# **Urban Water Management**

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## **Overview**

## **Contents today: Drainage**

#### Waste water plus storm water

- amount and pollution
- drainage systems
  - $\rightarrow$  combined systems
  - $\rightarrow$  separate systems
- dimensioning of pipes
- storage
  - $\rightarrow$  stormwater overflow tanks
  - $\rightarrow$  stormwater retention tanks
- dimensioning of tanks

#### **Domestic** plus industrial plus external

amount (domestic)

= depending on habitants connected to the sewer system

= equivalent to water consumption (disposed = delivered)

consumption e.g. 140 l/(C\*d) for design: often higher (safety margin)

#### **Domestic** plus industrial plus external

- amount (industrial)
  - = individual, often expressed in "population equivalents" (PE)

PE<sub>ind.</sub> = waste water of plant / waste water per capita Example: discharge of industrial plant: 6000 l/d

 $PE_{ind.} = 6000 / 150 = 40$ 

• amount (external)

= water not wanted in the system

Origin: cracked pipes, incorrect connections etc.

#### **External water**

#### Where does it come from?



#### **Domestic** plus industrial plus external

• pollution (domestic)

mean value (rule of the thumb) = 600 mg/l COD load per capita: 150 l/d \* 600 mg/l = 90 g/d COD

• pollution (industrial)

= individual, often expressed in "population equivalents" (PE)

PE<sub>ind.</sub> = pollution load of plant / pollution load per capita

Example: pollution load of industrial plant: 6000 l/d \* 1200 mg/l COD = 7200 g/d COD $\text{PE}_{\text{ind.}} = 7200 / 90 = 80$ 

• pollution (extraneaous)

= generally not accounted for, assumed to be "clean"

#### **Design runoff**

espec. for subcatchments: population density (counted or assumed) is used (total or sub-catchment area is easy to obtain)

- $Q_{d24}$  = mean discharge per day
- Q<sub>dx</sub> = daily discharge compressed into x hours

#### **Daily variations of runoff and concentration**



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#### **Design runoff**

espec. for subcatchments: population density (capita per ha)
 (counted or assumed) is used
 (→ total or sub-catchment area is easy to obtain)

- Q<sub>d24</sub> = mean discharge per day
- Q<sub>dx</sub> = daily discharge compressed into x hours

often used: normalized values (per ha):

 $q_{d24} = I/(C^*d) * C/ha * d/86400 s = I/(s^*ha)$ 

with freshwater consumption = 150 I/(C\*d) and 50 C/ha:

 $q_{d24} = 150 * 50 * 1 / 86400 = 0,0868 I / (s*ha)$ 

rule of the thumb: 0,1 l(s\*ha)

## **Storm water**

#### **Design runoff**

- no defined design load
- rain is a stochastic entity
- dimensioning not for maximum possible load (inefficient from an economical viewpoint)
- as in hydrology in general:
  - feature / attribute
     e.g. water level, volume, runoff
     plus
  - recurrence interval of exceedence
     T [a]

## **Storm water**

#### Design

- Define: frequency / recurrence interval of what?
- Find: design runoff
- Choose: appropriate diameter / profile (diameter depends on runoff and slope)
- Frequency of a limit state, e.g.
  - the pipe surcharging
  - flooding

water level at pipe crown or higher

water level at surface

→ allow exceedence of limit state at recurrence interval / with defined frequency



## History of urban hydrology and sewer design

Ancient times	Water supply Drainage of waste water Stormwater drainage as a by-product	
Modern Urban Drainage	1830 1840-50 1842 1843	Cholerac epidemic in London Sewersystem in London Great fire in Hamburg Design of a sewer system

#### **Industrielle Revolution**

- since 1850: Systematic determination of required diameters depending on
  - drained area
  - connected habitants

## History of urban hydrology and sewer design

- 1851 Mulvaney Relation between rainfall, runoff and area Principle of the rational formula
- 1889 Kuichling Rational Formula Sewer system for Rochester, NY (1877 - 1889)
- 1906Lloyd-DaviesRational formula for the anglo-saxon sphere
- **1922** Imhoff: German version of the rational formula
- 1940 Reinhold: statistical rain data analysis
   Definition of time coefficient φ to allow for change of charted base rainfall intensity r15,1 (15 min, once a year) dependent on duration and frequency

## **Rational formula**

$$Q_p = C \cdot i_T \cdot A$$

- $Q_p$  Design peak flow
- C Proportion of effective rainfall
- $i_{T}$  mean rainfall intensity of decisive duration and design frequency
- A Catchment area above design point
- $t_{\,f} \quad \text{Time of flow} \quad$



## **Storm water**

## Design

- Design peak flow is dependent on rainfall
- Assumption: rainfall frequency = runoff frequency
- Consequence: rainfall statistics are needed



- Needed: long time series of rainfall recordings
- one of the possible ways:
  - choose a duration
  - move duration-wide window over time series sequence of data
  - collect all extreme rainfall sums within window

#### **Overlapping rainfall sums**



- Needed: long time series of rainfall recordings
- one of the possible ways:
  - choose a duration
     move duration-wide window over time series sequence of data
  - collect all extreme rainfall sums within window
  - analyse statistically



- Needed: long time series of rainfall recordings
- one of the possible ways:
  - choose a duration
  - move duration-wide window over time series sequence of data
  - collect all extreme rainfall sums within window
  - ✤ analyse statistically
  - repeat for other durations
  - smooth parameters over duration
  - result: Intensity-Duration-Frequency

curves  $\rightarrow$  IDF curves



## **Statistical rainfall**

1940 Reinhold

$$r_{D,f} = r_{15,1} \cdot \left\{ \frac{38}{D+9} \cdot \left( \frac{1}{\sqrt[4]{f}} - 0,369 \right) \right\}$$

time coefficient  $\phi$ 

1990/97 KOSTRA ,,Coordinated statistical and regionalisation analysis "

> Statistical rainfall amounts for: D = 15, 60 min, 12, 24, 48, 72 hf = 1, 0.1, 0.01 (0.5, 0.2) [1/a]

**Rainfall statistics** 

**KOSTRA demonstration** 

#### **Open channel flow**

Velocity:

$$v = \frac{4 \cdot Q}{\pi \cdot D^2}$$

$$f = \lambda = \text{friction factor} \quad v = \text{velocity}$$

$$D = \text{diameter}$$
(substitute with 4\*R<sub>H</sub> for non-circular profiles)

Darcy-Weisbach:

$$I_e = I_b = I_s = f \cdot \frac{1}{D} \cdot \frac{v^2}{2g}$$

energy gradient = bed slope = surface slope  $\rightarrow$  stationary flow

#### **Prandtl-Colebrook:**

$$\frac{1}{\sqrt{f}} = -2\log_{10}\left(\frac{\varepsilon}{3,71 \cdot D} + \frac{2,51}{\text{Re}\sqrt{f}}\right) \qquad \begin{array}{l} \varepsilon = k_b = \text{roughness height} \\ \text{Re} = \text{Reynolds number} \\ v = \text{kinematic viscosity} \end{array} \qquad \begin{array}{l} \text{Re} = v \cdot \frac{D}{v} \\ \end{array}$$

### **Dimensioning of pipes**

wanted:diameter Dgiven:design runoff Qgiven or choose:gradientroughness height

should not be less than 0,01 % (1 in 10.000) typically  $k_b = 0,25 \dots 1,5$  [mm]

Solution:

by iterative calculation or tables or nomograms







#### **Design principles**

#### sufficient minimum velocity

v > 0,2 m/s to avoid deposition
and to keep the settleable solids in suspension
→ gradient: I > 0,01% (1 in 10000)

#### appropriate diameter and profile

sufficient water depths at minimum flow (during the night)

pipe crown line continuation

when diameter increases

or

pipe base line continuation

when diameter decreases









#### **Separate systems**

#### a) the sanitary sewer system

- Design load: well defined by
  - water consumption
  - connected habitants
  - additional dischargers (industry)
- uncertainty: external water
- branched system with treatment plant as endpoint
- impact on receiving waters
  - quasi stationary flow
  - quasi stationary concentrations of pollutants

#### **Separate systems**

#### b) the storm water sewer system

- Design load: dependent on
  - rainfall statistics
  - design frequency
  - connected area
- distributed system with multiple endpoints
- impact on receiving waters
  - hydraulics
  - pollution

# Seperate systems: storm water sewer system Impact on receiving waters

- Hydraulic impact
  - direct discharge of stormwater runoff into the river
    - $\rightarrow$  high peak flows
    - $\rightarrow$  hydraulic stress
  - counter action: storm water detention tanks / basins
    - $\rightarrow$  temporary storage of storm water
    - $\rightarrow$  reduction of peak flow
- Pollution
  - generally no treatment
  - storm water is <u>not</u> clean

#### **Storm water pollution**

 For impervious areas (example: Germany): assumed wash-off:

600 kg COD per ha per year

with annual rainfall = 800 mm and storm water runoff = 560 mm

 $\rightarrow$  <u>mean</u> storm water concentration:

$$C_r = \frac{600 \ kg \ /(ha \ /a)}{560 \ l \ /m^2} = 107 \ mg \ /l \quad COD$$

- actual concentration varies
  - from event to event
  - within the event

#### **Combined systems**

- Design load: combined loads from
  - waste water
  - storm water
- distributed system with multiple endpoints (overflow outlets)
- impact on receiving waters
  - hydraulics
  - pollution
  - quasi-stationary as well as sporadic

#### **Combined systems**

- Design load:
  - waster water <u>plus</u> storm water
- Treatment plant has limited capacity, generally 2 .. 3 times dry weather flow
- Excess runoff in the sewer system:
  - has to be disposed by "overflow" into receiving waters (river)

intended, designed and appropriately constructed

- at the treatment plant or on the way
- Combined sewer overflow is a non-neglectable pollution source
   = waste water diluted by storm water
- generally no bio-chemical treatment

No treatment at all ???