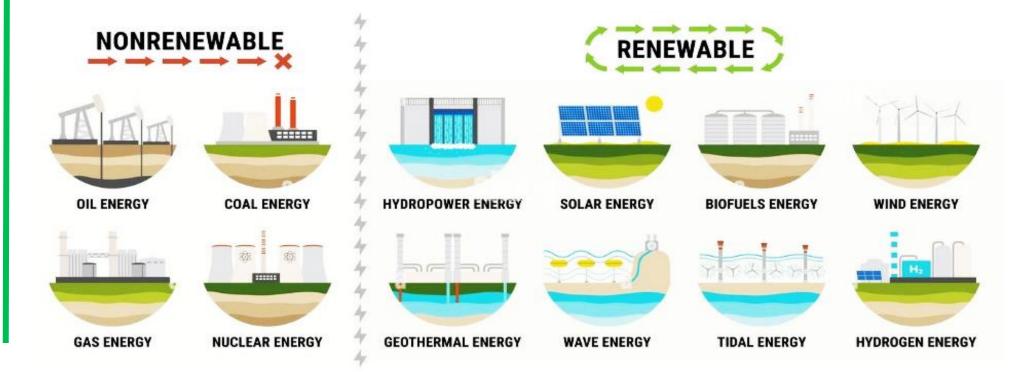


"TITAME" National Research University

PUMPED-HYDRO ENERGY STORAGE



Dilshod KODIROV Professor, Doctor of Science

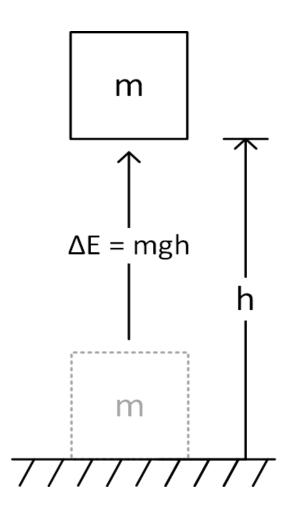
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- Energy can be stored as *potential energy*
- Consider a mass, m, elevated to a height, h
- Its potential energy increase is

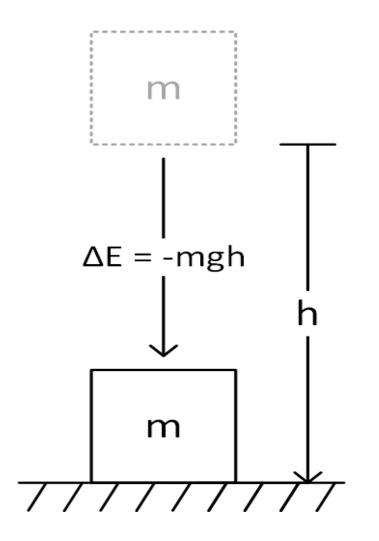
E = mgh

- where $g = 9.81 \, m/s^2$ is gravitational acceleration
- Lifting the mass requires an input of work equal to (at least) the energy increase of the mass
 - We put energy in to lift the mass
 - That energy is stored in the mass as potential energy





- If we allow the mass to fall back to its original height, we can capture the stored potential energy
 - Potential energy converted to kinetic energy as the mass falls
 - Kinetic energy can be captured to perform work
 - Perhaps converted to rotational energy, and then to electrical energy





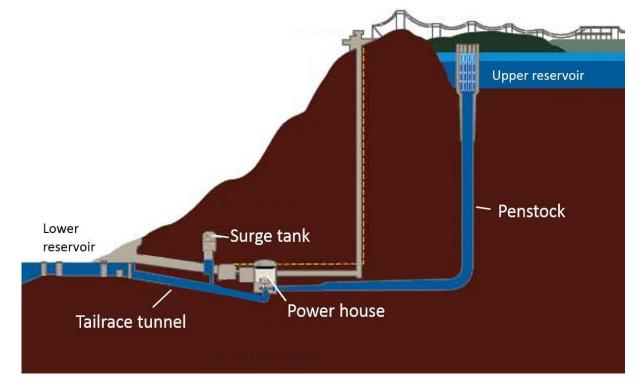
PUMPED-HYDRO ENERGY STORAGE

Renewable Energy Resources

- Potential energy storage in elevated mass is the basis for *pumped-hydro energy storage* (PHES)
 - Energy used to pump water from

a lower reservoir to an upper reservoir

- Electrical energy input to motors converted to rotational mechanical energy
- *Pumps* transfer energy to the water as *kinetic*, then *potential energy*



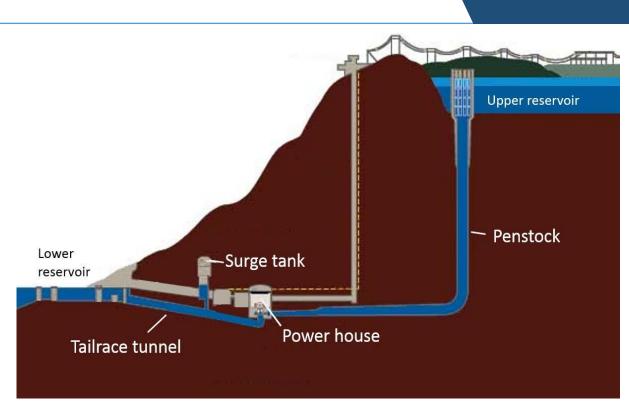


PUMPED-HYDRO ENERGY STORAGE

Renewable Energy Resources

 Energy stored in the water of the upper reservoir is released as water flows to the lower reservoir

Potential
 energy
 converted to
 kinetic energy



- □ Kinetic energy of falling water turns a turbine
- Turbine turns a generator
- Generator converts mechanical energy to electrical

energy



Renewable Energy Resources

- PHES first introduced in Italy and Switzerland in the 1890's

 - Four-unit (quaternary) systems
 - Turbine
 - Generator
 - Motor
 - Pump



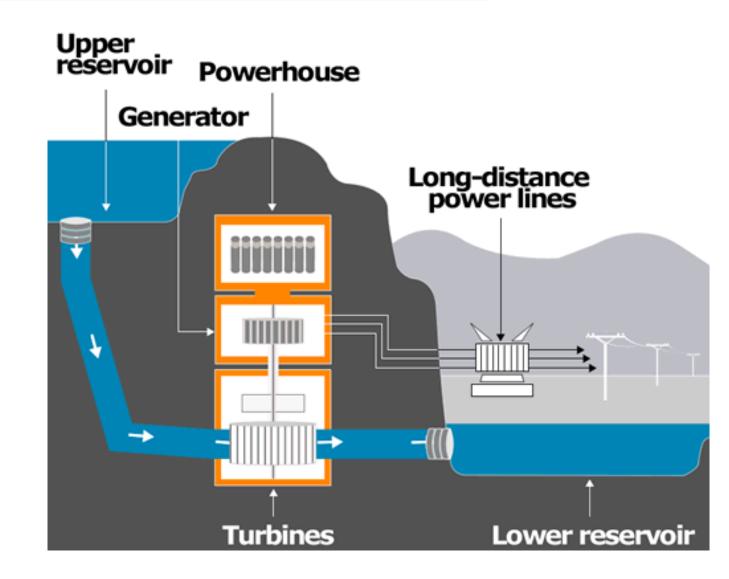


HISTORY OF PHES

Renewable Energy Resources

□ First PHES plant in the US:

- Rocky River hydro plant, New Milford, CT
- Water from the
 Housatonic River pumped
 up into Candlewood Lake
- 230 feet of head
- □ 6 billion ft³ of water
- Two-unit (binary) system
 - Reversible pump/turbine one of the first
- 29 MW of generating power





□ PHES accounts for 99% of worldwide energy storage

- □ Total power: \sim 127 GW
- Total energy: \sim 740 TWh
- Power of individual plants: 10s of MW 3 GW
- In the US:
 - □ ~40 operational PHES plants
 - 75% are > 500 MW strong economies of scale
 - □ Total power: ~23 GW
 - Current plans for an additional ~6 GW
 - □ Total energy: \sim 220 TWh



upper reservoir

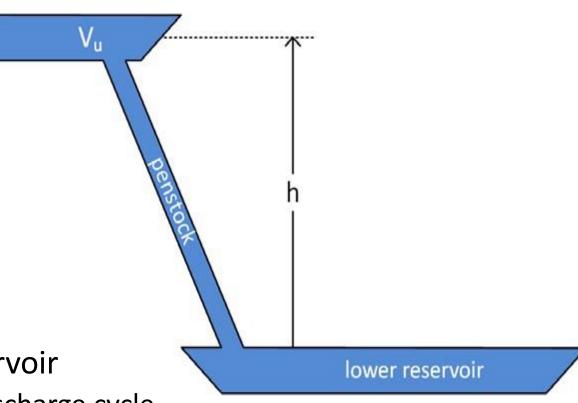
Two storage reservoirs

- Upper and lower
- Lower reservoir
 may be a river or
 even the sea

Separated by a height, h

- The hydraulic head
- \square Assume $h \gg$ depth of the upper reservoir
 - h remains constant throughout charge/discharge cycle

 \Box Upper reservoir can store a volume of water, V_u





□ **Total stored energy** (assuming it is all at a height, h)

 $E_t = mgh = V_u \rho gh$

where $ho = 1000 \ kg/m^3$ is the density of water

Verifying that we do, in fact, have units of energy

$$[E_t] = m^3 \frac{kg}{m^3} \frac{m}{s^2} m = \frac{kg \cdot m}{s^2} m = N \cdot m = J$$

The *energy density* – energy per unit volume – of the stored water is therefore

$$e_v = \frac{E_t}{V_u} = \rho g h$$
$$[e_v] = \frac{kg}{m^3} \frac{m}{s^2} m = \frac{kg \cdot m^2}{s^2} \frac{1}{m^3} = \frac{J}{m^3}$$



The energy density of the stored water is also the *hydrostatic pressure* at the level of the lower reservoir

$$p = \rho g h$$

$$[p] = \frac{kg}{m^3} \frac{m}{s^2} m = \frac{kg \cdot m}{s^2} \frac{1}{m^2} = \frac{N}{m^2} = Pa$$

This is the *energy density* of the water at the turbine



The rate at which energy is transferred to the turbine (from the pump) is the power extracted from (delivered to) the water

$$P = e_{v}QQ = pQQ = \rho ghQQ$$

where *Q* is the *volumetric flow rate* of the water

$$[P] = \frac{J}{m^3} \frac{m^3}{s} = \frac{J}{s} = MW$$

This is the total power available at the turbine

 Greater than (less than) the power actually delivered to the turbine (from the pump), due to inefficiencies



Note that *power* is given by the product of a driving potential, or *effort*, p, and a *flow*, Q

P = pQQ

□ Similar to power for a *translational mechanical* system

P = Fv

where the effort is force, F, and the flow is velocity, v

□ Or, a *rotational mechanical* system

$$P = \tau \omega$$

where the effort is torque, $\tau,$ and the flow is angular velocity, v



- Pumped hydro plants can supply large amounts of both *power* and *energy*
- Can quickly respond to large load variations
- □ Uses for PHES:

Peak shaving/load leveling

- Help meet loads during peak hours
 - Generating while releasing water from upper reservoir
 - Supplying expensive energy
- Store energy during off-peak hours
 - Pumping water to the upper reservoir
 - Consuming inexpensive energy



Frequency regulation

- Power variation to track short-term load variations
- Helps maintain grid frequency at 60 Hz (50 Hz)

Voltage support

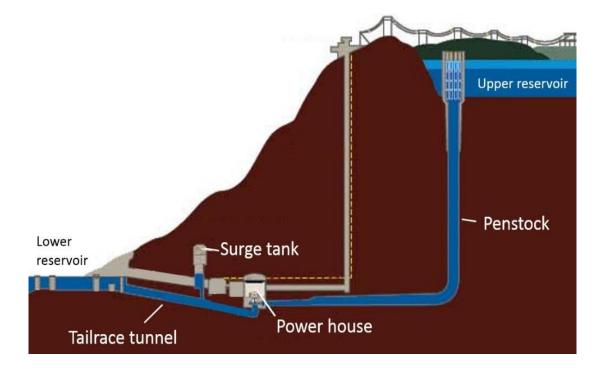
- Reactive power flow control to help maintain desired grid voltage
 - Varying the field excitation voltage of the generator/motor
- □ Even at zero real power not pumping or generating
 - unloaded motor/generator can serve as synchronous condenser
 - Pump/turbine spinning in air



- Upper and lower
 reservoirs separated by
 an elevation difference
- □ Two configurations:
 - **Open-loop**:
 - At least one of the reservoirs connected to a source of natural inflow
 - Natural lake, river, river-fed reservoir, the sea

Closed-loop:

- Neither reservoir has a natural source of inflow
- Initial filling and compensation of leakage and evaporation provided by ground water wells
- Less common than open-loop



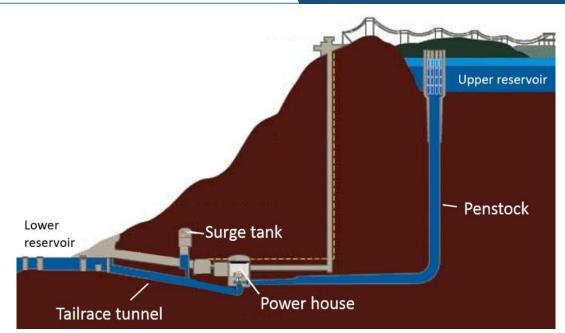


PHES COMPONENTS – PENSTOCK

Renewable Energy Resources

Penstock

- Conduit for water flowing between reservoirs and to the pump/generator
- Above-ground pipes or below ground shafts/tunnels
 - 5 -10 m diameter is common
 - One plant may have several penstocks
 - Typically steel- or concrete-lined, though may be unlined
- □ Flow velocity range of 1 5 m/s is common
- $\hfill Tradeoff between cost and efficiency for a given flow rate, <math display="inline">Q\!\!Q$
 - Larger cross-sectional area:
 - Slower flow
 - Lower loss
 - Higher cost





PHES COMPONENTS

Renewable Energy Resources

Upper reservoir

Tailrace tunnel

- Typically, larger
 diameter than penstocks
- □ Lower pressure
- Lower flow rate
- Downward slope from lower reservoir to pump/turbine
 - Inlet head helps prevent cavitation in pumping mode

Lower reservoir Tailrace tunnel

Surge tanks

- Accumulator tanks to absorb high pressure transients during startup and mode changeover
- May be located on penstock or tailrace
- Especially important for longer tunnels
- Hydraulic bypass capacitors



Renewable Energy Resources

Power house

- Contains pump/turbines and motor/generators
- Often underground
- Typically below the level of the lower reservoir to provide required pump inlet head

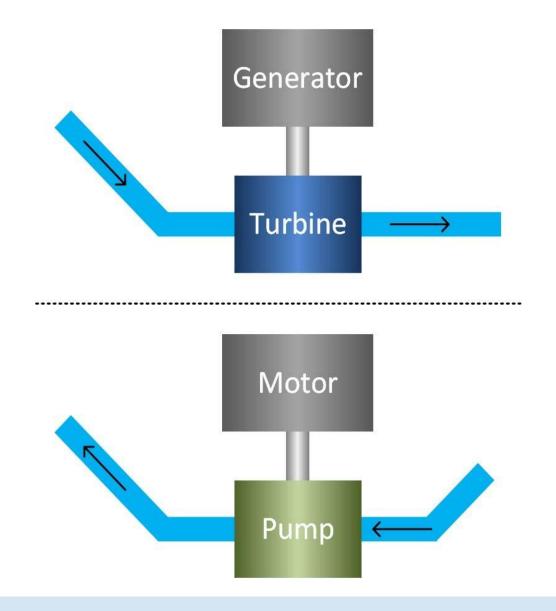
- Lower reservoir Tailrace tunnel
- □ Three possible configurations
 - Binary set: one pump/turbine and one motor/generator
 - Ternary set: one pump, one turbine, and one motor/generator
 - Quaternary set: separate pump, turbine, motor, and generator



POWER PLANT CONFIGURATIONS – QUATERNARY SET

Quaternary set

- Pump driven by a motor
- □ Generator driven by a turbine
- Pump and turbine are completely decoupled
- Possibly separate penstocks/tailrace tunnels
- Most common configuration prior to 1920
- High
 equipment/infrastructure
 costs
- High efficiency
 - Pump and turbine designed to optimize individual performance

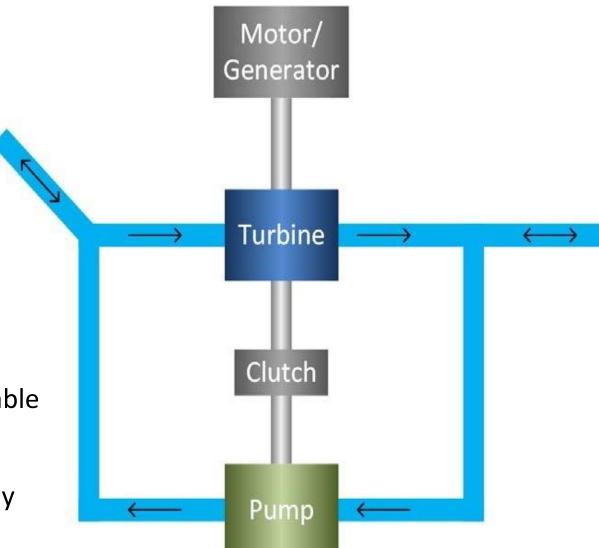




POWER PLANT CONFIGURATIONS – TERNARY SET

Ternary set

- Pump, turbine, and motor/generator all on a single shaft
 - Pump and turbine rotate in the same direction
- Turbine rigidly coupled to the motor/generator
- Pump coupled to shaft with a clutch
- Popular design 1920 1960s
- Nowadays, used when head exceeds the usable range of a single- stage pump/turbine
 High-head turbines (e.g., Pelton) can be used
- Pump and turbine designs can be individually optimized

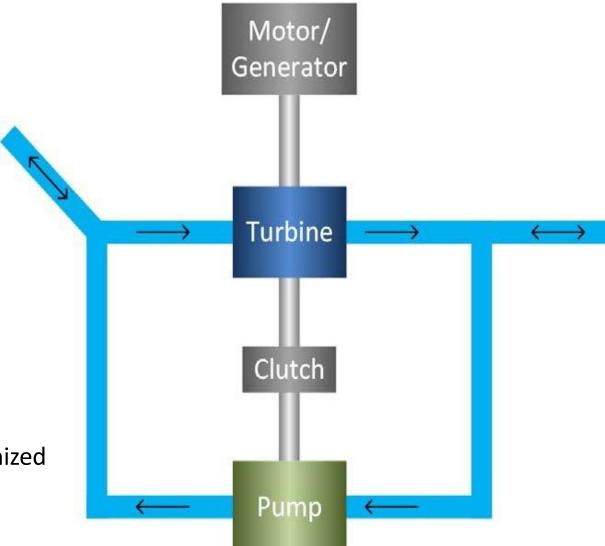




POWER PLANT CONFIGURATIONS – TERNARY SET

Ternary set

- Generating mode:
 - Turbine spins generator
 - Pump decoupled from the shaft and isolated with valves
- Pumping mode:
 - Motor turns the pump
 - Turbine spins in air, isolated with valves
- Both turbine and pump can operate simultaneously
- Turbine can be used for pump startup
 - Both spin in the same direction
 - Turbine brings pump up to speed and synchronized with grid, then shuts down
 - Changeover time reduced

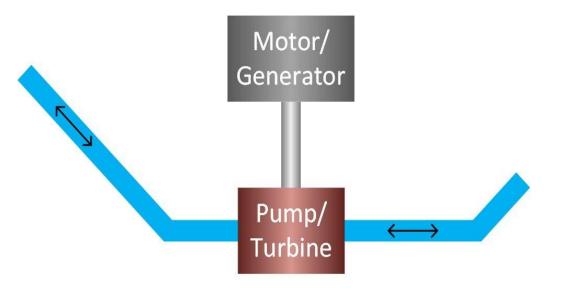




POWER PLANT CONFIGURATIONS – BINARY SET

Binary set

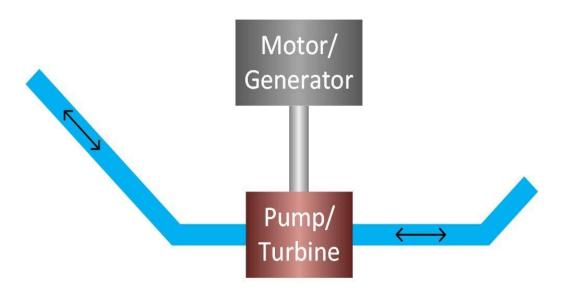
- Single reversible
 pump/turbine coupled to a
 single motor/generator
- Most popular
 configuration for modern
 PHES
- Lowest cost configuration
 - Less equipment
 - Simplified hydraulic pathways
 - Fewer valves, gates, controls, etc.
- Lower efficiency than for ternary or quaternary sets
 - Pump/turbine runner design is a compromise between pump and turbine performance





Binary set

- Rotation is in opposite directions for pumping and generating
- Shaft and motor/generator must change directions when changing modes



- Slower changeover than for ternary or quaternary units
- Pump startup:
 - Pump/turbine runner dewatered and spinning in air
 - Motor brings pump up to speed and in synchronism with the grid before pumping of water begins



- Hydro turbine design selection based on
 - □ Head
 - Flow rate
- PHES plants are typically sited to have large head
 - Energy density is proportional to head
 - Typically 100s of meters
- Reversible *Francis* pump/turbine
 - Most common turbine for PHES applications
 - Single-stage pump/turbines operate with heads up to 700
 - m
- □ For higher head:
 - Multi-stage pump/turbines
 - Ternary units with *Pelton* turbines



- Pump/turbine shaft connects to a motor/generator unit
 - Above the turbine runner in typical vertical configuration
- □ Motor/generator type depends PHES category:
 - □ Fixed-speed pump/turbine
 - Variable-speed pump/turbine

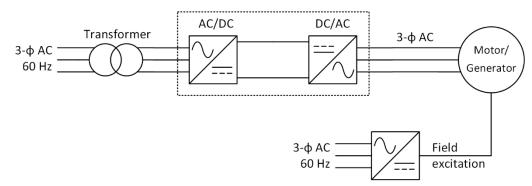
Fixed-speed pump/turbine

- Motor/generator operates at a fixed speed in both pumping and generating modes
- **Synchronous motor/generator**
 - Rotation is synchronous with the AC grid frequency
 - Stator windings connect to three-phase AC at grid frequency
 - Rotor windings fed with DC excitation current via slip rings
 - DC excitation current generated with thyristor AC/DC converters



MOTOR/GENERATOR

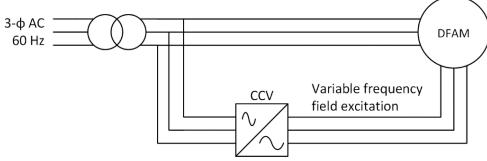
- Variable-speed (adjustable-speed) pump/turbine
 - Rotational speed of motor/generator is adjustable
 - Two options:
 - Variable speed using a synchronous motor/generator (singly-fed)
 - Doubly-fed asynchronous machine (DFAM)
- □ Variable-speed operation with synchronous motor/generator:



- Motor driven with variable frequency
- Decoupled from grid frequency by back-to-back converters
- Converters must be rated for full motor/generator power
 - Large, expensive



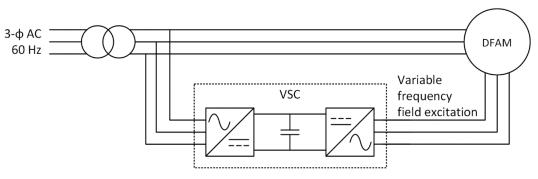
- □ Variable speed using doubly-fed asynchronous machines
 - Field excitation fed with variable, low-frequency AC, not DC as in synchronous machines
 - Static frequency converter generates variable AC
 - Cycloconverter
 - Back-to-back voltage-source converters
 - Typically small speed range (e.g., $\pm 10\%$)
- With *cycloconverter* generating variable-frequency excitation for rotor:



- Converters need not be sized for rated motor/generator power
 - Only supply lower-power excitation to the rotor



DFAM with variable-frequency field excitation generated by back-to-back VSCs:



- The preferred configuration for large (>100 MW) PHES plants nowadays
- □ Advantages of variable-speed plants
 - Pump and turbine speeds can be independently varied to optimize efficiency over range of flow rate and head
 - Pumping power can be varied in addition to generating power

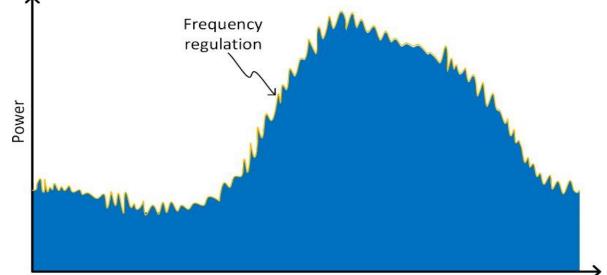


Frequency regulation

- Tracking short-term load variations to maintain grid frequency at 60 Hz (or 50 Hz)
- PHES plants can provide frequency regulation
 - Different for fixed- or variable-speed plants

Fixed-speed plants

- Generating mode
 - Frequency regulation provided by rapidly varying power output
 - Power varied by using wicket gates to modulate flow rate
 - Same as in conventional hydro plants
- Pumping mode
 - Pump operates at rated power only power input cannot be varied
 - No frequency regulation in pumping mode

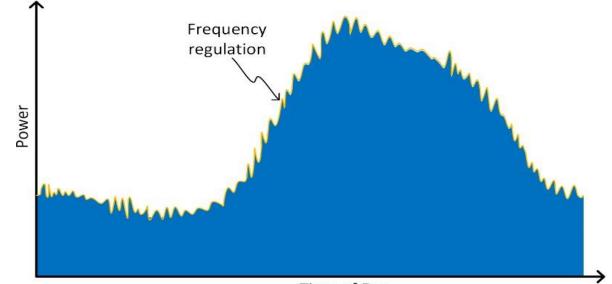


Time of Day



Variable-speed plants

- Pump speed can be varied
 over some range, e.g. ±10%
- Pump power is proportional to pump speed *cubed*
 - For ±10% speed variation, power is adjustable over ±30%



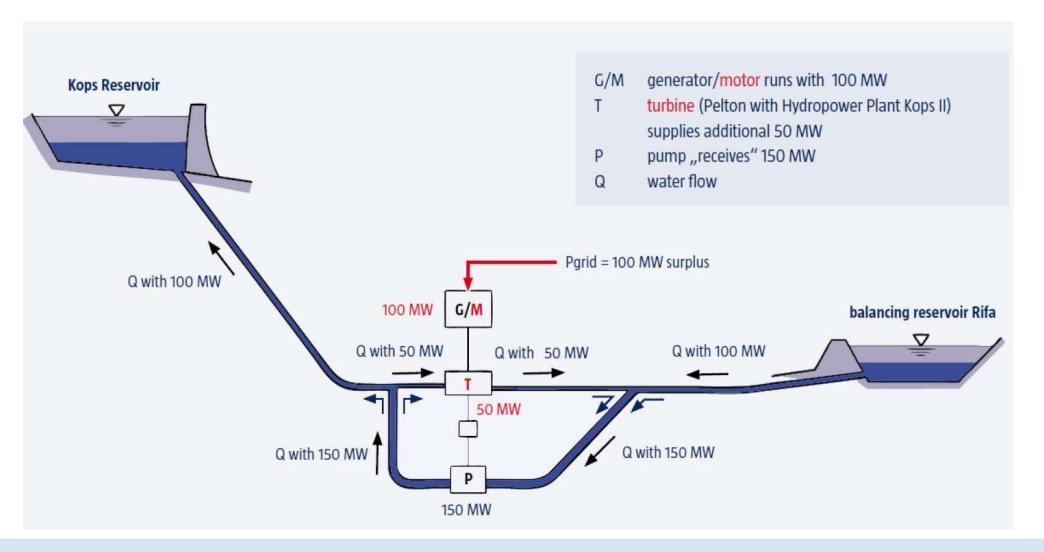
Time of Day

- Power variation in pumping mode can track rapid load variations
- Frequency regulation can be provided in both modes of operation



HYDRAULIC SHORT CIRCUIT

□ Kops II PHES plant in Austrian Alps:





1

□ Round-trip efficiency:

$$\eta_{rt} = \frac{E_{out}}{E_{in}} \cdot 100\%$$

where

- *E_{in}* is the electrical energy that flows in from the grid to the plant in pumping mode
- *E*_{out} is the electrical energy that flows from the plant to the grid in generating mode
- □ Typical round-trip efficiency for PHES plants in the range of 70% 80%
- PHES loss mechanisms
 - Transformer
 - Motor/generator
 - Pump/turbine
 - Water conduit



Transformers

- Pumped hydro plants connect to the AC electrical grid
 - Transformers step voltage between high voltage on the grid side to lower voltage at the motor/generator
- Transformer *loss mechanisms*:
 - Winding resistance
 - Leakage flux
 - Hysteresis and eddy currents in the core
 - Magnetizing current finite core permeability
- Power flows through transformers on the way into the storage plant and again on the way out
- □ Typical loss: ~0.5%



Motor/generator losses

- Electrical resistance
- Mechanical friction
- □ Typical loss: ~2%

Pump/turbine

- □ Single runner in binary sets
 - Typically lower efficiency, particularly for fixed-speed operation design of both compromised
- □ Separate runners in ternary, quaternary sets
 - Higher efficiency
- □ Typical loss: ~7% 10%

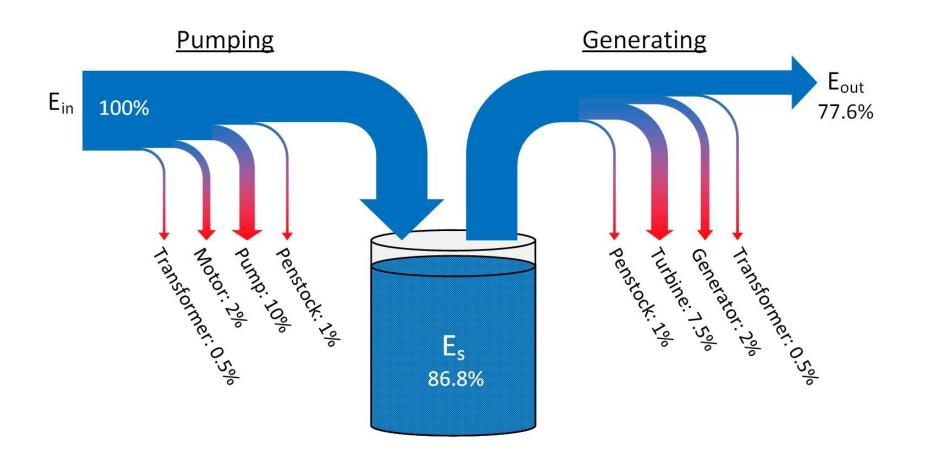


Penstock

- Frictional loss of water flowing through the conduit
 - Major losses along penstock
 - Minor losses from bends, penstock inlet, turbine inlet, etc.
- Dependent on
 - Flow velocity
 - Penstock diameter
 - Penstock length
 - Penstock lining steel, concrete, etc.
- High head is desirable, but long penstocks are not
 - Steeper penstocks reduce frictional losses for a given head
 - Typical length-to-head ratio: 4:1 12:1
- □ Typical loss: ~1%



□ Typical losses for PHES:





□ *Efficiency of the pumping operation* is given by

$$\eta_p = \frac{E_s}{E_{in}} \cdot 100\%$$

where

 \Box E_s is the energy stored

• Potential energy of the volume of water, V_u , pumped to the upper reservoir

 $E_s = V_u \rho g h$

 \Box E_{in} is the energy input from the grid during the pumping operation

□ The mechanical energy input to the pump is

$$E_{in,pump} = E_{in} \cdot \eta_{trans} \cdot \eta_{motor}$$

where

 η_{trans} and η_{motor} are the efficiencies of the transformer and motor, respectively



□ The volume of water pumped to the upper reservoir is

$$V_u = \frac{E_{in,pump}}{\rho g h} \cdot \eta_{pump} \cdot \eta_{pipe,p}$$

where

- \Box η_{pump} is the pump efficiency
- $\ \ \eta_{pipe,p}$ is the penstock efficiency in pumping mode
- So, the total pumped volume of water is $V_u = \frac{E_{in}}{\rho gh} \cdot \eta_{trans} \cdot \eta_{motor} \cdot \eta_{pump} \cdot \eta_{pipe,p}$
- □ The *pumping-mode efficiency* is therefore:

$$\eta_p = \frac{E_s}{E_{in}} = \eta_{trans} \cdot \eta_{motor} \cdot \eta_{pump} \cdot \eta_{pipe,p}$$



Efficiency of the generating operation is given by

$$\eta_{gg} = \frac{E_{out}}{E_s} \cdot 100\%$$

 Due to frictional losses in the penstock, the hydraulic energy that reaches the turbine is

$$E_{in,t} = E_s \cdot \eta_{pipe,gg}$$

□ The amount of rotational energy at the turbine output/generator input is

$$E_{in,gg} = E_{in,t} \cdot \eta_t = E_s \cdot \eta_{pipe,gg} \cdot \eta_t$$

 After generator and step-up transformer losses, the energy output to the grid is

$$E_{out} = E_{in,gg} \cdot \eta_{ggen} \cdot \eta_{trans}$$

$$E_{out} = E_s \cdot \eta_{pipe,gg} \cdot \eta_t \cdot \eta_{ggen} \cdot \eta_{trans}$$



Generating mode efficiency is

$$\eta_{gg} = \frac{E_{out}}{E_s} = \eta_{pipe,gg} \cdot \eta_t \cdot \eta_{ggen} \cdot \eta_{trans}$$

□ The *overall round-trip efficiency* is therefore

$$\eta_{rt} = \frac{E_{out}}{E_{in}} = \eta_p \cdot \eta_{gg}$$

 $\eta_{rt} = \eta_{trans} \cdot \eta_{motor} \cdot \eta_{pump} \cdot \eta_{pipe,p} \cdot \eta_{pipe,gg} \cdot \eta_t \cdot \eta_{ggen} \cdot \eta_{trans}$



Disadvantages of PHES

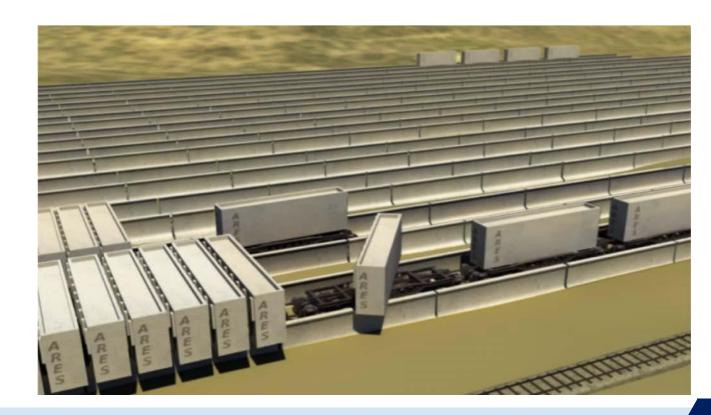
- Environmental issues
 - Water usage
 - River/habitat disruption
- Head variation
 - Pressure drops as upper reservoir drains
 - Efficiency may vary throughout charge/discharge cycle
 - Particularly an issue for lower-head plants with steep, narrow upper reservoirs
- Siting options are limited
 - Available water
 - Favorable topography
 - Large land area
- Possible alternative potential energy storage:
 - Rail energy storage



RAIL ENERGY STORAGE

Rail energy storage

- Electric-motor-driven railcars
- Weights are shuttled up and down an incline between upper and lower storage yards
- Power input drives motors to move weights up the track
- Regenerative
 braking on the way
 down supplies
 power to the grid
- Weights are loaded and unloaded at storage yards
 - Large quantities of energy can be stored with few trains

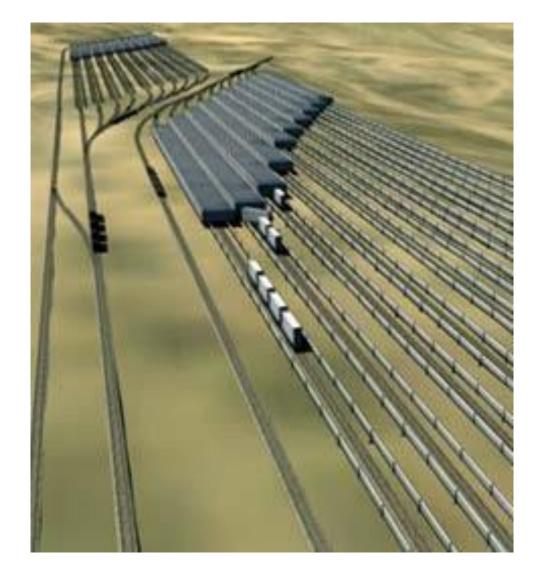




ADVANTAGES OF RAIL ENERGY STORAGE

Renewable Energy Resources

- More siting options than for PHES
 - Open space
 - Elevation change
 - No need for water or topography conducive to reservoirs
- Lower capital cost than PHES
- Easily scalable
- Efficient
 - RT efficiency: 78% 86%
 - Constant efficiency, independent of SoC
- No standby losses
 - No evaporation/leakage





HOW DOES IT WORK?

Renewable Energy Resources

Renewable Energy Resources



Thank you very much for your attention!

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