PAPER • OPEN ACCESS

Determination the installation efficiency of the evaporative air cooling in the greenhouse by temperature-moisture regime

To cite this article: A Anarbaev et al 2020 IOP Conf. Ser.: Earth Environ. Sci. 614 012026

View the article online for updates and enhancements.



This content was downloaded by o.tursunov@ from IP address 213.230.109.7 on 18/12/2020 at 09:09

IOP Conf. Series: Earth and Environmental Science 614 (2020) 012026 doi:10.1088/1755-1315/614/1/012026

Determination the installation efficiency of the evaporative air cooling in the greenhouse by temperature-moisture regime

A Anarbaev¹, O Tursunov^{1,2,3*}, R Zakhidov¹, D Kodirov¹, U Vakhidov¹, E Bozorov⁴, G Tuhtaeva⁵, and A Babaev¹

¹Department of Power Supply and Renewable Energy Sources, Tashkent Institute of Irrigation and Agricultural Mechanization Engineers, 100000 Tashkent, Uzbekistan ²School of Mechanical and Power Engineering, Shanghai Jiao Tong University, 200240 Shanghai, China

³Research Institute of Forestry, 111104 Tashkent, Uzbekistan

⁴Department of Automation and Control of Technology Process, Tashkent Institute of Irrigation and Agricultural Mechanization Engineers, 100000 Tashkent, Uzbekistan ⁵Department of Hydrology and Ecology, Bukhara branch of Tashkent Institute of Irrigation and Agricultural Mechanization Engineers, Bukhara, Uzbekistan

^{*}Email: anizan6004@mail.ru

Abstract. The results of theoretical studies and experiments of the developed exhaust ventilation system with direct evaporative air- cooling with using "wet mats" are given. It has shown sufficient efficiency with increasing quality of flower cutting in the summer months. The effect of moisture on the operation of this system was studied. It is established that the heat absorption capacity of air directly depends on its temperature and relative humidity. It is also determined that the temperature of leaves and flowers in summer is usually $2 \div 7$ °C greater than the air temperature in the greenhouses. In an experimental greenhouse, according to the results of experiments, the effectiveness of the developed installation for evaporative cooling of its operation was determined.

1. Introduction

In climatic zones where the maximum summer temperature is stably above 35° C, and the internal temperature of the greenhouse for a long period of time exceeds the mark of 30°C, it is advisable to combine the exhaust ventilation system with evaporative air cooling systems [1, 2]. The use of evaporative cooling with wet mats increases the quality and, consequently, the price of cutting flowers in the summer months [3].

Modern methods of growing cut flowers of roses include, on the one aspect, effective regulation of the microclimate in greenhouses throughout the year [4], and on the other aspect, technical re-equipment of greenhouses for low energy-intensive technology [5]. At the same time, during the blooming of the buds, the temperature needs to be slightly lowered, during the flowering period – increased [6]. The humidity level should be around 70 percent [7]. Additional lighting is required in winter [8]. In summer, on the contrary, it is necessary to slightly shade the bushes with curtains [9]. Among other things, regular



ICECAE 2020	IOP Publishing
IOP Conf. Series: Earth and Environmental Science 614 (2020) 012026	doi:10.1088/1755-1315/614/1/012026

ventilation is required. The problem with cooling greenhouses is that at high summer air temperatures in greenhouses, the length of the shoots and the diameter of the flowers of roses are sharply reduced [10].

The system of wet mats (the so-called "wet mattresses") is a new technical direction for reducing the air temperature in greenhouses in the summer. The mats are installed in special openings in the side glazing of greenhouses, facing the direction of the prevailing winds in the summer [11]. On the opposite side of the greenhouse, in the openings of the side fence, low-speed fans with a blade diameter of up to one meter and low-power electric motors are installed [12].

The fans work to exhaust air from the greenhouse. Moisture is sprayed onto the mats and cooled air is supplied to the greenhouse by lowering the temperature of the air passing through the wet mats. Despite certain energy costs, such a system effectively reduces the air temperature in greenhouses. During this process, the greenhouse vents are in a closed position [13].

For the roses, the air temperature in greenhouses in summer up to 27 ° C allows you to get high-quality cut flowers. In conditions of high summer temperatures greater 40° and low air humidity, a system of additional air humidification is used on the rose crop [14].

Fog-forming nozzles (foggers) spray water to particles with a diameter of less than 100 microns [15], which does not lead to the formation of drip moisture on the leaves and, as a result, the leaf surface of the roses. The use of such nozzles allows not only to effectively reduce the temperature of the leaves due to the evaporation of moisture from their surface, but also saves the energy expended by plants to evaporate water to cool the leaves. The temperature of leaves and flowers in summer is usually 2-7 $^{\circ}$ C greater than the air temperature in greenhouses [16].

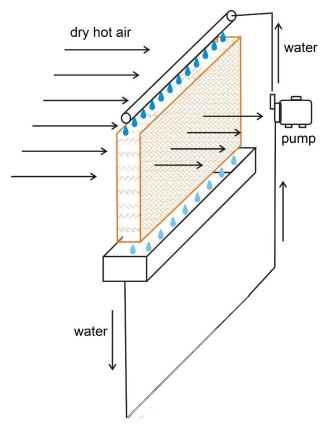


Figure 1. The construction of wet mats using energy-saving technology of indirect evaporative cooling in poultry farm

The efficiency of the exhaust fans is significantly affected by the degree of wear of the drive belts, as well as the presence of a large amount of dust on the fan blades and shutters.

IOP Conf. Series: Earth and Environmental Science 614 (2020) 012026 doi:10.1088/1755-1315/614/1/012026

A worn-out belt, while consuming the same (with a new belt) amount of energy, is not able to provide 100% fan performance. And even a 10% loss in capacity "costs" the 3^{0} C cooling effect of evaporative cooling exhaust ventilation based on evaporative cooling. Dust adhering to the blades during operation can change the aerodynamic characteristics of the blades and reduce air exchange by 30% [17].

An evaporative cooling unit was installed and investigated in a greenhouse located in the village of Tinchlik k.f.j., district - Yukori Chirchik, Tashkent region with an area of $47 \times 64 \text{ m}^2$ (flower farm LLC "Xamro-Mirodil").

2. Materials and Methods

Evaporative cooling is based on the principle of heat by evaporated liquid, the so-called adiabatic cooling [18].

With an increase in the absolute moisture content, the air temperature rises, as a result of which, simultaneously with humidification, excess heat is assimilated without artificial cold.

At the same time, the air humidity in the greenhouse has a very strong effect on the operation of any cooling system.

The heat absorption capacity of air is directly related to its temperature and relative humidity. The higher it is, the more difficult it is to achieve the desired effect [19-23].

During the hot season, tap water is supplied to the trays of the evaporative apparatus, which moistens hygroscopic material (wet mats) in the facade section.

The supplied outside air in the amount of 2500 m^3 per hour passes through the moist material and enters to the greenhouse.

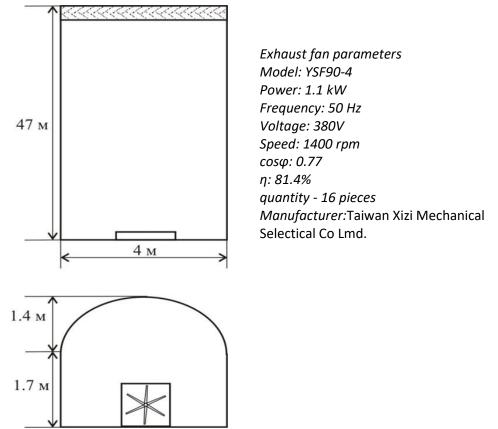


Figure 2. Installation of evaporative cooling in the experimental greenhouse of LLC "Xamro-Mirodil"

For the installation of direct evaporative cooling system devices, the territory is divided into 16 sections 4 m wide with a total area of the flower farm of $47 \times 64 \text{ m}^2$.

IOP Conf. Series: Earth and Environmental Science 614 (2020) 012026 doi:10.1088/1755-1315/614/1/012026

One of the main characteristics of a wet mat evaporative cooler is its efficiency E [24-26]. As for other heat and mass transfer installations, the value of E for the coolers of the type under consideration is determined from the ratio

$$E = \frac{t_{air_{inlet}} - t_{air_{outlet}}}{t_{air_{inlet}} - t_m} \tag{1}$$

IOP Publishing

For an ideal evaporative cooler, E should be one. In the process of ideal adiabatic evaporation of water, the air temperature at the outlet of the cooler is equal to its adiabatic wet bulb temperature, i.e $t_{air_{out}} = t_m^{ad}$, and hence the relative humidity $\varphi = 1$, while the analytical formula for the specific enthalpy of humid air at the outlet from the evaporative cooler

$$I_{out}^{ab} = 1,0048 \cdot t_{M}^{ab} + \left(1555,75 + 1,146 \cdot t_{M}^{ab}\right) \left(\frac{P_{\delta}}{4,579 \cdot 10^{\frac{7,45r_{m}^{ab}}{235 + r_{m}^{ab}}} - 1\right)^{-1}$$
(2)

Based on the calculated data according to (2), an approximation dependence was determined at a given value of $P_b = 715$ mm Hg. st., typical for the Tashkent region.

$$t_m^{ad} = A \cdot \ln I_{out}^{ad} - B \tag{3}$$

here A and B are coefficients depending on P_b . According to the results of calculations with $P_b = 715$ mm Hg: st. A = 18.853 and B = 57.25.

At numerically calculating the maximum possible temperature value of wet mats cooled in evaporative coolers, it is required to determine the values $t_m = \frac{t_m^{ad}}{t_m}$ at the outside air temperature $\frac{t_{air}}{t_{air}} = 35$ °C, $\varphi_0 = 70\%$ $P_b = 715$ mm Hg.st.

By equation (2), it is determined the enthalpy of humid air at the outlet from the evaporative cooler of wet mats

$$I_{out}^{ab} = 1,0048 \cdot 35 + \left(155575 + 1,146 \cdot 35\right) \left(\frac{715}{4,579 \cdot 10^{\frac{7,4535}{235+35}}} - 1\right)^{-1} = 68.92 \text{ kJ / kg dry air}$$

By equation (3), we determine the adiabatic temperature of a wet thermometer

$$t_m^{tm} = 18.853 \cdot \ln 68.92 - 57.25 = 22.55 \,^{\circ}\text{C}$$

The following formula allows you to define the influence of the irrigation coefficient (μ) of wet mats on the temperature of the cooled air

$$t_{air_{out}} = t_m + \left(t_{air} - t_m\right) \cdot e^{-\frac{\left(u_k + \rho_p, r\right) \cdot u \cdot \sigma}{\mu \cdot \vartheta_{Wa} \cdot \rho_{Wa} \cdot C\rho_{air}}} \tag{4}$$

The values of α_{κ} and β_p for the irrigated layer of the wet mats system with a diameter of 0.135 mm, a length of 200 mm, $a = F_{HE}/V=16000 \text{ m}^2/\text{ m}^3$ can be selected respectively 58.15W/(m² °C), 120 kg/(m²h) [3].

According to the results of the calculations performed to determine
$${}^{cair_{out}} = 58 \text{ W} / (\text{m}^{2} \,^{0}\text{C}),$$

 $\beta_{pr} = 120 \text{ W}/(\text{m}^{2} \,^{0}\text{C}), a = 16000 \text{ m}^{2} / \text{m}^{3}, \delta = 0.002\text{m}, \mu = 0.1, \text{ density humid } \rho_{wa} = 1.25\text{kg} / \text{m}^{3} \text{ and heat}$
capacity ${}^{Cp}_{air} = 4186.8$ the value of ${}^{tad}_{m}$ at ${}^{t}_{air} = 35^{\circ}\text{C}$ and ${}^{t}_{m} = 22.55^{\circ}\text{C}$ is
 $t_{air_{out}} = 22.5 + (35 - 22.55) \cdot e^{-0.12.0 \cdot 1.25 \cdot 4186.8} = 22.55 + 12.45 \cdot e^{-2.0407} = 24.19 \,^{\circ}C$
The value of the thermal efficiency of the evaporative water cooler, determined by (4), is
 $F = {}^{35 - 24.19} = 0.70$

$$E = \frac{35 - 24,19}{35 - 22,55} = 0,79$$

3. Results and Discussions

Measurements were made of the temperature and humidity parameters of the air inside the greenhouse during the operation of the evaporative air cooling system, as well as the relative humidity of the air.

IOP Publishing

Figure 3 shows the temperatures and humidity inside the greenhouse when the evaporative cooling unit is operating, cyclical changes in the daily average temperature versus the cyclical changes in relative humidity.

Obviously, during the hottest hours of the day, the relative humidity drops to below 50%. Under such conditions, the developed evaporative-type coolers consistently increase their efficiency by lowering and lowering the air temperature in the greenhouse, or maintaining it at the desired level throughout the day using sensors installed in the greenhouse.

However, the relative humidity decreases as the temperature rises. The absolute amount of water vapor in the air changes insignificantly with temperature changes.

Considering that the absolute humidity remains approximately constant throughout the day, measurements show that as the outside temperature rises, the temperature indicated by the wet bulb thermometer decreases significantly [23]. For example, with an absolute humidity of 0.015 kg / kg of air and a relative humidity of 75%, the outdoor temperature drops to 25 ° C. At 36 $^{\circ}$ C the relative humidity will be 40%.

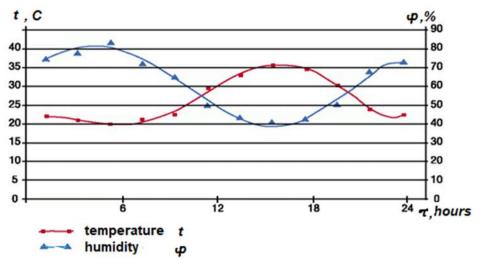


Figure 3. The cycle of temperature and humidity during the summer day inside the experimental greenhouse during the operation of the evaporative cooling unit

4. Conclusions

The thermal efficiency of the evaporative water cooler is 0.79.

At the same time, during the operation of the evaporative air cooling system, it was possible to achieve the optimal values of temperature (up to 27^{0} C) and relative humidity (about 70%) when growing roses in a greenhouse.

The tests carried out have shown sufficient efficiency of the developed direct evaporative cooling unit for use at farm facilities.

References

- [1] Okanlawon SA, Olorunnisola AO 2017 Agric. Eng. Intern.: CIGR J. 19(1) 178–186.
- [2] Zakhidov RA, Anarbaev AI 2014 *Applied Solar Energy* **50** 178-183.
- [3] Ndukwu MC, Manuwa SI 2014 Agric. Eng. Intern.: CIGR J. 7(5) 85–102.
- [4] Korir MK, Mutwiwa UN, Kituu GM, Sila DN 2017 Agric. Eng. Intern.: CIGR J. 19(1) 162–168.
- [5] Amer O, Boukhanouf R, Ibrahim HG 2015 Int J Environ. Sci. Dev. 6(2) 111–117.
- [6] Misra D, Ghosh S 2018 Agric. Eng. Intern.: CIGR J. **20**(11) 1–14.
- [7] Chijioke OV 2017 J. Greener Sci. Eng. Technol. Res. 7(1) 1–20.
- [8] Zakari MD, Abubakar YS, Muhammad YB, Shanono NJ, Nasidi NM, Abubakar MS, Muhammed AI, Lawan I, Ahmad RK 2016 *J Eng. Appl. Sci.* **11**(4) 2340–2348.

IOP Conf. Series: Earth and Environmental Science **614** (2020) 012026 doi:10.1088/1755-1315/614/1/012026

- [9] Deoraj S, Ekwue EI, Birch R 2015 J. West Indian Eng. **38**(1) 86–95.
- [10] Ogbuagu NJ, Green IA, Anyanwu CN, Ume JI 2017 Nigeria J. Technol. 36(1) 302–307.
- [11] Sibanda S, Workneh TS 2019 *CyTA J. Food* **17**(1) 603–612.
- [12] Ndukwu MC, Manuwa SI, Olukunle OJ, Oluwalana IB 2013 Agric. Eng. Intern.: CIGR J. 15(4) 307–313.
- [13] Babaremu KO, Omodara MA, Fayomi SI, Okokpujie IP, Oluwafemi JO 2018 Int. J. Mech. Eng. Technol. 9(10) 1051–1061.
- [14] Seweh M, Darko JO, Addo A, Asagadunga PA, Achibase S 2016 *Agric. Eng.Intern.: CIGR J.* **18**(2) 435–448.
- [15] Obura JM, Banadda N, Wanyama J, Kiggundu N 2015 Agric. Eng. Intern.: CIGR J. 17(4) 327–336.
- [16] Nkolisa N, Magwaza LS, Workneh TS, Chimphango A 2018 Sci. Hort. 241 131–143.
- [17] Manuwa SI, Odey SO 2012 *Mod. Appl. Sci.* **6**(6) 45–53.
- [18] Basediya ALD, Samuel VK, Beera V 2013 J. Food Sci. Technol. 50(3) 429–442.
- [19] Tursunov O, Dobrowolski J, Zubek K, Czerski G, Grzywacz P, Dubert F, Lapczynska-Kordon B, Klima K, Handke B 2018 *Thermal Science* **22** 3057-3071.
- [20] Tursunov O, Zubek K, Czerski G, Dobrowolski J 2020 J Therm Anal Calorim 139 3481-3492.
- [21] Tursunov O, Zubek K, Dobrowolski J, Czerski G, Grzywacz P 2017 Oil & Gas Science and Technology Rev. IFP Energies Nouvelles 72(6) 37.
- [22] Tursunov O, Isa KM, Abduganiev N, Mirzaev B, Kodirov D, Isakov A, Sergiienko SA 2019 *Procedia Environmental Science, Engineering and Management* **6**(3) 365-374.
- [23] Tursunov O, Abduganiev N 2020 Materials Today: Proceedings 25(1) 67-71.
- [24] Anarbaev A, Tursunov O, Kodirov D, Muzafarov Sh, Babayev A, Sanbetova A, Batirova L, Mirzaev B 2019 E3S Web of Conferences 135 01035.
- [25] Xuan YM, Xiao F, Niu XF, Huang X, Wang SW 2012 Renew. Sustain. Energy Rev. 16(5) 3535– 3546.
- [26] Olosunde WA, Aremu AK, Okoko P 2016 Agric. Eng. Intern.: CIGR J. 18(4) 280–292.