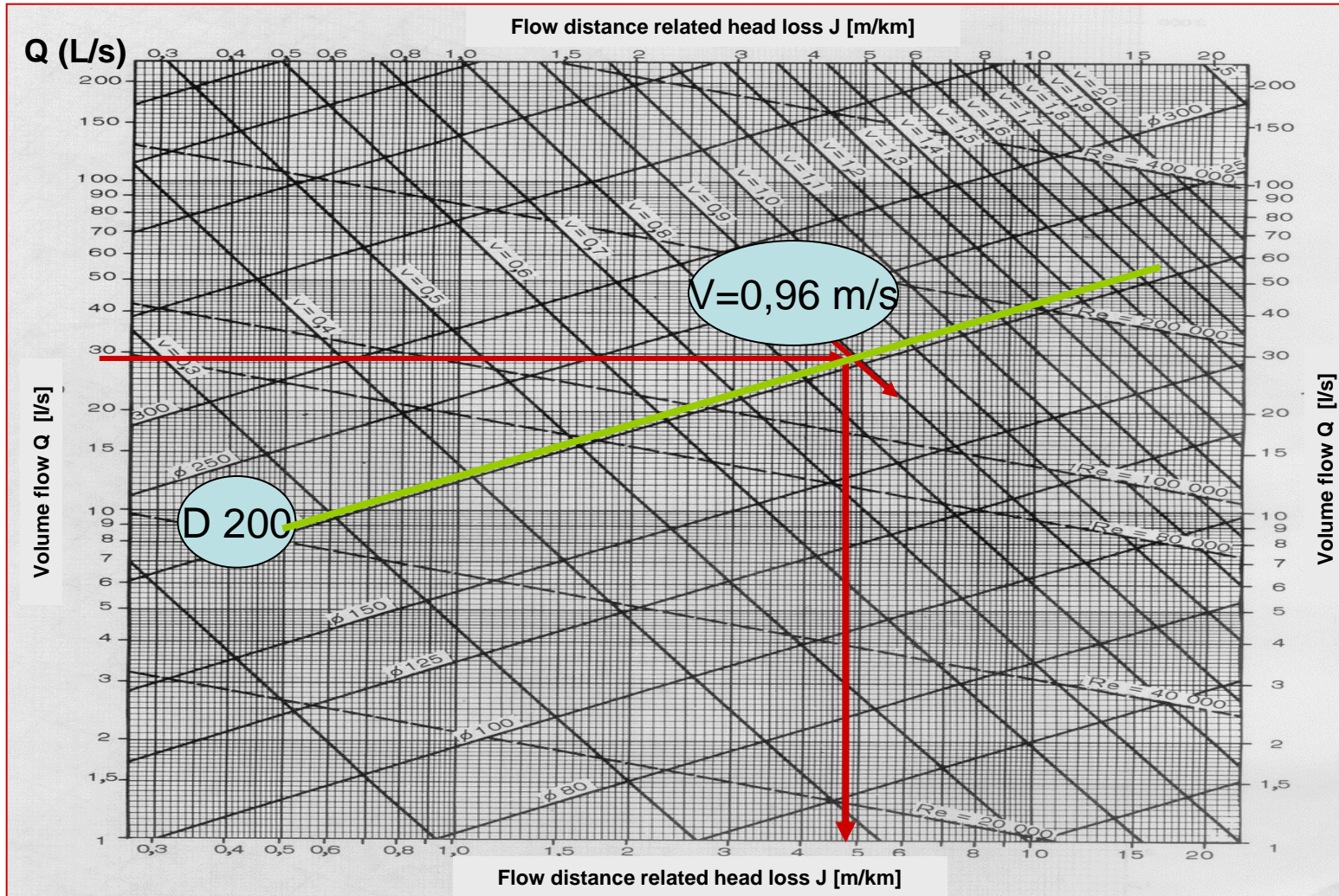
# Determination of the pipe friction loss

Coefficients  $\zeta_k$  for pipe curvatures

$\varphi$	Curvature radius: nominal size = R : DN					
	1	2	4	5	6	10
15°	0,03	0,03	0,03	0,03	0,03	0,03
22,5°	0,045	0,045	0,045	0,045	0,045	0,045
45°	0,14	0,09	0,08	0,075	0,07	0,07
60°	0,19	0,12	0,10	0,09	0,07	0,07
90°	0,21	0,14	0,11	0,1	0,09	0,08



# General Concept



Head loss diagram

For  $k_i = 0,4$  mm

According to DVGW-W302

# Determination of pipe friction head loss (DVGW W 302)

Flow distance related head loss for  $k_i = 0,4 \text{ mm}$   
 $\emptyset =$  inside diameter (mm)

Q L/s	$\emptyset 100$		$\emptyset 125$		$\emptyset 150$		$\emptyset 200$	
	v m/s	J m/km	v m/s	J m/km	v m/s	J m/km	v m/s	J m/km
1	0,13	0,302	0,08	0,101	0,06	0,041		
1,5	0,19	0,638	0,12	0,210	0,08	0,085		
2	0,25	1,094	0,16	0,356	0,11	0,144		
3	0,38	2,359	0,24	0,759	0,17	0,304	0,10	0,073
4	0,51	4,095	0,33	1,307	0,23	0,520	0,13	0,124
5	0,64	6,301	0,41	2,001	0,28	0,791	0,16	0,187
6	0,76	8,977	0,49	2,839	0,34	1,118	0,19	0,262
7	0,89	12,123	0,57	3,821	0,40	1,501	0,22	0,350
8	1,02	15,738	0,65	4,948	0,45	1,938	0,25	0,449
9	1,15	19,822	0,73	6,219	0,51	2,431	0,29	0,562
10	1,27	24,375	0,81	7,635	0,57	2,979	0,32	0,686
15	1,91	54,182	1,22	16,876	0,85	6,546	0,48	1,489
20	2,55	95,719	1,63	29,723	1,13	11,490	0,64	2,595
30			2,44	66,229	1,70	25,509	0,95	5,715
40			3,26	117,154	2,26	45,034	1,27	10,044
50					2,83	70,064	1,59	15,582
60					3,40	100,601	1,91	22,328
70							2,23	30,283
80							2,55	39,447
90							2,86	49,819
100							3,18	61,400



## Manning-Strickler

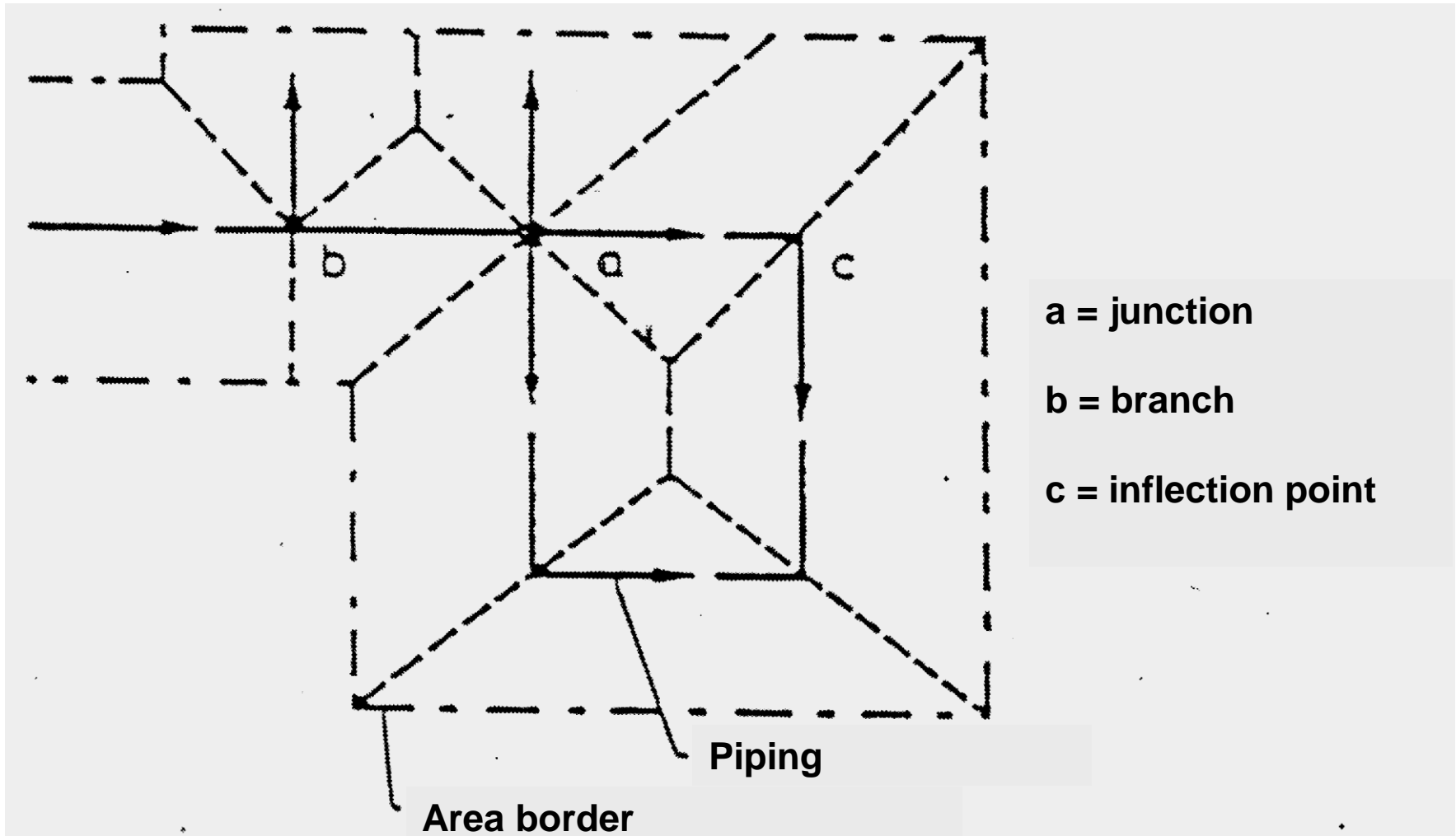
$$v = k_{St} \cdot r_{hy}^{2/3} \cdot I_E^{1/2}$$

with  $r_{hy} = A / I_u =$  hydraulic radius [m]  
 $k_{St} =$  Manning-Strickler roughness coefficient [m<sup>1/3</sup>s<sup>-1</sup>]  
 $I_E =$  energy gradient [-]

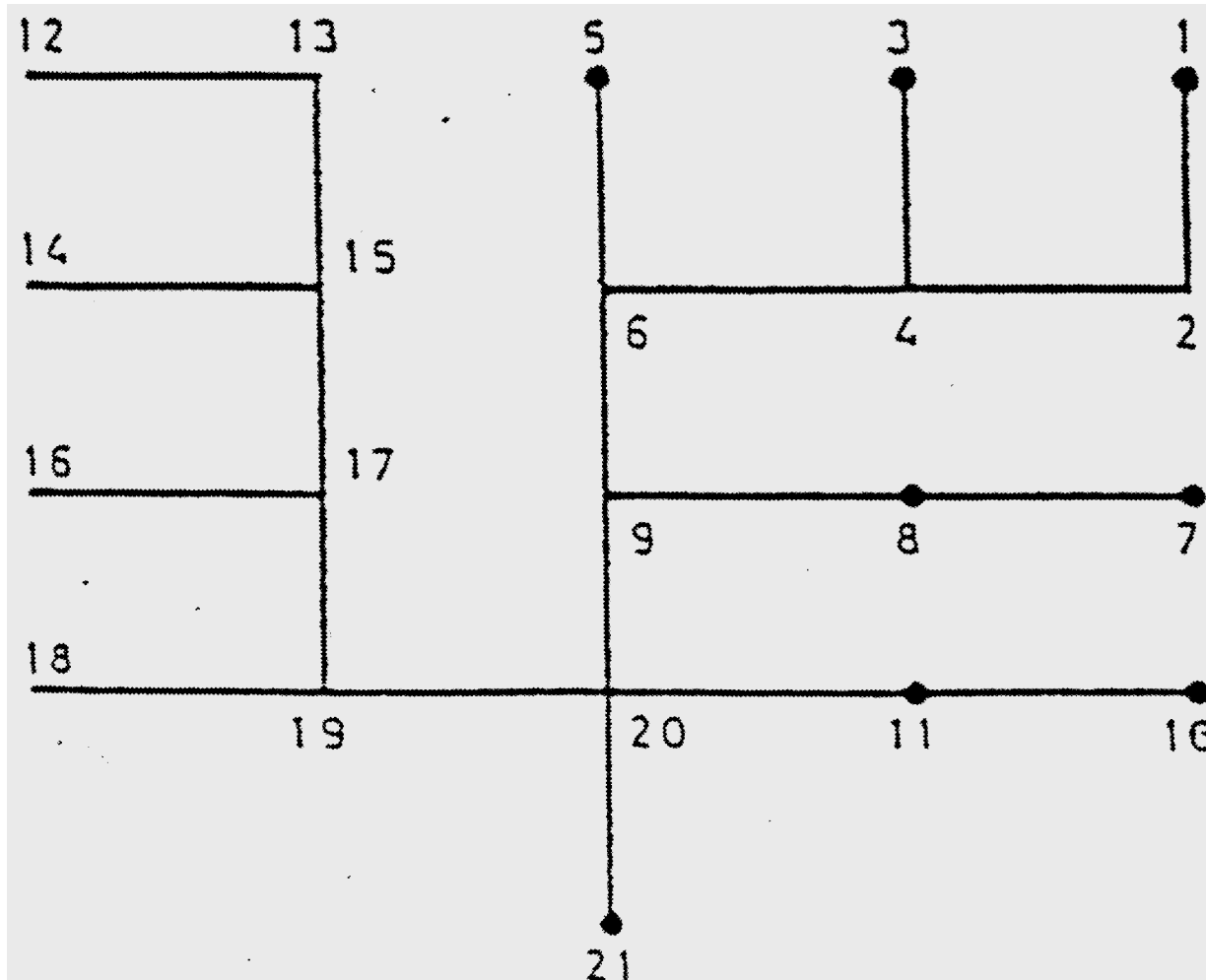
### $k_{St}$ values

Soil canal	30 - 50
Stonewalled canal	50 - 75
Concrete canal	50 - 95

# Area segmentation for the calculation of water flow quantities



# Determination of calculation points



Assuming that the consumption within the area of supply along the lines is constant, and that the total consumption  $Q$  and the entire pipe length  $L$  is well-known, than the **distance quantity value** (*Metermengenwert*) and/or **surface quantity value** (*Flächenmengenwert*) can be calculated as follows:

$$q_m = \frac{Q}{L} \quad [m^3/m \cdot s \cdot 1000 = (l/s)/m]$$

Considering the area and population,  $q_m$  can be calculated with:

$$q_m = \frac{A \times E_{\max} \times Q_h}{S l' \times 3600} \quad [(l/s)/m]$$

$l'$  = comparison length, e.g. = 2  $L$  when bilateral/double-sided construction,  
 $\max Q_h$  in  $l/\text{inhabitant} \cdot h$ , e.g. 10 - 15  $l/\text{inhabitant} \cdot h$

# Reference values for the determination of distance quantity values

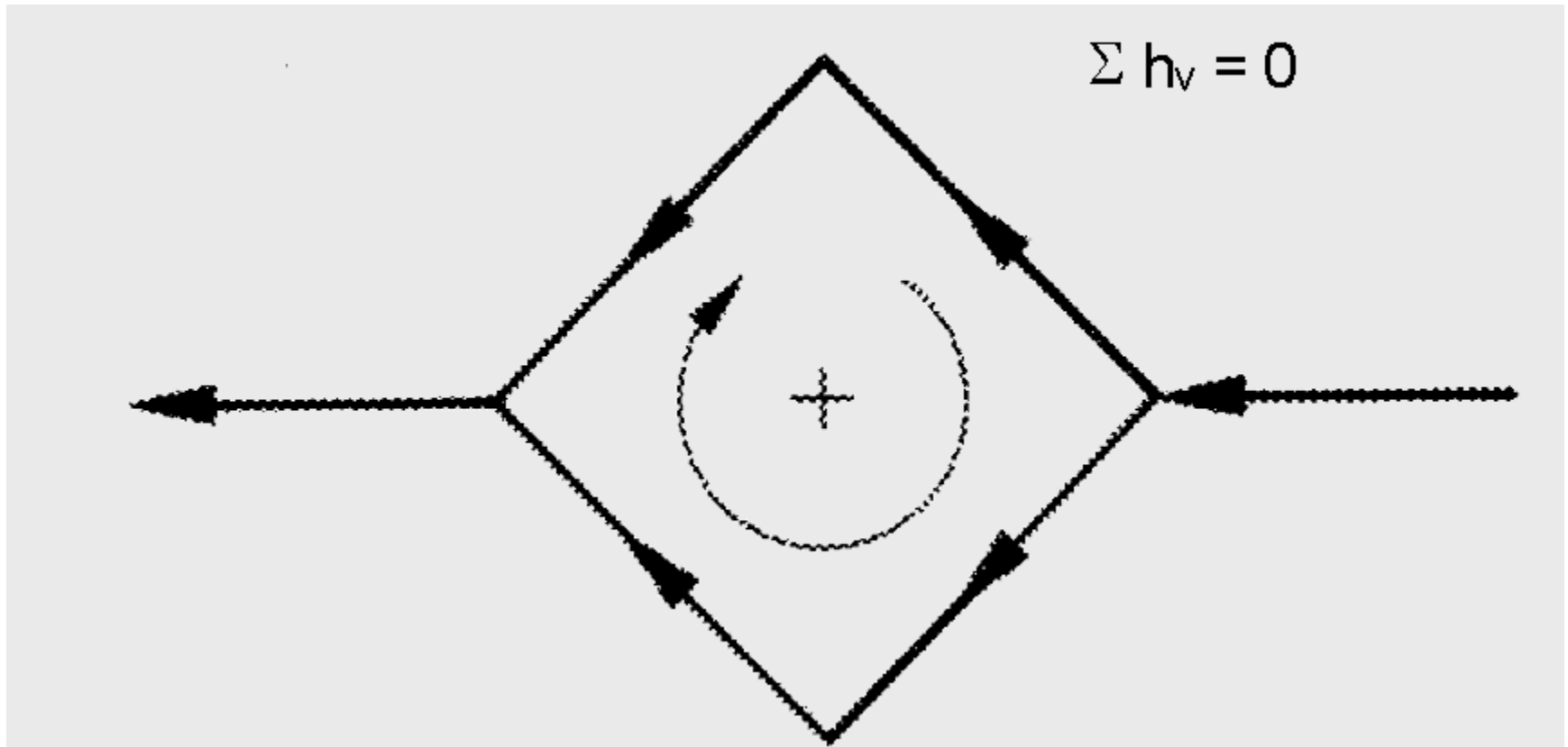
Type of development	Built-up area %	Inhabitants per ha	Pipe length per ha	Distance quantity value $q_m$ [l/s/m]
very dense (downtown area)	50	400 - 800	230	0,0048
dense (row houses)	40	250 - 350	220	0,0034
middle dense (houses)	30	150 - 200	200	0,0028
spacious (one-family-house)	20	100 - 120	130 - 150	0,0025
outer region	10	60 - 90	90 - 100	0,0023

A ring distribution network can be calculated with the **iterative Cross-method**

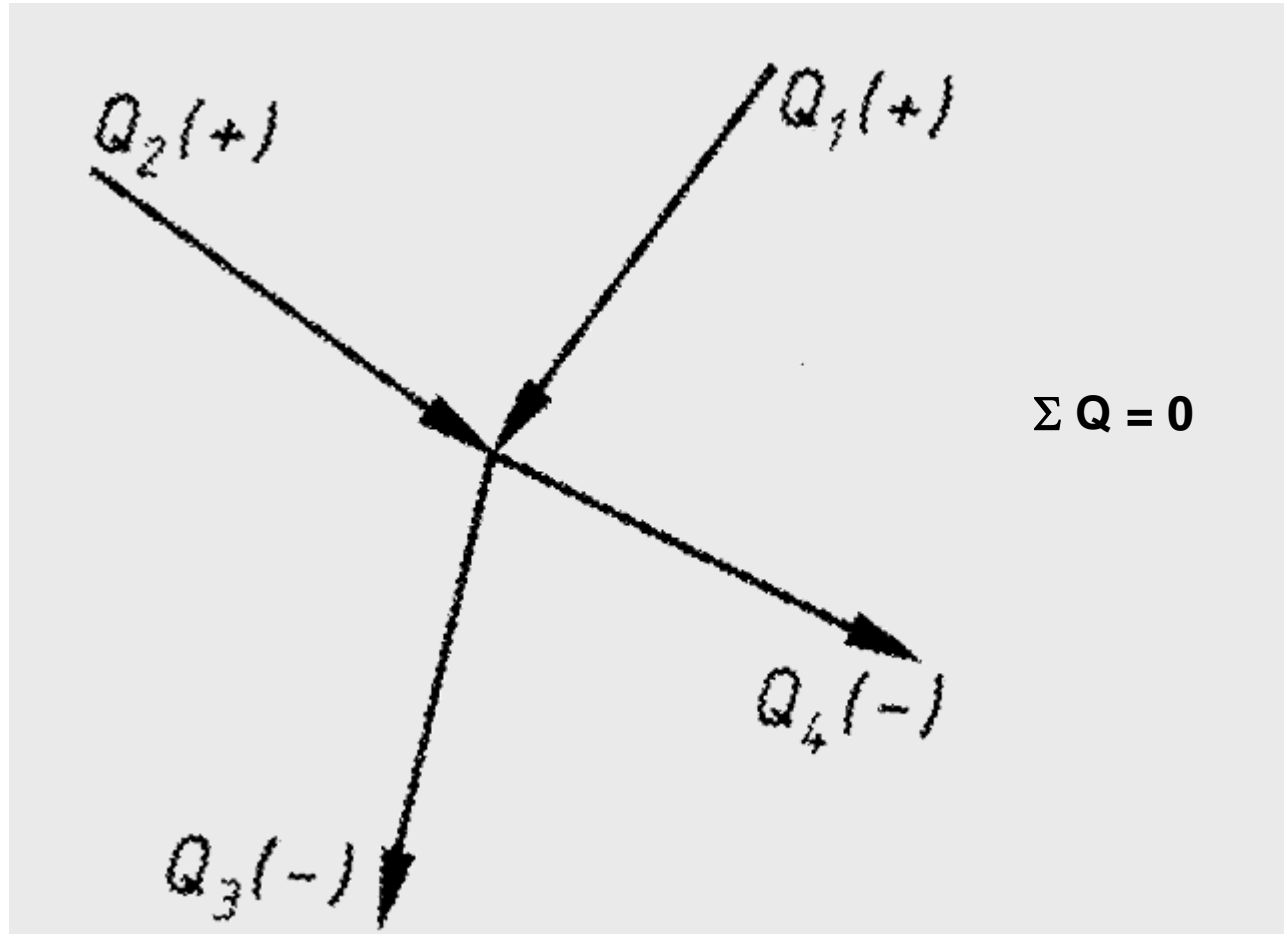
In meshed pipe distribution networks the two **Kirchhoff Laws** are valid:

1. **Mesh rule** (*Maschenbedingung*)
2. **Nodal-rule or knot-rule** (*Knotenbedingung*)

# Mesh rule according to CROSS

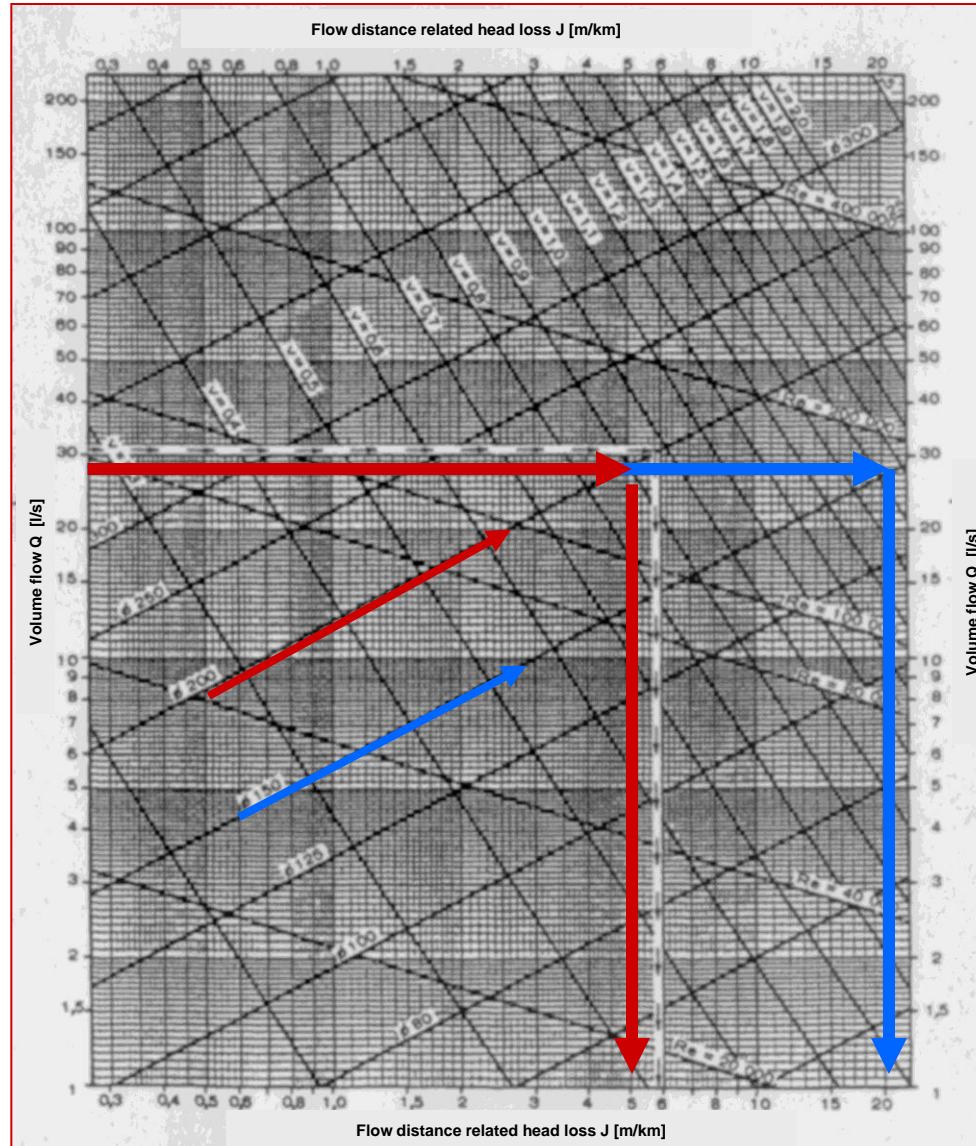


# Nodal rule or knot-rule



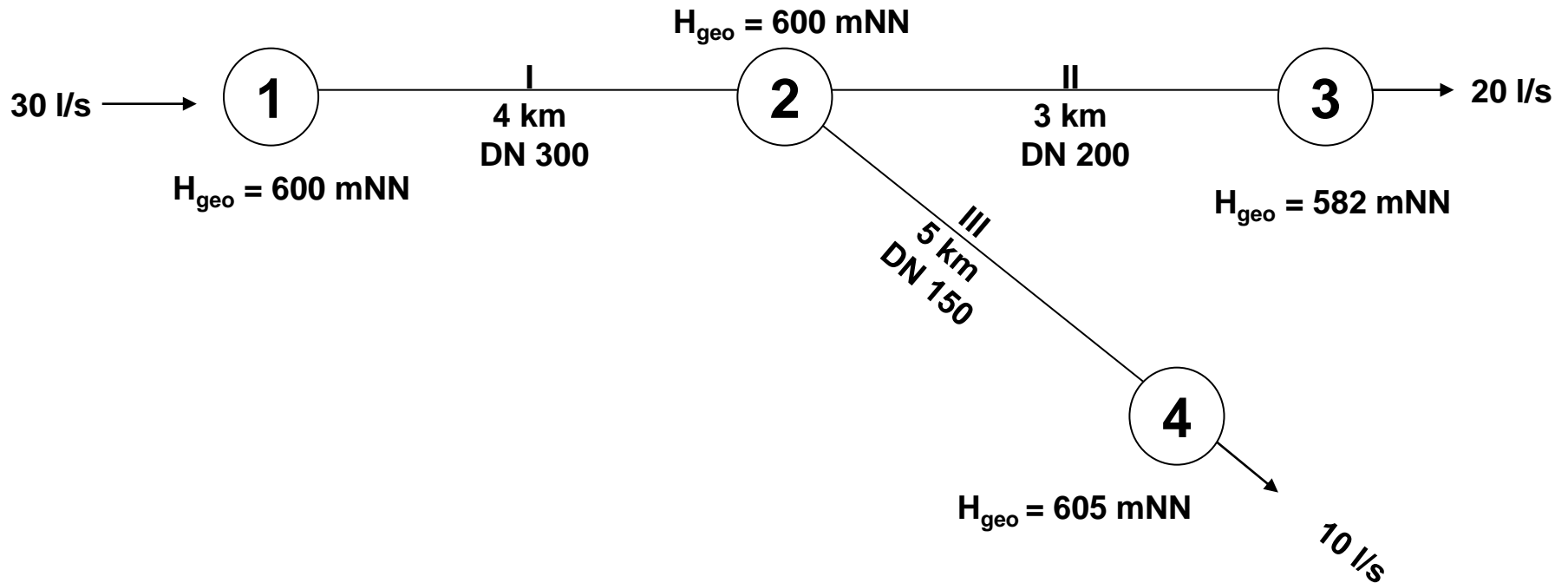


# Calculation of a distribution network



# Calculation of a distribution network

The following system is given:

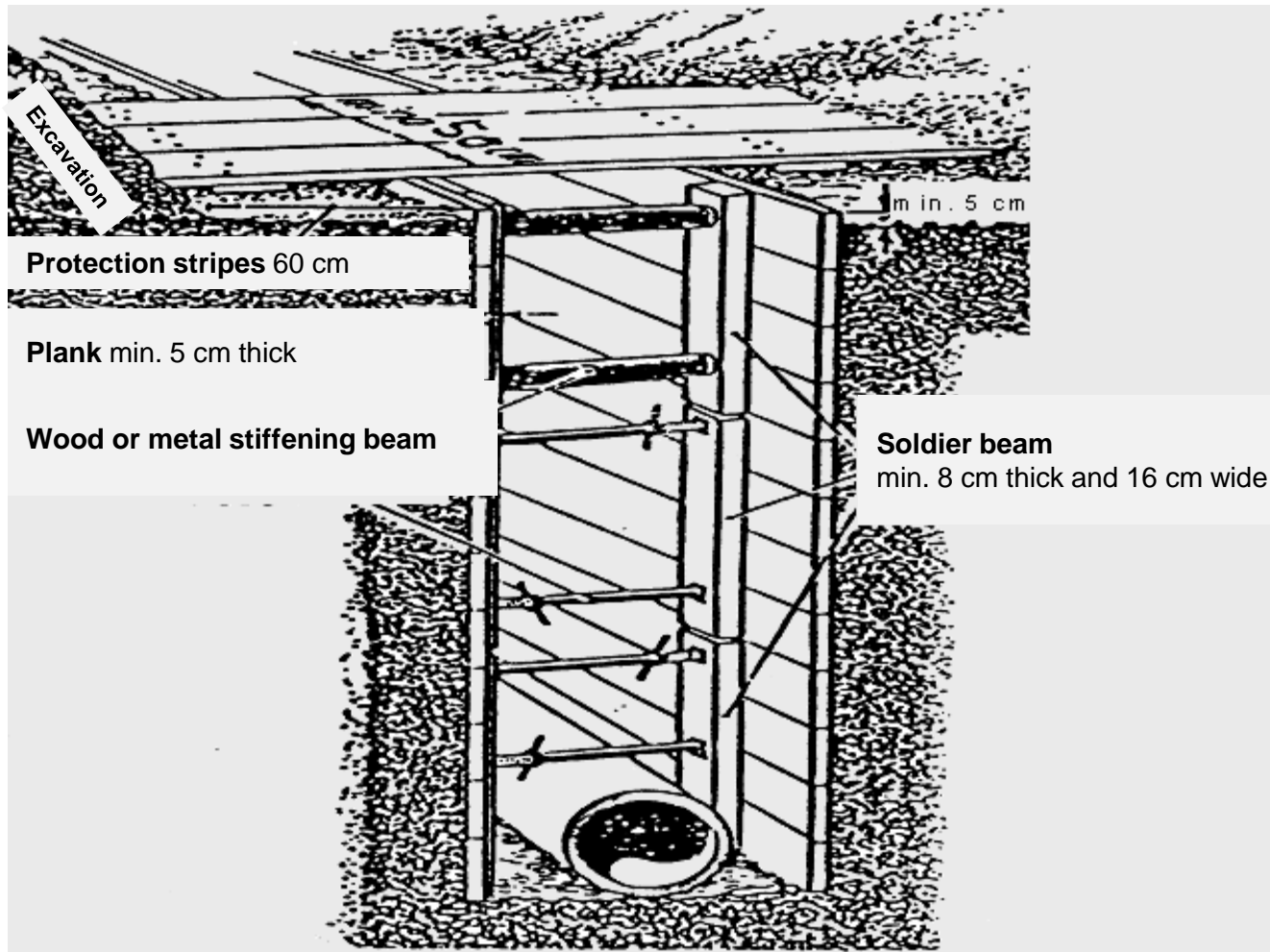


## Piping materials:

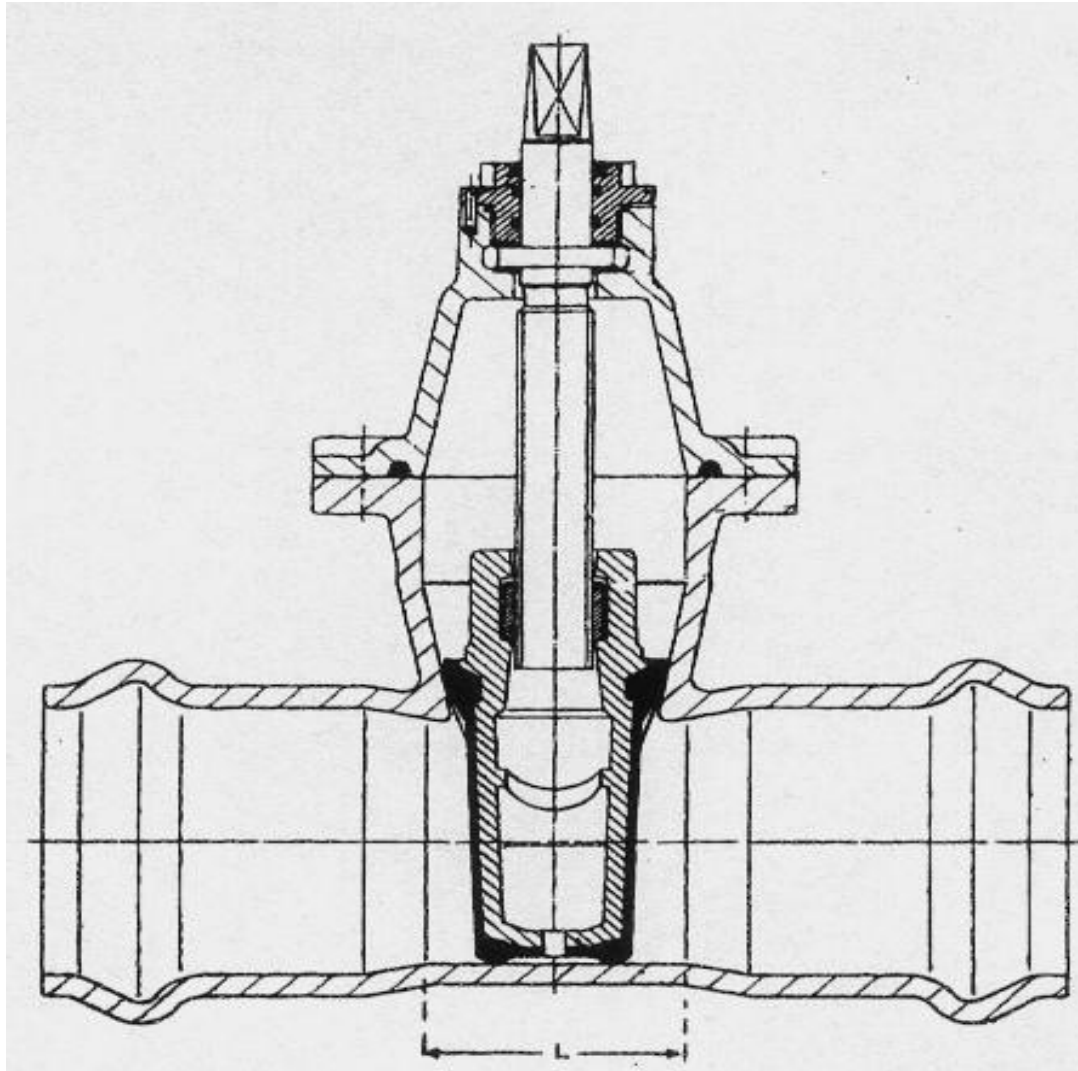
- Grey iron-cast pipe (*Graugussrohr*)
- Steel pipe (*Stahlrohr*) (at high pressures)
- Asbestos cement pipe (*Asbestzementrohre*) (forbidden since 1989)  
nowadays fibre-cement-pipes
- Pre-stressed concrete pressure pipe (*Spannbetondruckrohr*) and reinforced concrete pressure pipe (*Stahlbetondruckrohr*) (for big diameters (2.25 m), e.g. long-distance pipe line)
- Plastic pipes (*Kunststoffrohre*) (PVC and PE, corrosion-resistant and hydraulically smooth)

- Minimal depth of cover of pipes 1.5 m (frost danger).
- Marked-out pipe lines to be kept free from tree planting.
- Pipe must be laid out properly.
- Pipe must be cleaned carefully.
- Afterwards pressure proof for 24 h with nominal pressure + 5 bar extra, valid pressure decrease 0.1 bar with PN 10.
- Before start-up flush pipeline thoroughly and disinfect with chloric Water. Chlorine solution should have a reaction time of 24 h. Afterwards pipes have to be rinsed.

# Horizontal trench lining



# Valve with push-in, flexible joint



# Labeling of water pipes DIN 4067

**This label contains the following information**

Water pipe  
Serial number

Type of fitting

Nominal size

Position of fitting  
1,8m to the right

4.7 m to the front

The image shows a blue rectangular label with white text and numbers. The label is divided into several sections. At the top, it says 'Wasser Nr 320'. Below that, it says 'S 200'. In the middle, it says '1,8 T'. At the bottom, it says '4,7'. Lines connect the text on the left to the corresponding parts of the label.

This label contains the following information

Hydrant

Nominal size of the pipes

Serial number in the system

Position of hydrant  
1,2 m to the right

6,1 m to the front





**This label contains the following information:**

Sewage \_\_\_\_\_

Serialnumber in the system \_\_\_\_\_

Valve type \_\_\_\_\_

Nominal size of the pipes \_\_\_\_\_

Position of fitting  
16,3m to the right \_\_\_\_\_

17,4m to the front \_\_\_\_\_

Information for the control of operations and special indications e.g. name of operator and tel. number in case of emergency \_\_\_\_\_

Abwasser

258083

S 1200

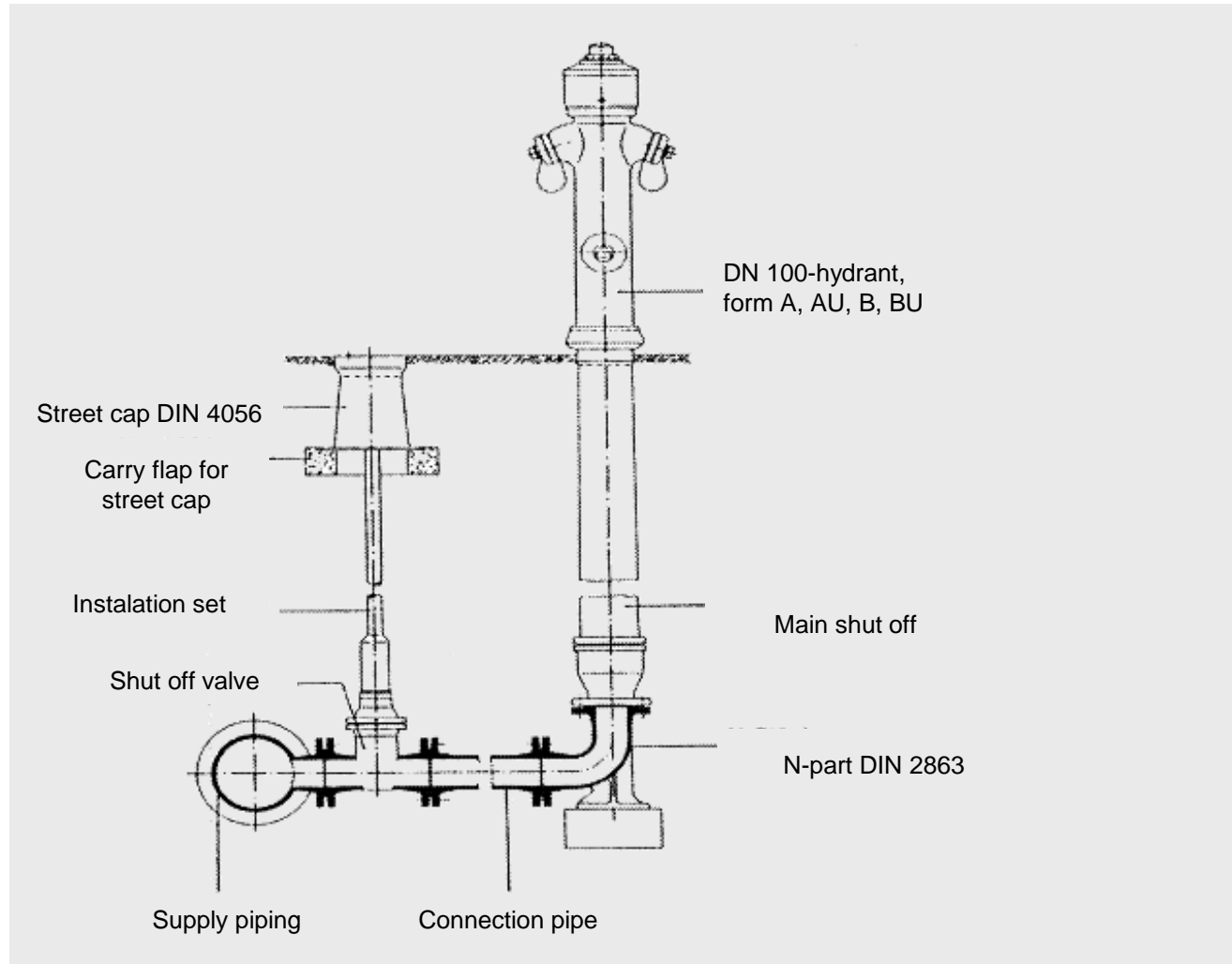
16,3

17,4

Gemeinde  
Gr. Nordende

# Piping system equipment

## Fire-fighting-hydrant

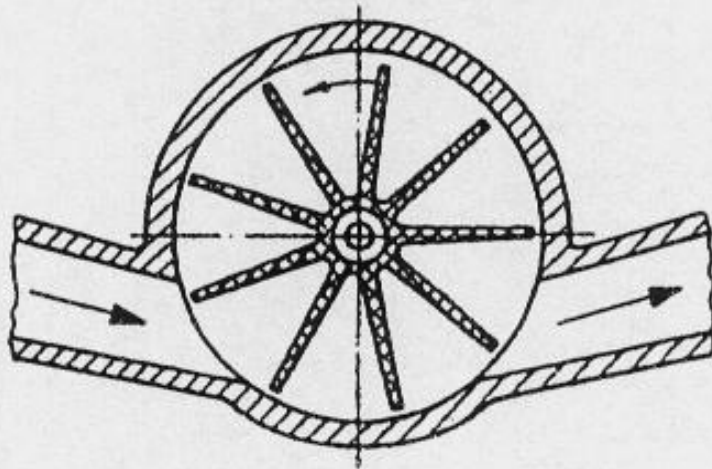
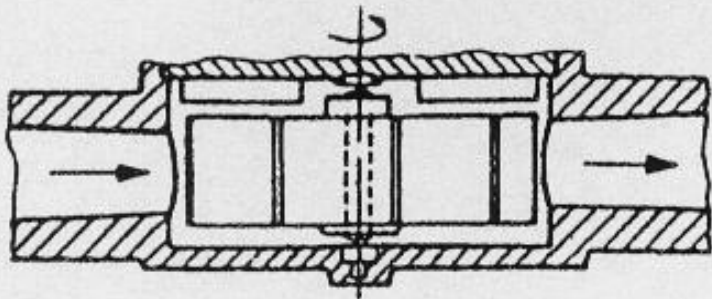


Water meters are subject to the law over the measuring and calibration of 1970.

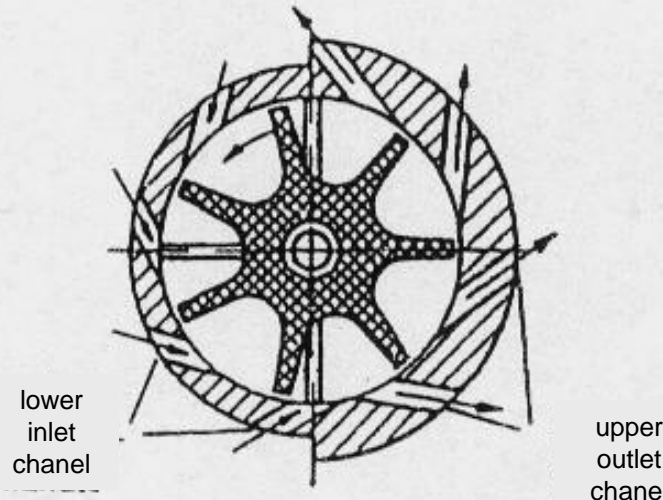
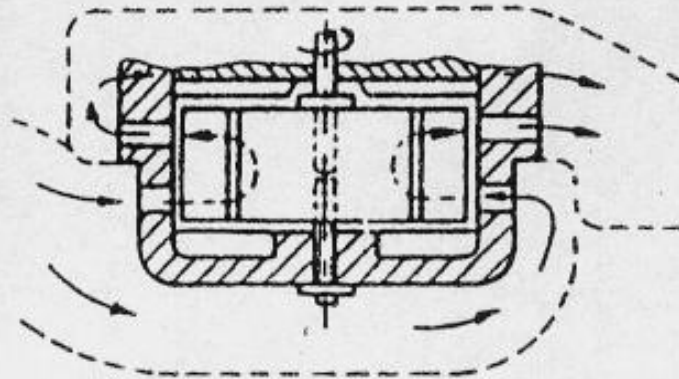
According to this law must all in the trade of water used water meters be calibrated or certified by a state-approved inspection station.

# Wheel counter (*Flügelradzähler*)

One-stream wheel / impeller counter



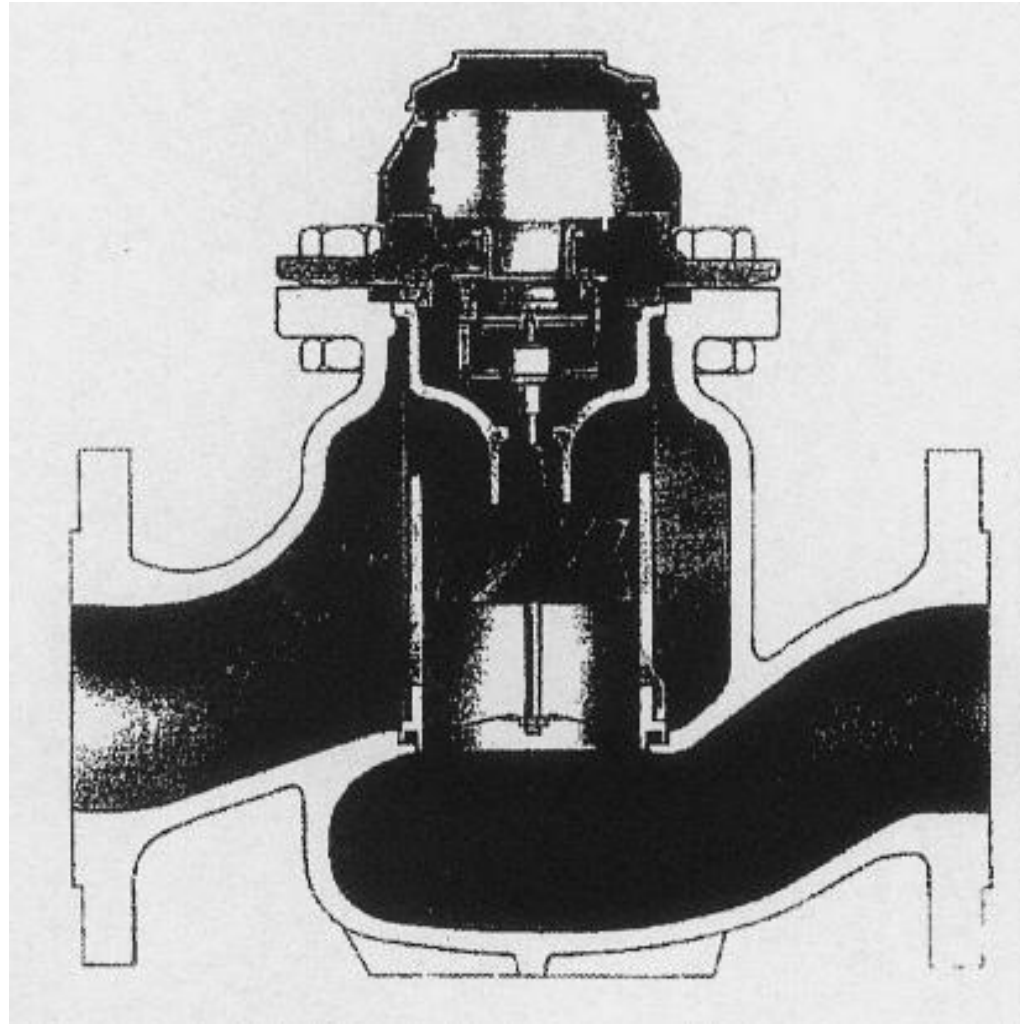
multiple-stream wheel / impeller counter



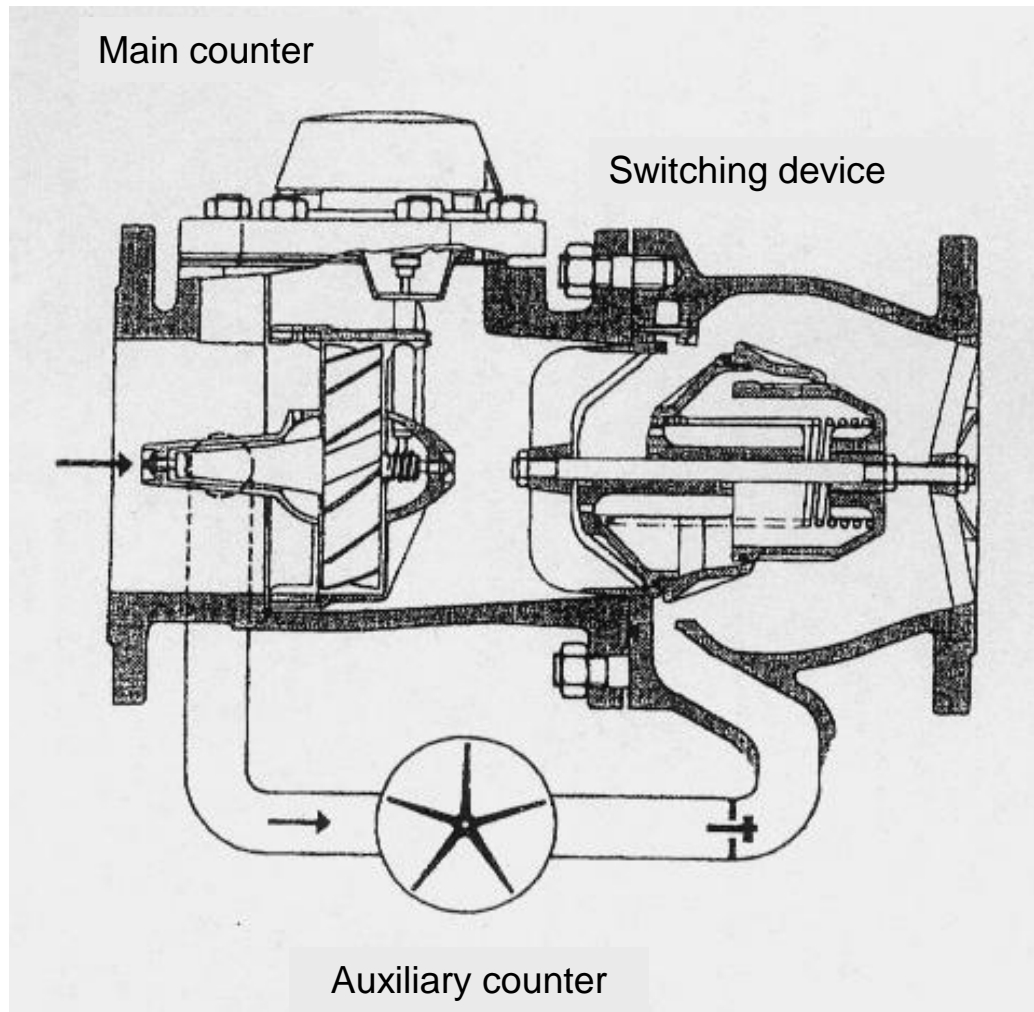
lower  
inlet  
channel

upper  
outlet  
channel

# Woltmann counter

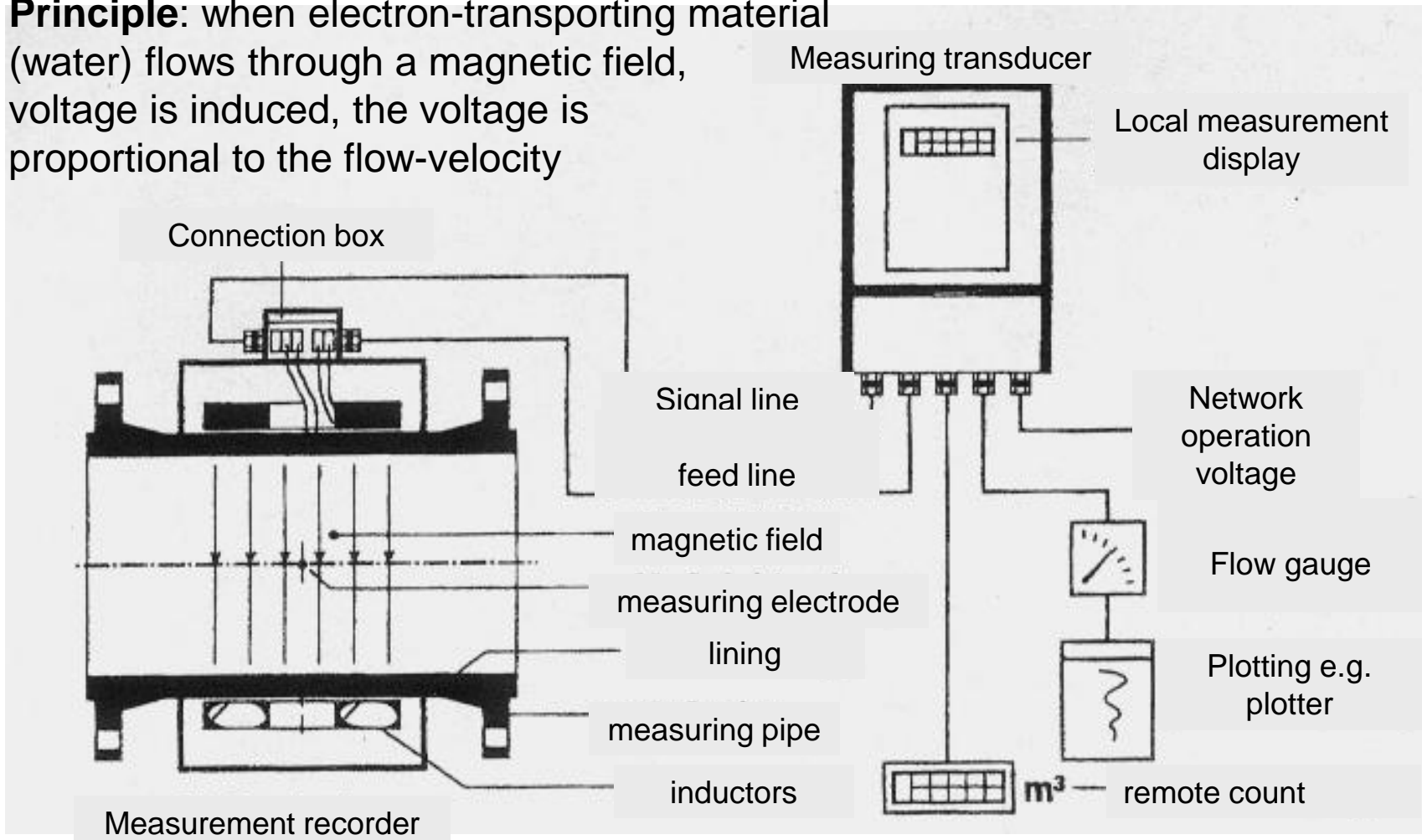


# Compound counter (*Verbundwasserzähler*)

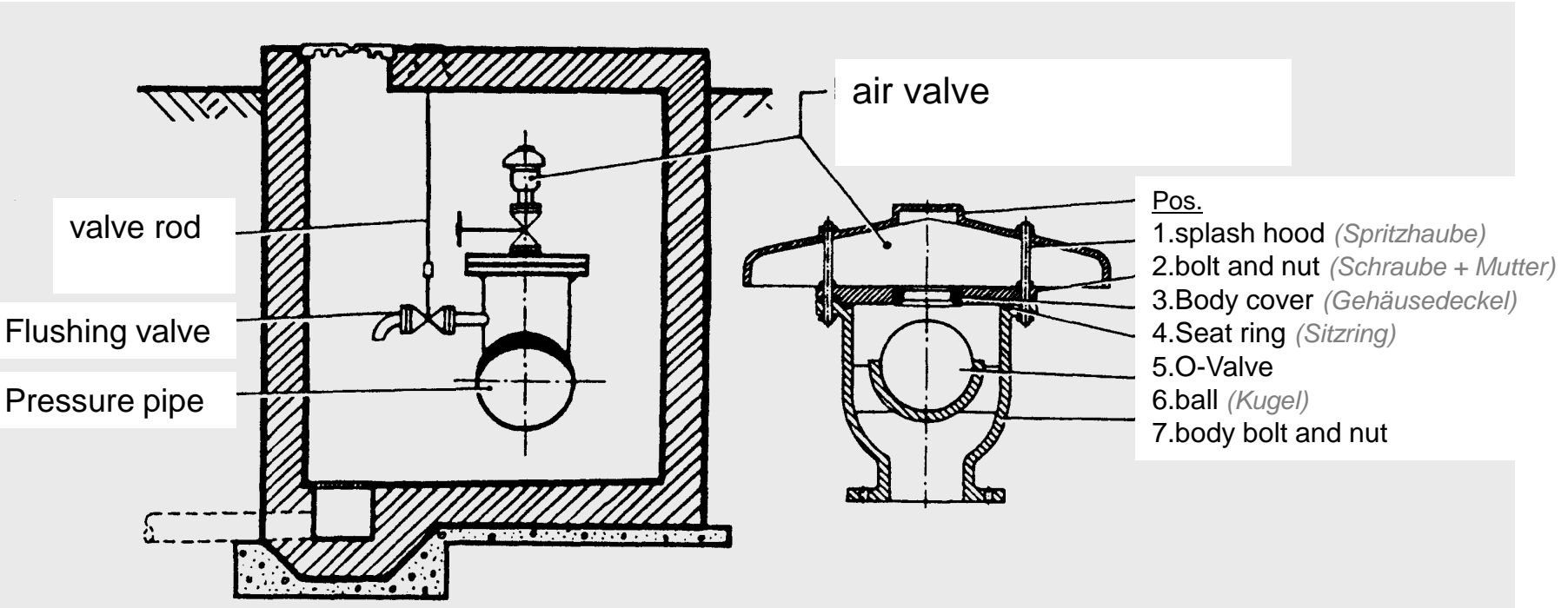


# Magnetic inductive flow measurement

**Principle:** when electron-transporting material (water) flows through a magnetic field, voltage is induced, the voltage is proportional to the flow-velocity

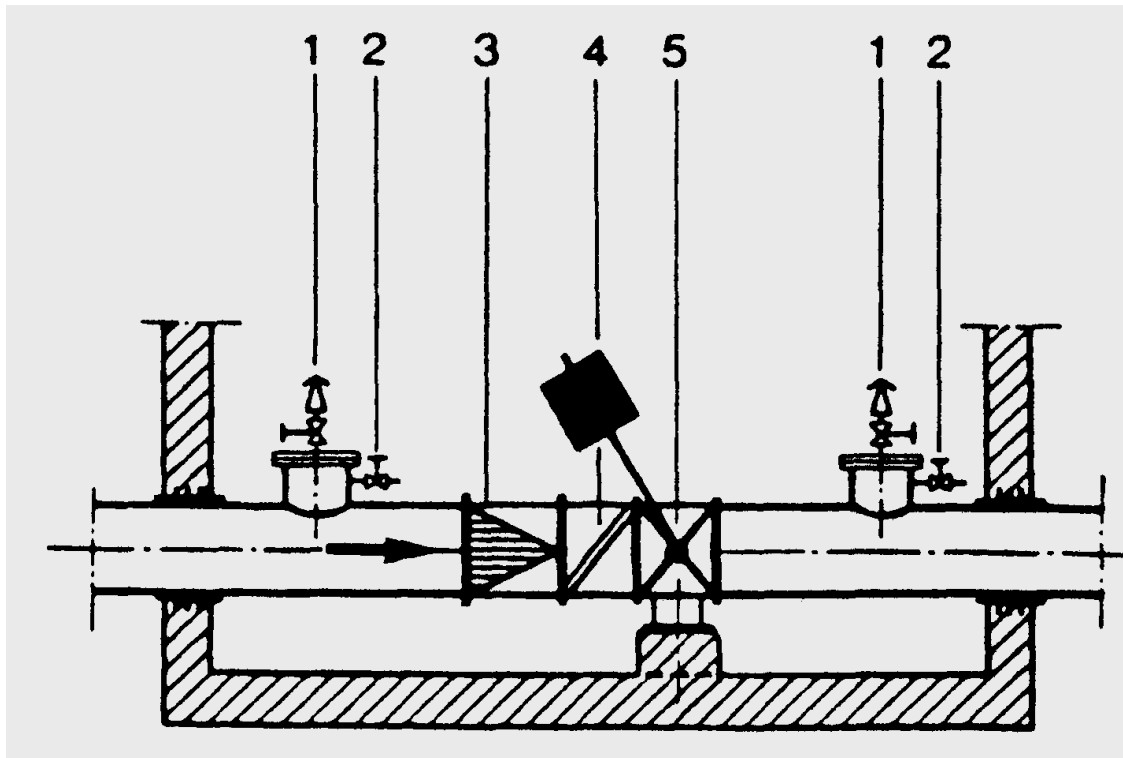


# Aeration and degassing valves





# Example for pipe burst protection



1. Air valve
2. Manual ventilation system
3. Flow measurement device
4. Disassembling device
5. Pipe burst protection

„instrument“